

REPORT OF GEOTECHNICAL CONSULTING SERVICES

Wal★Mart SuperCenter Store No. 3873-00 SEC Interstate Highway 75 and U.S. Highway 441 City of Alachua, Alachua County, FL

> UES Project No. 70080-077-06 UES Report No. 385573

Prepared for:

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April 30, 2005

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April 30, 2005

CPH Engineers, Inc. 500 West Fulton Street Sanford, FL 32771

Attention: Maria C. Zapata, P.E.

Reference: Report of Geotechnical Consulting Services Proposed Wal★Mart SuperCenter Store No. 3873-00 SEC Interstate Highway 75 and U.S. Highway 441 City of Alachua, Alachua County, Florida UES Project No. 70080-077-06 UES Report No. 385573

Dear Ms. Zapata:

Universal Engineering Sciences, Inc. (UES) has completed the final geotechnical study for the above referenced site in the City of Alachua, Alachua County, Florida. The geotechnical exploration was conducted in general accordance with the Professional Services Subconsultant Agreement prepared by CPH Engineer on December 27, 2004 for the Final Geotechnical Evaluation. The geotechnical exploration program was performed in accordance with generally accepted soil and foundation engineering practices, and Wal * Mart's "Geotechnical Investigation Specifications and Report Requirements for Florida Projects" effective October 5, 2004.

This Report incorporates the findings of the final subsurface exploration program plus the findings of the preliminary exploration program as summarized in UES Report of Preliminary Geotechnical Consulting Services dated October 28, 2004. The information presented in this final Report supercedes our office's previous submittals for the referenced project.

This Report presents the results of our field and laboratory exploration programs, and provides recommendations for geotechnical site preparation, subgrade preparation, excavations, foundation design and construction, pavement design, retaining wall design, groundwater control, stormwater management system design, and other pertinent geotechnical concerns.

Respectfully submitted,

UNIVERSAL ENGINEERING SCIENCES, INC.

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EXECUTIVE SUMMARY

This final Report incorporates the findings of the final subsurface exploration program plus the findings of the preliminary exploration program as summarized in UES Report of Preliminary Geotechnical Consulting Services dated October 28, 2004. The information presented in this final Report supercedes our office's previous submittals for the referenced project.

We have prepared this executive summary solely to provide a general overview. We recommend that you do not rely on this executive summary for any purpose except for which it was prepared. We recommend that you rely on the complete final geotechnical Report for information about findings, recommendations and other project-related concerns.

Project Location and Description

UES was provided a Conceptual Site Plan prepared by CPH Engineers, Inc. The drawing shows the proposed project as consisting of a Wal Mart SuperCenter retail complex. The proposed project parcel is located adjacent to, and in the southeast quadrant of the intersection of, Interstate Highway 75 and U.S. 441 in the City of Alachua, Alachua County, Florida.

The proposed parcel lies within Sections 15 and 16, Township 8 South and Range 18 East, and covers approximately 31 acres. The parcel is undeveloped and historically has been used as agricultural pasture land.

The proposed parcel for the building, parking and stormwater management pond has approximate plan dimensions of about 1,000 feet by 1,300 feet. The main retail structure is shown to be single story, block construction with a gross plan area of approximately 183,347 square feet. Parcel access driveways and roadways will be sited to the east of the main project parcel.

The proposed project layout has the building complex located on the northern 1/3 portion of the main parcel, with the majority of the parking areas located in the central 1/3 of the same parcel, and the stormwater management pond located in the southern 1/3 of the parcel.

Based on the finished floor elevation and grading plan information provided to our office, it is anticipated that on the order of 2 to 20 feet of cut will be needed for building pad construction, as reflected by 13 out of 17 soil test borings, which suggests approximately 75% of the building footprint will require some degree of cut operations. The remaining building footprint will require on the order of 4 to 6 feet of fill placement.

Based on the finished pavement elevation and grading plan information provided to our office, it is anticipated that on the order of 2 to 23 feet of cut will be needed for proposed parking lot construction, as reflected by 46 out of 83 soil test borings, which suggests approximately 55% of the parking lot will require some degree of cut operations. The remaining portions of the parking lot will require on the order of 2 to 19 feet of fill placement.

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Based on the finished pond elevation and grading plan information provided to our office, it is anticipated that on the order of 2 to 18 feet of cut will be needed for the retention pond construction, as reflected by 35 out of 37 soil test borings, which suggests approximately 95% of the retention pond will require some degree of cut operations during construction. The remaining portions of the retention pond will require on the order of 5 to 6 feet of fill placement.

Soil and Groundwater Condition

Groundwater levels were apparent and measured at only 12 soil test borings locations during the field exploration program. The groundwater level measurements ranged from about 3 to 23 feet below the existing site grades. Fluctuations in the measured groundwater level depths can most likely be attributed to topographic and soil compositional differences across the project site, and borehole disturbance associated with the soil drilling process. The potentiometric surface map of the upper Florida aquifer suggest groundwater elevations, outside perched zones, might be expected to be on the order of +40 feet NGVD in the general area of the project site.

Building Footprint - Generally a sand profile was encountered from ground surface to depths of 4 to 19 feet below the existing site grades. The upper 1 to 4 feet, with an average of about 2 feet, of the subsurface profile are primarily represented by relatively clean (percent fines of 10 or less) sands, and these are underlain by clayey to very clayey sands with thicknesses varying from 3 to 17 feet with an average of about 6 feet.

Underlaying the upper sands and clayey sands all the soil test borings encountered a sometimes sandy clay layer. The clay layer varied in thickness from 6 to 41 feet, with an average layer thickness of about 17 feet.

The clay zone was then found to be underlain by a clayey to slightly clayey sand varying in thickness from about 8 to 25 feet, with an average layer thickness of about 17 feet. The top of the limestone stratum was then encountered in 13 out of 17 soil test borings, representing about 76% of the test sites, at depths ranging from 27 to 57 feet, and with an average of about 39 feet, below the existing site grades. The limestone stratum was encountered continuous to the boring termination depths. Organic soils were not encountered in any of the soil test borings.

Stormwater Retention Pond - Generally a sand profile was encountered from ground surface to the boring termination depths, except where the top of the limestone stratum was encountered in the soil test borings. A total of 37 soil test borings were performed in this general area of the project parcel. In 35, or about 95% of those boring sites a relatively clean to slightly clayey sand layer was encountered from ground surface with a layer thickness range of 1 to 22 feet, and with an average layer thickness of approximately 6 feet.

Beneath the surficial sands, a clayey to slightly clayey sand zone was encountered with a thickness range of 6 to 40 feet, and with an average thickness of about 24 feet. This sand zone is characterized with laterally discontinuous clay lenses or seams found at various depths in the subsurface profile. The clay seams were found in 14, or about 38%, of the borings with thicknesses varying from 2 to 20 feet and average of about 7 feet.

The top of the limestone stratum was encountered in 21 out of 37 soil test borings, representing about 57% of the test sites, at depths ranging from 18 to 37 feet, and with an average of about 28 feet, below the existing site grades. The limestone stratum was encountered continuous to the boring termination depths. Organic soils were not encountered in any of the soil test borings.

Parking Lot - A total of 83 soil test borings were performed in this general area of the project parcel. Generally a sand profile, grading with increasing depth from relatively clean at ground surface to clayey to very clayey, was encountered overlying a sometimes sandy clay zone. In 45, or about 54%, of the borings the relatively clean surficial sand zone was found from ground surface with a layer thickness range of 1 to 8 feet, and with an average layer thickness of 2 feet.

In 82 out of 83 borings, the surficial sands were directly underlain by 3 to over 20 feet of clayey to very clayey sands. These clayey sands were sometimes encountered from ground surface, and were measured with an average layer depth of about 9 feet.

In 70, or about 84% of the soil test borings a sometimes sandy clay zone was encountered with a layer thickness range of 1 to 20 feet, and with an average layer thickness of approximately 8 feet. In one soil test boring the clay layer was encountered from ground surface.

Beneath the clay zone, a clayey to slightly clayey sand zone was encountered in 33, or about 40%, of the soil test borings with a thickness range of 1 to 12 feet, and with an average thickness of about 5 feet. Neither the limestone stratum nor organic soil layers were encountered in these soil test borings.

Groundwater Control

Groundwater levels and seasonal high groundwater levels will be significantly affected by the proposed construction and grading plans which will modify the surface and subsurface hydrology. Earthwork in both building and pavement areas is anticipated to encroach on the seasonal high water table. It may be necessary to provide a permanent subsurface drainage system for some improvements to maintain the recommended separation between the water table and various structural elements in the building and pavement areas.

Positive drainage measures should be established and maintained on the project site during construction and throughout the life of the project. Excavation dewatering may be required during site preparation and excavation activities during some phases of the proposed construction. Contract documents should provide for determining the depth to the groundwater table just prior to construction, and for any required remedial dewatering.

Geotechnical Site Preparation

Geotechnical site preparation on the subject parcel will consist of general site clearing and grubbing to remove the existing vegetation, organic topsoils, plant roots and other deleterious materials, followed by cut operations, proof-rolling, surface densification, and fill placement to construction grade with structural fill soils.

Foundation Design

Following completion of geotechnical site preparation activities and building pad construction, the proposed structure may be supported on conventional, shallow spread foundations designed with an allowable soil bearing pressure of 2,500 pounds per square foot (psf) provided the building pad preparation recommendations presented in this Report are followed. Foundation design and construction recommendations are also presented in this Report.

Pavement Design

Rigid and flexible pavement sections may be used on this project. The most readily available flexible pavement base material in Alachua County is crushed limerock. Pavements should be designed as a function of the anticipated traffic loadings. Flexible pavements should incorporate a stabilized subgrade, a base course, and a surface course. Rigid pavement sections should be used in areas subject to heavy truck traffic and impact loading. All pavement designs should incorporate the effects of groundwater, irrigated landscape areas, and construction traffic. Complete recommendations for both flexible and rigid pavements are presented in this Report.

Stormwater Retention Pond Design

Design recommendations for the proposed stormwater retention pond are presented in this Report. The subsurface conditions at the proposed stormwater management areas were evaluated in the field using standard penetration test borings. The soil profile encountered in the proposed retention pond area can be generalized as follows: 1 to 22 feet of relatively clean to slightly clayey sand layer (average layer thickness of approximately 6 feet), followed by a clayey to slightly clayey sand zone with a thickness range of 6 to 40 feet (average thickness of about 24 feet). This lower sand zone is characterized with laterally discontinuous clay lenses or seams found at various depths in the subsurface profile.

Groundwater levels were not apparent in any of the stormwater retention pond boreholes during the exploration work. Our best estimate for the pre-development wet season high groundwater level is approximately from the existing ground levels to 6 feet below ground surface. The results of the laboratory permeability tests on the surficial sands ranged from 1 to 9 feet per day indicating moderate infiltration characteristics.

Excavation Considerations

Geotechnical site preparation on the subject parcel will include significant cut and fill earthwork operations. Within the proposed building footprint, cut operations are anticipated to expose clayey to very clayey sand layers. Over-excavation of clayey soils may be recommended based on their engineering characteristics and/or seasonal groundwater and seepage considerations.

It also may be recommended to place an underdrain system along the toe of major cut areas up-slope of the building pad and pavement areas to intercept lateral seasonal seepage and stormwater runoffs that could affect performance of these improvements. Temporary groundwater control should be anticipated during certain excavation procedures. Typically, these measures are determined by the contractor but may consist of perimeter ditches and interior ditches, as necessary, which are graded to sumps so the groundwater can be pumped away from the excavated construction areas.

Within the proposed parking lot, cut operations are also anticipated to penetrate primarily clayey to very clayey sand layers. Excavations for retention pond construction are anticipated to yield mostly relatively clean to slightly clayey sands.

Suitability of the excavated soils will require further evaluation, however, as a rule the relatively clean sands should be appropriate for both structural fill and backfill purposes, where as the clayey to very clayey sands generally require more construction/compaction effort, are more sensitive to moisture content in the soil mass, and would require more attention from the Geotechnical Engineer during earthwork activities. Optimal use of the clayey sands might be found in the initial (deeper) fill lifts in both building footprint and parking lot areas. Appropriate compaction levels should be evaluated.

Due to the significant quantities of anticipated on-site excavated soils, and the cost impact associated with off-site fill soil sources, a comprehensive soils laboratory program will be warranted for the evaluation of soil engineering properties and applications suitability. These tests should be used to assess the following at a minimum: shrink/swell potential of clay and clay/sand soils; slope stability of planned cut banks including recommended slope inclinations and benching; and earth retaining structure design parameters. If needed, additional structural fill may be imported from local borrow pits.

1.0 INTRODUCTION

Universal Engineering Sciences, Inc. (UES) has completed various subsurface explorations for the above referenced site in Alachua, Alachua County, Florida. The geotechnical explorations were conducted in general accordance with the Professional Services Subconsultant Agreement prepared by CPH Engineer on December 27, 2004 for the Final Geotechnical Evaluation. The geotechnical exploration programs were performed in accordance with generally accepted soil and foundation engineering practices, and Wal ★ Mart's "Geotechnical Investigation Specifications and Report Requirements for Florida Projects" effective October 5, 2004.

This Report incorporates the findings of our recent subsurface exploration plus the findings of our previous explorations (Interim Preliminary Geotechnical Exploration Report dated October 20, 2004, and the Preliminary Geotechnical Exploration Report dated October 28, 2004) completed by UES. The information presented in this final Report supercedes our office's previous submittals for the referenced project.

2.0 PROJECT LOCATION AND DESCRIPTION

UES was provided a Conceptual Site Plan prepared by CPH Engineers, Inc. The drawing shows the proposed project as consisting of a Wal ★ Mart Supercenter retail complex. The proposed project parcel is located adjacent to, and in the southeast quadrant of, the intersection of Interstate Highway 75 and U.S. 441 in the City of Alachua, Alachua County, Florida.

The proposed parcel lies within Sections 15 and 16, Township 8 South and Range 18 East, and covers approximately 31 acres. The parcel is undeveloped and historically has been used as agricultural pasture land.

The proposed parcel for the building, parking and stormwater management pond has approximate plan dimensions of about 1,000 feet by 1,300 feet. The main retail structure is shown to be single story, block construction with a gross plan area of approximately 183,347 square feet. Parcel access driveways and roadways will be sited to the east of the main project parcel.

The proposed project layout has the building complex located on the northern 1/3 portion of the main parcel, with the majority of the parking areas located in the central 1/3 of the same parcel, and the stormwater management pond located in the southern 1/3 of the parcel.

2.1 Building

The proposed building finished floor elevation has been set at +118 feet MSL. Current ground surface elevations in this general area of the project parcel range from about +140 feet MSL (southwest end) to about +110 feet MSL (northeast end), with a fairly uniform downward slope to the north and northeast.

The above information suggests both cut and fill earthwork operations will be required for geotechnical site preparation and building pad construction. Based on the finished floor elevation and grading plan information provided to our office, it is anticipated that on the order of 2 to 20 feet of cut will be needed for building pad construction, as reflected by 13 out of 17 soil test borings, which suggests approximately 75% of the building footprint will require some degree of cut operations. The remaining building footprint will require on the order of 4 to 6 feet of fill placement.

2.2 Parking Lot

The proposed paved parking lot finished elevations will result in a downward slope (approximately 2.5%) to the north from elevation +117 feet MSL to elevation +107 feet MSL. Current ground surface elevations in this general area of the project parcel range from about +122 feet MSL (southwest end) to about +92 feet MSL (northeast end), with a fairly uniform downward slope to the north-northeast.

The above information suggests both cut and fill earthwork operations will be required for geotechnical site preparation and parking lot pavement construction. Based on the finished pavement elevation and grading plan information provided to our office, it is anticipated that on the order of 2 to 23 feet of cut will be needed for proposed parking lot construction, as reflected by 46 out of 83 soil test borings, which suggests approximately 55% of the parking lot will require some degree of cut operations. The remaining portions of the parking lot will require on the order of 2 to 19 feet of fill placement.

2.3 Stormwater Retention Pond

The proposed stormwater retention pond will have a bottom elevation of +77 feet MSL, with top of north bank elevation set at +88 feet MSL and a top of south bank elevation of +83 feet MSL. An earth retaining wall is proposed along the south side of the retention pond adjacent to the parking lot. Current ground surface elevations in this general area of the project parcel range from about +97 feet MSL (southwest end) to about +79 feet MSL (north end), with a fairly uniform downward slope to the north.

The above information suggests both cut and fill earthwork operations will be required for pond construction. Based on the finished pond elevation and grading plan information provided to our office, it is anticipated that on the order of 2 to 18 feet of cut will be needed for the retention pond construction, as reflected by 35 out of 37 soil test borings, which suggests approximately 95% of the retention pond will require some degree of cut operations during construction. The remaining portions of the retention pond will require on the order of 5 to 6 feet of fill placement.

We understand it would be desirable to reuse the excavated soils from the various project areas for general site grading purposes over other project areas.

2.4 Structural Loading Information

The proposed Wal \bigstar Mart SuperCenter will be a prototype C-176-SGR-OR, single story, high bay commercial structure. The retail store building will be constructed using a combination of concrete masonry shear walls (load-bearing and non-load-bearing), and steel columns supporting roof loads by means of steel joist girders and steel joists. Typical bay spacing between columns and walls is approximately 55 by 48 feet, with exterior columns spaced at about 48 feet apart. Typical gravity loads for interior columns are 85 kips with a maximum total loading under severe live load conditions of 150 kips.

Maximum column uplift force from wind is estimated at 30 kips. Typical gravity loads for exterior columns are 50 kips each. The concrete masonry wall gravity loads range from 1.5 to 2 kips per lineal foot for non-load bearing walls, and 4 to 6 kips per lineal foot for load bearing walls. The estimated maximum uniform floor slab live load is 125 pounds per square foot, and the estimated maximum concentrated floor slab load is 5 kips.

2.5 Pavement Design Information

Two types of pavement sections will be utilized on this project: standard duty pavement and heavy duty pavement. The standard duty pavement will have primarily car and pickup truck traffic which will exert equivalent 18 kip single axle loads (E_{18} SAL) of 109,500 over a 20-year design life. The heavy duty pavement section will have periodic heavy truck traffic exerting loadings of approximately 335,800 E_{18} SAL over the 20-year design life. Terminal serviceability, initial serviceability, and reliability for all pavement sections will be 2.0, 4.2 and 85%, respectively.

If any of the above information is incorrect or changes prior to construction, please contact Universal Engineering Sciences immediately so that we may revise the recommendations contained in this Report, as necessary. In order to verify that our recommendations are properly interpreted and implemented, Universal Engineering Sciences must be allowed to review the final design and specifications prior to the start of construction, and understand that this is part of the overall geotechnical contract.

3.0 SITE DESCRIPTION

3.1 General

The subject site is a proposed Wal★Mart Supercenter Store located in the city of Alachua at the Southern Quadrant of US HWY 441 and I-75 and lies within Sections 15 and 16, Township 8 South, Range 18 East in Alachua County, Florida.

The general location of the subject site is shown in the attached Site Location Map. The proposed Wal-mart site contains approximately 31 acres (Wal Mart itself contains about 30 acres and the proposed gasoline station contains about 1 acre). The entrance roads contain approximately 5 acres.

UES engineering personnel visited the project parcel on several occasions prior to and during the performance of the field portion of this geotechnical study. The site is currently undeveloped. The parcel terrain was observed with a fairly uniform, downward slope from south to north. Most of the parcel is open pasture land with heavy grass cover. There are a number of trees, primarily concentrated along a natural shallow gully, found within the central portions of the parcel.

We did not observe evidence of shallow buried trash or debris or construction materials on the parcel. Fill soil conditions were not apparent. Surface soils were observed to be sands with fine roots, and with varying degrees of moisture content. We did not observe ponded surface water during our site visits except as noted below. The parcel is partially fenced.

The overall Wal \bigstar Mart site has a downward slope from south to north, from about +145 feet to +82 feet NGVD, and a natural ditch in the central section of the site ranging from about +150 feet to +110 feet NGVD. Ponded surface water was observed on the site at the time of our visit within the lateral limits of this natural ditch.

3.2 Soil Survey

The USDA Soil Survey of Alachua County, Florida describes the near-surface soil profile in the general project area as a mixture of Lochloosa fine sand with 2 to 8 percent slopes, Norfolk loamy fine sand with 2 to 8 percent slopes, Millhopper sand with 5 to 8 percent slopes, and Blichton sand with 2 to 5 percent slopes.

Lochloosa fine sand is characterized as gently sloping, somewhat poorly drained soils, with an estimated high water table in the range of 2.5 to 5 feet below ground under short-duration perched conditions.

Norfolk loamy fine sands are characterized as gentle sloping, well drained soils, with an estimated high water table in the range of 4 to 6 feet below ground under short-duration perched conditions.

Millhopper sand soils as sloping, moderately well drained soil, with an estimated high water table in the range of 3.5 to 6 feet below ground under short-duration perched conditions.

Blichton sand is characterized as gently sloping, poorly drained soils, with an estimated high water table in the range of 0 to 1 feet below ground under short-duration perched conditions.

Relevant engineering index properties of the sandy soils described above are summarized in Tables 1, 2, 3 and 4 on the following pages.

Depth	Туре	Classification	%	Plasticity	Shrink- Swell	Coef. of Perm	Risk of Corrosion	
(ln)			Fines	Index	Potential	(In/Hr)	Steel	Concrete
0 - 31	Sand	SP-SM, SM A-3, A-2-4	8 to 20	NP	Low	2 to 20	High	High
31-35	Loamy Sand	SM, SM-SC A-2-4	18 to 30	NP to 6	Low	0.6 to 6	High	High
35-54	Sandy Ioam	SC, SM-SC A-2, A-4, A-6	25 to 40	5 to 18	Low	0.6 to 0.2	High	High
54-83	Sandy clay, sandy clay loam	SC	40 to 50	15 to 25	Low	0.06 to 0.2	High	High

Table 1 - Engineering Index Properties of Lochloosa fine sand Soils

Table 2 - Engineering Index Properties of Norfolk loamy fine sand Soils

Depth	Туре	Classification	%	Plasticity	Shrink- Swell	Coef. of Perm.	Risk of Corrosion	
(ln)			Fines	Index	Potential	(In/Hr)	Steel	Concrete
0 - 11	Loamy fine sand	SM A-2	13 to 30	Nonplasti c	Low	2 to 20	Mod.	High
11- 46	Sandy loam, sandy clay loam	SC, SM-SC, CL, CL-ML A-2, A-4, A-6	30 to 55	4 to 15	Low	0.6 to 2	Mod.	High
46 - 75	Sandy clay, sandy clay loam	SC, SM-SC, Cl, CL-ML A-4, A-6, A-7-6	36 to 72	4 to 23	Low	<0.06 to 2	Mod.	High

Depth	Type Classification		%	Plasticity	Shrink- Swell	Coef. of Perm.	Risk of Corrosion	
(ln)			Fines	Index	Potential	(ln/Hr)	Steel	Concrete
0 - 58	Sand	SP-SM, SM A-3, A-2-4	5 to 20	Nonplasti c	Low	6 to 20	Low	Moderate
58-64	Loamy Sand	SM A-2-4	15 to 22	Nonplasti c	Low	2 to 6	Low	Moderate
64 - 89	Sandy loam, sandy clay loam	SM, SM-SC, SC A-2-4, A-4	18 to 40	NP to 10	Low	0.06 to 2	Low	Moderate

Table 3 - Engineering Index Properties of Millhopper sand Soils

Table 4 - Engineering Index Properties of Blichton sand Soils

Depth	Type C	Classification	%	Plasticity	Shrink- Swell	Permeabi lity	Risk of Corrosion	
(.ln)			Fines	Index	Potential	(In/Hr)	Steel	Concrete
0 - 28	Sand	SP-SM, SM A-2-4, A-3	8 to 25	Nonplasti c	Low	6 to 2	High	High
28- 62	Sandy clay loam	SC A-6	36 to 45	15 to 24	Low	0.06 to 0.6	High	High
62 - 80	Sandy clay loam, Sandy clay	SC A-2, A-6, A-7	30 to 50	11 to 24	Low	0.06 to 0.6	High	High

3.3 Regional Geology

The general geology of Alachua County is characterized by 30 to 50 feet of undifferentiated fine to medium grained sands and clayey sands of Holocene age (the last 10,000 years) overlying the Miocene age (circa 10 million years old) Hawthorn Formation.

The Hawthorn is approximately 100 feet thick and is comprised of interbedded layers of clay, clayey sand, sandy clay and phosphate carbonates. The underlying Tertiary age (circa 50 million years old) carbonates gently dip east under an increasing thickness of younger sediments. The general area of the proposed project parcel is characterized with unconsolidated and undifferentiated quartz sands near the surface, and karst (sinkhole) features such as collapse depressions, sinkholes, disappearing streams, springs, and mapped underground caves.

3.4 Topography

The natural topography of the proposed project parcel is best described as hilly. Current ground surface elevations in the southern one-third portion of the subject parcel range from about +140 feet MSL (southwest end) to about +110 feet MSL (northeast end), with a fairly uniform downward slope to the north and northeast.

Current ground surface elevations in the central one-third portion of the subject parcel range from about +122 feet MSL (southwest end) to about +92 feet MSL (northeast end), with a fairly uniform downward slope to the north-northeast.

Current ground surface elevations in the northern one-third portion of the subject parcel range from about +97 feet MSL (southwest end) to about +79 feet MSL (north end), with a fairly uniform downward slope to the north.

4.0 OBJECTIVE AND SCOPE OF SERVICES

4.1 Objective

The objectives of this geotechnical exploration were:

- to explore and evaluate the subsurface conditions at the subject site with special attention to potential geotechnical considerations that may impact the proposed design, construction, or serviceability of the proposed site improvements, and
- to provide geotechnical engineering recommendations for site preparation procedures, pavement and foundation design parameters, stormwater retention areas, gas station, and other pertinent geotechnical project concerns.
- Provide estimates for the high season ground water elevation.

This Report presents an evaluation of site conditions on the basis of traditional geotechnical procedures for site characterization. The recovered samples were not examined, either visually or analytically, for chemical composition or environmental hazards. UES previously performed a Phase I Environmental Assessment of the subject site and issued that report under a separate cover.

Our geotechnical exploration as presented in this Report was confined to the zone of soil likely to be stressed by the proposed construction after accounting for the significant cuts that will be performed to develop the site. Our work as summarized in this Report did not address the potential for surface expression of deep geological conditions, such as sinkhole development related to karst activity.

The proposed project parcel is located within a region in Florida that is characterized by karst topography, where the surface of the land has been shaped by faulting, fracturing and dissolution within the underlaying limestone bedrock. Karst related project parcel issues are addressed under separate cover.

4.2 Scope of Services

The preliminary services conducted by UES during the initial subsurface exploration program are documented on the Interim Report of Preliminary Geotechnical Exploration dated October 20, 2004, and the Report of Preliminary Geotechnical Consulting Services dated October 28, 2004, and are summarized as follows:

- Drilling of three (3) standard penetration test (SPT) borings in the area of the proposed Wal★Mart building footprint to maximum depths of 50 feet below the existing land surface.
- Drilling of four (4) standard penetration test (SPT) borings in the area of the proposed stormwater retention facility to depths of 40 feet below the existing land surface.
- Securing samples of representative soils encountered in the soil borings for examination, laboratory analysis and classification by members of UES geotechnical staff.
- Measuring the existing site groundwater levels at the boring locations and providing estimates of the wet season groundwater levels.
- Conducting laboratory tests on selected soil samples obtained in the field to evaluate their engineering properties.
- Assessing the existing soil conditions with respect to the proposed construction.
- Preparing Preliminary Reports which document the results of the preliminary subsurface exploration, discussions and engineering recommendations

The additional services conducted by UES during our recent subsurface exploration program are as follows:

- Drilling of seventeen (17) standard penetration test (SPT) soil borings in the area of the proposed Wal★Mart building footprint to maximum depths of 60 feet below the existing land surface.
- Drilling of four (4) standard penetration test (SPT) soil borings within the area of the proposed gasoline station to depths of 30 feet below the existing land surface.
- Drilling of thirty-seven (37) standard penetration test (SPT) soil borings within the area of the proposed stormwater retention facility to depths of 40 feet below the existing land surface.
- Drilling of eighty-three (83) standard penetration test (SPT) soil borings within the proposed parking lot and driveway areas to maximum depths of 25 feet below the existing land surface.
- Securing samples of representative soils encountered in the soil borings for examination, laboratory analysis and classification by members of UES geotechnical staff.
- Measuring the existing site groundwater levels at the boring locations and providing an estimate of the wet season groundwater levels.
- Conducting laboratory tests on selected soil samples obtained in the field to evaluate their engineering properties.
- Assessing the existing soil conditions with respect to the proposed construction.
- Preparing a Report which documents the results of our subsurface exploration and analysis with geotechnical engineering recommendations.

The site and planned construction are not located in a jurisdiction governed by International Building Code (IBC), and therefore the 100-foot deep test boring and IBC site classification were not performed as part of the subsurface exploration programs.

4.3 Limitations

This report is hereby certified to Wal-Mart Stores, Inc. and CPH Engineers, Inc. and its affiliates, successors and assigns. Accordingly, Wal-Mart has a right to rely on this report and all of the contents therein as though it were issued to Wal-Mart directly. This Report should aid the Architect/Engineer in the design of the proposed Wal★Mart SuperCenter Store No. 3873-00.

The scope is limited to the specific project and locations described herein. Our description of the project's design parameters represents our understanding of the significant aspects relevant to soil and foundation characteristics. In the event that any changes in the design or location or elevation of the structures as outlined in this Report are planned, we should be informed so the changes can be reviewed and the conclusions of this Report modified, if required, and approved in writing by Universal Engineering Sciences.

The recommendations submitted in this Report are based upon the data obtained from the soil borings performed at the locations indicated on the Boring Location Plan and from other information as referenced. This Report does not reflect any variations which may occur between the boring locations. The nature and extent of such variations may not become evident until the course of construction. If variations become evident, it will then be necessary for a re-evaluation of the recommendations of this Report after performing on-site observations during the construction period and noting the characteristics of the variations.

All users of this Report are cautioned that there was no requirement for UES to attempt to locate any man-made buried objects or identify any other potentially hazardous conditions that may exist at the site during the course of this exploration. Therefore, no attempt was made by UES to locate or identify such concerns. UES cannot be responsible for any buried man-made objects or subsurface hazards which may be subsequently encountered during construction that are not discussed within the text of this Report.

For a further description of the scope and limitations of this Report please review the document attached within Appendix G "Important Information About Your Geotechnical Engineering Report" prepared by the Association of Engineering Firms Practicing in the Geosciences.

5.0 FIELD EXPLORATION

5.1 General

The boring locations were field staked by UES and CPH engineering personnel. The approximate locations of the soil test borings are shown on the Boring Location Plans presented in Appendices B and C. Elevations of the existing ground surface adjacent to the boring locations were provided to our office and are shown on the individual Borings Logs included in the Appendices of this Report.

5.2 Standard Penetration Test Borings

As previously described in Section 4.0 above, and as shown on the Boring Location Plans in Appendices B and C, standard penetration test borings were advanced to maximum depths of 60 feet within the proposed building footprint, 30 feet within the proposed gas station area, 40 feet within the proposed stormwater retention pond area, and maximum of 25 feet within the proposed parking lot areas.

The standard penetration test borings were performed in general accordance with the procedures outlined in ASTM D-1586 (Standard Method for Penetration Test and Split-Barrel Sampling of Soils). In addition, continuous sampling was performed within the upper 10 feet of the subsurface profile at each soil test boring location.

The standard penetration test method involves driving a standard split-barrel sampler into the soil by dropping a 140-pound hammer, free falling 30 inches. The number of blows required to drive the sampler 1 foot, after an initial seating of 6 inches, is designated the standard penetration resistance, or N-value, an index to soil strength and consistency. This method is described on the Field Exploration Procedures included in the Appendices of this Report.

Recovered soil samples will be kept in our Gainesville facility and will be available for inspection for a period of 6 months in accordance with Wal \star Mart requirements. At the end of 6 months we will discard these samples, unless we are instructed otherwise.

6.0 LABORATORY SOIL TESTING

Soil samples recovered from the soil test borings were returned to our Gainesville laboratory where an experienced Geotechnical Engineer visually examined and classified the samples, and reviewed the field stratifications. The soil samples were visually examined and classified in general accordance with the guidelines of ASTM D-2487 Standard Classification of Soils for Engineering Purposes (Unified Soil Classification System). Representative soil samples were then selected for testing in our laboratory. In all we performed the following tests:

- Fifty-seven (57) percent fines content determinations ASTM Procedure D 1140, Amount of Material in Soils Finer than the #200 Sieve.
- Thirteen (13) Atterberg Limits tests ASTM Procedure D 4318, Standard Test Methods for Liquid Limit, Plastic Limit, and Plasticity Index of Soils.
- Fifteen (15) Permeability tests ASTM D-5084, Standard Test Methods for Measurement of Hydraulic Conductivity of Saturated Porous Materials Using a Flexible Wall Permeameter.
- Four (4) Corrosion Series (pH) tests FM5 -550 and FM5 -551.

Laboratory soil tests were performed to aid the Geotechnical Engineer with the soil descriptions, and to help evaluate the general engineering characteristics of the site soils. The laboratory data is presented on the Boring Logs at the approximate test sample depths, and is summarized in tabular format in Appendices E and F attached to this Report. The corrosion series tests and laboratory test procedures are also summarized in the Appendices. The quantity, and type of laboratory tests performed for the geotechnical exploration were determined and adjusted by UES based on the uniformity of the subsurface soil conditions encountered, and our experience and knowledge of local soil conditions.

7.0 SOIL STRATIGRAPHY

7.1 Generalized Subsurface Soil Profile

The results of our field exploration and laboratory analysis, together with pertinent information obtained from the standard penetration test borings, including penetration resistance values and stabilized groundwater levels, are shown on the Boring Logs included in Appendices B and C. The Key to Boring Logs is also included in the same Appendices.

The generalized subsurface soil profiles were prepared after the recovered soil samples were examined by our Geotechnical Engineer. Soil strata lines shown on the Boring Logs represent the approximate boundaries between soil types, and may not depict exact subsurface soil conditions. The actual soil boundaries may be more transitional than those depicted. Generalized subsurface soil profiles representing the soil conditions encountered at the soil test boring locations are presented in Appendix D.

7.2 Building Footprint

Twenty soil test borings were performed within the proposed building footprint. The standard penetration test (ASTM D-1586) was used to evaluate in-place relative density and collect soil samples. The soil test borings were advanced to maximum depths of 60 feet below ground surface, and the boreholes were grouted upon work completion.

The soil test borings encountered slightly clayey to very clayey sands (SM to SC) and sandy clays to clays (CL to CH) in the upper 27 to 57 feet of the subsurface profile. The sands are characterized with very loose to dense in-place relative densities. The clays are characterized with soft to very stiff in-place consistencies.

More specifically, a sand profile was encountered from ground surface to depths of 4 to 19 feet below the existing site grades. The upper 1 to 4 feet, with an average of about 2 feet, of the subsurface profile are primarily represented by relatively clean (percent fines of 10 or less) sands, and these are underlain by clayey to very clayey sands with thicknesses varying from 3 to 17 feet with an average of about 6 feet.

Underlaying the upper sands all the soil test borings encountered a sometimes sandy clay layer. The clay layer varied in thickness from 6 to 41 feet, with an average layer thickness of about 17 feet. The clay zone was then found to be underlain by a clayey to slightly clayey sand varying in thickness from about 8 to 25 feet, with an average layer thickness of about 17 feet.

The top of the limestone stratum was encountered in 16 out of 20 soil test boring locations at depths ranging from about 27 to 57 feet below ground surface, and with an average of about 39 feet. The limestone was generally encountered continuous to the boring termination depths, and can be characterized as moderately to well cemented. Organic soils were not encountered in these soil test borings.

The groundwater level was only apparent in one of the soil test borings and was measured at a depth of 20 feet below ground surface upon soil test boring work completion. Some of the boreholes were noted to have air releasing upward from the borehole once the limestone zone was approached or penetrated; this is indicative of a very porous rock matrix (perhaps cavernous) with significant confined, pressurized groundwater flow conditions.

7.3 Parking Lot

Eighty-three soil test borings were performed within the proposed at-grade parking and driveway project areas. The standard penetration test (ASTM D-1586) was used to evaluate in-place relative density and collect soil samples. The soil test borings were advanced to maximum depths of 25 feet below ground surface, and the boreholes were grouted upon work completion.

Generally a sand profile, grading with increasing depth from relatively clean at ground surface to clayey to very clayey, was encountered overlying a sometimes sandy clay zone. In 45, or about 54%, of the borings the relatively clean surficial sand zone was found from ground surface with a layer thickness range of 1 to 8 feet, and with an average layer thickness of 2 feet.

In 82 out of 83 borings, the surficial sands were directly underlain by 3 to over 20 feet of clayey to very clayey sands. These clayey sands were sometimes encountered from ground surface, and were measured with an average layer depth of about 9 feet.

In 70, or about 84% of the soil test borings a sometimes sandy clay zone was encountered with a layer thickness range of 1 to 20 feet, and with an average layer thickness of approximately 8 feet. In one soil test boring the clay layer was encountered from ground surface.

Beneath the clay zone, a clayey to slightly clayey sand zone was encountered in 33, or about 40%, of the soil test borings with a thickness range of 1 to 12 feet, and with an average thickness of about 5 feet. Neither the limestone stratum nor organic soil layers were encountered in these soil test borings.

The groundwater level was only apparent in 11 out of 83 of the soil test borings and was measured at a depths varying from about 3 to 23 feet below ground surface upon soil test boring work completion.

7.4 Stormwater Retention Pond

Forty-one soil test borings were performed within the proposed stormwater retention pond area. The standard penetration test (ASTM D-1586) was used to advance the borings and collect soil samples. The soil test borings were advanced to maximum depths of 40 feet below ground surface, and the boreholes were grouted upon work completion.

The soil test borings generally encountered a sand profile which varies from relatively clean (percent fines less than 10 or so) sand (SP), to slightly clayey to clayey sand (SM to SC). Laterally discontinuous sandy clay seams were encountered at various depths and with various thicknesses in the upper 40 feet of the subsurface profile in this portion of the site. The sandy profile is generally characterized with very loose to medium in-place relative densities.

More specifically, the sand profile was encountered from ground surface to the boring termination depths, except where the top of the limestone stratum was encountered in the soil test borings. A total of 37 soil test borings were performed in this general area of the project parcel. In 35, or about 95% of those boring sites a relatively clean to slightly clayey sand layer was encountered from ground surface with a layer thickness range of 1 to 22 feet, and with an average layer thickness of approximately 6 feet.

Beneath the surficial sands, a clayey to slightly clayey sand zone was encountered with a thickness range of 6 to 40 feet, and with an average thickness of about 24 feet. This sand zone is characterized with laterally discontinuous clay lenses or seams found at various depths in the subsurface profile. The clay seams were found in 14, or about 38%, of the borings with thicknesses varying from 2 to 20 feet and average of about 7 feet.

The top of the limestone stratum was encountered in 23 out of 41 soil test boring locations at depths ranging from about 18 to 39 feet below ground surface, and with an average of about 28 feet. Organic soils were not encountered in these soil test borings. Groundwater levels were not apparent in any of the stormwater retention pond boreholes during the exploration work.

7.5 Sinkhole Potential

The proposed project parcel is located within a region in Florida that is characterized by karst topography, where the surface of the land has been shaped by faulting, fracturing and dissolution within the underlying limestone bedrock.

The Mill Creel Sink Property consist of 8.8 acres of land lying on the north side of U.S. 441. Mill Creek Sink (previously known as the Alachua Sink) is located behind Sonny's BBQ on U.S. 441 east of I-75 and directly to the north of the proposed parcel. The Mill Creek Sink Property does not include any land on the high ground west of the sinkhole. The property is managed for diving, research, and education purposes.

The surface stream, Mill Creek and Townsend Branch, drains over 70 square miles north of Mill Creek Sink and is dissected by over ten sinkholes. Mill Creek goes completely underground north of the proposed project parcel. Mill Creek Sink is the only known window (or sinkhole) that allows access to the mapped underwater cave system. This general area has been documented with small short caves, solution pipes, and water-filled limestone sinkholes. A review of the United States Department of the Interior Geological Survey, High Springs Quadrangle sheet reveals the existence of a series of water filled sinkholes directly to the south and southwest of the proposed project parcel.

Based on current technology, there is no consistent method to predict sinkhole activity or to positively identify incipient sinkholes. Since the prediction is uncertain, the exploration programs attempt to locate and identify subsurface discontinuities, abnormalities, and other features in the bedrock and overlying sediments, as well as terrain, topographic, geologic, and hydrological research. Knowledge of the general geology of the area, coupled with geophysical techniques, physical site and structural features, and direct subsurface exploration, generally in the form of soil test borings, can provide a basis for assessment of "sinkhole activity". Karst related issues at the subject parcel are addressed in greater detail under separate cover.

7.6 Soil Corrosion Characteristics

According to the guidelines of the Florida Department of Transportation (FDOT) "Florida-Concrete Design, Environmental Classification and Construction Criteria" the results of the pH indicate the upper 15 feet of the subsurface soil profile may have a soil corrosion classification of "Extremely Aggressive" to steel and concrete (based on the three tier scale of slightly, moderately and extremely aggressive). The subsurface soil profile at depths of 20 feet and deeper may have a soil corrosion classification of "Moderately Aggressive" to steel and concrete.

The results of these tests are listed on the Report of Corrosion Parameters sheet enclosed with the laboratory test results in Appendix F.

Based on our review of the test results and past experience with similar soils, we recommend the use of Class IV concrete to counter the moderately aggressive corrosion potential. Further, adequate concrete cover must be provided for concrete substructures and protective galvanized coating is recommended for steel utility lines which extend below the seasonal high groundwater level. Accelerated corrosion conditions typically occur when below grade structures are in prolonged contact with groundwater, allowing the contact of corrosive compounds to the concrete and reinforcing steel.

8.0 GROUNDWATER CONDITIONS

8.1 Existing Groundwater Levels

Water levels were measured in some of the boreholes upon soil boring work completion, and it should be noted that the measurements may not reflect fully stabilized groundwater levels. The groundwater levels are shown on the attached Boring Logs. At the time the recent field exploration was conducted (January thru February 2005), the groundwater levels in the borings ranged from depths of about 3 feet 23 feet below existing grades. The variation of groundwater levels is attributed to topographic variations across the site, localized perched groundwater conditions, and insufficient time for stabilization in boreholes due to the presence of cohesive soils in the profiles.

Fluctuations in groundwater levels should be anticipated throughout the year, primarily due to seasonal variations in rainfall, surface runoff, construction activity, and other site specific factors that may vary from the time the borings were conducted.

The potentiometric surface map of the upper Floridan aquifer suggests groundwater elevations, outside perched zones, might be expected to be on the order of +40 feet NGVD in the general site area, which corresponds to depths of 40 to 100 feet below current ground surface elevations.

8.2 Typical Wet Season Groundwater Levels

The typical wet season groundwater level is defined as the highest groundwater level sustained for a period of 2 to 4 weeks during the "wet" season of the year, for existing site conditions, in a year with average normal rainfall amounts. Based on historical data, the rainy season in North Central Florida is normally between June and September and December and February. To estimate the wet season water level at the boring locations, many factors are considered, including the following:

- a. Measured groundwater level
- b. Drainage characteristics of existing soil types
- c. Season of the year (wet/dry season)
- d. Current & historical rainfall data (recent and year-to-date)
- e. Natural relief points (such as lakes, rivers, swamp areas, etc.)
- f. Man-made drainage systems (ditches, canals, etc.)
- g. Distances to relief points and man-made drainage systems
- h. On-site types of vegetation
- i. Area topography (ground surface elevations)
- j. Available Published Data

Based on site-specific information and factors listed above, we estimate that the pre-development wet season groundwater levels could range from approximately the existing ground levels to 6 feet below the existing site grades. Seasonal high groundwater levels will reflect transient perched groundwater conditions following periods of rainfall activity.

It should be noted that peak stage elevations immediately following various intense storm events, may be somewhat higher than the estimated typical wet season levels. Further, it should be understood that changes in the surface hydrology and subsurface drainage could have significant effects on the normal and seasonal high groundwater levels.

9.0 EVALUATION AND RECOMMENDATIONS

Our geotechnical engineering evaluation of the site and subsurface conditions with respect to the proposed construction, and our recommendations for site preparation and foundation design are based on (1) our site observations, (2) the collected field and laboratory data, and (3) our understanding of the project information and structural conditions as presented in this Report.

If the structural conditions or other project information is incorrect, please contact us so that we can review our recommendations. Also, the discovery of any site or subsurface conditions during construction which deviate from the data obtained during this geotechnical exploration should also be reported to us for further evaluation.

The recommendations presented in the subsequent sections of this Report present design and construction techniques which we consider appropriate for the planned construction. As part of the overall geotechnical contract, we recommend that UES be provided the opportunity to review the foundation plans and earthwork specifications to verify that our recommendations have been properly interpreted and incorporated into the design documents.

9.1 Foundation Design Recommendations

Based on the results of our exploration, we believe the subsurface conditions at the Wal \star Mart Supercenter site are suitable for support of the proposed structure on a properly designed and constructed conventional shallow foundation system. Provided the site preparation and earthwork construction recommendations presented herein are implemented, the following parameters may be used for foundation design. The goal of the building pad earthwork shall be to create a uniformly compacted subgrade of non-expansive soil to a depth of at least 4 feet *below the prevailing base of foundation elevation*.

9.1.1 Bearing Pressure

The maximum allowable soil bearing pressure for use in shallow foundation design should not exceed 2,500 psf. The foundations should be designed based on the maximum load which could be imposed by all loading conditions.

9.1.2 Foundation Size

The minimum width recommended for any isolated column or continuous wall footing is 24 and 18 inches, respectively. Even though the maximum allowable soil bearing pressure may not be fully achieved, this width recommendation should control the minimum size of the foundations.

9.1.3 Bearing Depth

The exterior foundations should bear at a depth of at least 18 inches below the finished exterior grades, and the interior foundations should bear at a depth of at least 18 inches below the finished floor elevation to provide confinement of the bearing level soils. We recommend stormwater and surface water run-off be diverted away from the building exterior, both during and after construction, to reduce the possibility of erosion beneath the exterior footings.

9.1.4 Bearing Material

The foundations and floor slabs may bear on either the compacted suitable natural sandy soils or compacted structural fill soils. The bearing level soils, after compaction, should be densified to at least 95 percent of the Modified Proctor maximum dry density (ASTM D 1557) to a depth of at least two feet below the base of the foundations. The bearing soils must also be firm and unyielding and should not "pump" under the action of the compaction equipment.

9.1.5 Settlement Estimates

Post-construction settlements of the structure will be influenced by several interrelated factors, such as (1) subsurface stratification and strength/compressibility characteristics of the bearing soils, (2) footing size, bearing level, applied loads, and resulting bearing pressures beneath the foundations, and (3) site preparation and earthwork construction techniques used by the contractor.

Our settlement estimates for the structure are based on the successful implementation of the site preparation/earthwork construction techniques recommended in this Report. Any deviation from these recommendations could result in an increase in the estimated post-construction settlements of the structure.

Using the recommended maximum bearing pressure, the indicated maximum structural loads, and the field and laboratory test data which we have correlated to geotechnical strength and compressibility characteristics of the subsurface soils, we estimate total settlements of the structure to be on the order of 3/4 inch. Without appropriate geotechnical site preparation procedures, total settlements could exceed our estimate. We expect a significant portion of the settlement to occur coincidental with, or shortly after, cut operations, fill placement, compaction operations and building dead load application.

Differential settlements result from differences in applied bearing pressures and variations in the compressibility characteristics of the subsurface soils. We anticipate differential settlements on the order of ½ inch or less for properly constructed building pads and shallow foundations. Differential settlements should be anticipated to occur over a lateral distance of 50 feet.

9.1.6 Ground Floor Slab

We understand that the proposed new free-standing Wal \star Mart structure will utilize an exposedconcrete floor slab throughout the building footprint. The floor slab can be constructed as a slab-ongrade provided unsuitable material is removed and replaced with compacted clean structural fill with less than 10 percent fines. The floor slab can be designed using a subgrade reaction modulus of 150 pounds per cubic inch for well compacted fill soil.

The Wal \star Mart geotechnical requirements prefer the use of a capillary break consisting of freedraining crushed aggregate. The specifications further allow the use of a plastic vapor barrier if justified by severe site conditions or if required by the local building code.

In addressing the requirements outlined in the Wal Mart "Geotechnical Investigation Specifications and Report Requirement", the Florida Building Code (Revised 2003) requires the use of vapor barriers beneath floor slabs. Typically, polyethylene plastic sheets are used in Florida to reduce floor dampness and minimize moisture emissions through floor slabs. In conformance with the Florida Building Code, we recommend the use of a vapor barrier beneath the floor slab.

The vapor barrier should consist of a plastic sheet or membrane (10 MIL polyethylene) and care should be exercised during construction to prevent tearing or puncturing of the sheet prior to slab placement. The vapor barrier should be placed directly under the slab and underlain by 6 inches of compacted aggregate material to provide a permeable absorptive base beneath the slab.

The latest Wal \bigstar Mart geotechnical requirements for exposed floor slabs specify 2 inches of fine aggregate and 4 inches of coarse aggregate with specified gradation requirements. Based on the choices offered, we recommend the fine aggregate meet the gradation requirements of ASTM D-448, #10 with 6 to 12% material passing the #200 sieve and the coarse aggregate meet the requirements of ASTM D-448, #67.

9.1.7 Retaining Walls and Tire Lube Express (TLE) Service Pit

9.1.7.1 Cast-In-Place Walls

Assuming the retaining walls and the subsurface walls in the tire lube express (TLE) service pit will be smooth concrete, we recommend using the following parameters for the upper 3 to 5 feet of insitu sands and/or on-site and imported free draining sand backfill soil compacted to 95 percent of the Modified Proctor test maximum dry density for your retaining wall design.

Rigid or unmoving structures should be designed to resist soil pressures developed in the "at-rest" condition. Where retaining structure are allowed to rotate or translate, the "active" and "passive" soil pressure conditions apply. The Table 5 values do not include a factor of safety and therefore, the designer should incorporate an appropriate factor of safety.

It should be noted that uplift and lateral hydrostatic pressures could be exerted on the structure during the time the groundwater level behind the walls is at peak levels due to natural or maninduced causes. We recommend that the hydrostatic effects of groundwater be considered as a part of the lateral earth pressure diagram. The hydrostatic pressures can result in net "uplift" conditions requiring the use of ballast or other anchorage to prevent displacement of the buried structures.

Retaining walls and subsurface walls should be provided with appropriate wall drains/underdrains to prevent water from accumulating and exerting excessive hydrostatic pressures. Also, retaining walls with adjacent sloping earth embankments or structural loadings may require special considerations.

TABLE 5 Lateral Earth Pressure Design Parameters (Level Backfill)					
Design Parameter Recommended Value					
At-rest Earth Pressure Coefficient, K_o	0.50				
* Minimum Equivalent Fluid Pressure, pcf	120				
Active Earth Pressure Coefficient, K _a	0.33				
Passive Earth Pressure Coefficient, K _p	3.0				
Saturated Unit Weight of Soil , pcf	120				
Submerged Unit Weight of Soil, pcf	50				
Coefficient of Friction (sliding)	0.4				
Angle of Internal Friction, φ	30 degrees				

* Includes Hydrostatic Force

The above parameters apply to the surficial sandy soils or imported sand backfill with less than 5 percent soil fines, extending a minimum of 5 feet behind the retaining structure or equal to the wall height (whichever is greater). Variations of these values may occur within deeper site soils and other soil types imported for backfill purposes.

The equivalent fluid pressure noted above includes the hydrostatic pressure associated with the rise in the groundwater level due to seasonal high conditions; an estimated seasonal high groundwater table of 2.5 feet below existing grade in the general location of the TLE pit. Other factors, such as surcharge loads imposed by equipment, internal structures or vehicular traffic, may significantly increase lateral earth pressures. The equivalent fluid pressure recommended above does not include the effects of any surcharge loads.

9.1.7.2 Mechanically Stabilized Earth (MSE) Walls

If proprietary MSE walls are used in this project they should be backfilled in accordance with the manufacturer's recommendations. In the absence of specific requirements from the manufacturer or in the interest of local availability of materials, we recommend that the MSE backfill soils meet the requirements of Section 145 (Subsection 145-3.2) of the current FDOT "Standard Specifications for Road and Bridge Construction".

9.1.8 Excavation Recommendations

Excavations should be sloped as necessary to prevent slope failure and to allow backfilling. Based upon the soil types and conditions encountered during our subsurface investigation we recommend that all excavations less than 20 feet in depth follow OSHA regulations (Standards - 29 CFR) for maximum allowable slopes as summarized in Table 6.

Where lateral confinement will not permit slopes to be laid back, the excavation should be shored in accordance with OSHA requirements. During excavation, excavated material should not be stockpiled at the top of the slope within a horizontal distance equal to the excavation depth. Provisions for maintaining workman safety within excavations is the sole responsibility of the contractor.

Soil or Rock Type	Typical Depth of Subsurface Profile	Maximum Allowable Slopes (H:V) (1) for Excavations Less Than 20 Feet Deep (3)
Stable Rock	35 to 50 feet	Vertical (90 Deg.)
Type A (2)	32 to 35 feet	3/4:1 (53 Deg.)
Туре В	6 to 32 feet	1:1 (45 Deg.)
Туре С	0 to 6 feet	1-1/2:1 (34 Deg.)

TABLE 6 - OSHA MAXIMUM ALLOWABLE SLOPES

Footnote (1): Numbers shown in parentheses next to maximum allowable slopes are angles expressed in degrees from the horizontal. Angles have been rounded off.

Footnote (2): A short-term maximum allowable slope of 1/2:1 H:V (63 degrees) is allowable in excavations in Type A soil that are 12 feet (3.67 m) or less in depth. Short-term maximum allowable slopes for excavations greater than 12 feet (3.67 m) in depth shall be 3/4:1 H:V (53 degrees)

Footnote (3): Sloping or benching for excavations greater than 20 feet deep shall be designed by a registered professional engineer per OSHA design regulations.

9.1.9 Seismic Considerations

Universal Engineering Sciences reviewed the Standard Building Code (Section 1607) in regard to seismic considerations for the site. Per Figures 1607.1.5A and B, all of Florida falls below coefficient values of 0.05 g for both peak ground acceleration and peak velocity-related acceleration. Accordingly, the liquefaction potential of this site due to earthquake forces is negligible.

Per Table 1607.1.6, a typical Wal★Mart facility could be considered a Group II Seismic Hazard Exposure, due to potential occupancy of over 250. Based on the above, the Seismic Performance category for the structure is A per Table 1607.1.8.

Based on the soil stratigraphy disclosed by the soil borings performed, review of the published site geologic data, and per Table 1607.3.1, this property is assigned a Site Coefficient equal to 1.0.

9.2 Pavement Recommendations

9.2.1 General

Either rigid or flexible pavement sections may be used on this project. Flexible pavement combines the strength and durability of several layer components to produce an appropriate and cost-effective combination of available construction materials. Concrete pavement has the advantage of the ability to "bridge" over isolated soft areas, it requires less security lighting, and it typically has a longer service life than asphalt pavement. Disadvantages of rigid pavement include an initial higher cost and more difficult patching of distressed areas than occurs with flexible pavement.

Referencing the "Geotechnical Investigation Specifications and Report Requirements" as provided by Wal★Mart, the Minimum Pavement Surface Thickness is specified as follows:

A. Standard Duty Asphalt - 3 inches Concrete - 5 inches

B. Heavy Duty
 Asphalt - 4 inches
 Concrete - 6 inches

Within the following tables, we have provided our recommendations for pavement design based on the above minimum values and FDOT Pavement Design Guidelines (which are based on AASHTO methodology). We note however, that the recommended flexible pavement sections are generally thicker than those typically specified for similar traffic loading conditions. Certainly, no detriment will be realized in constructing the pavements with the thicker sections; however, we can provide alternative pavement recommendations based upon local experience with similar pavement conditions to those proposed and upon Florida Department of Transportation guidelines that will produce acceptable, durable pavements at a cost savings.

9.2.2 Asphalt (Flexible) Pavements

Standard duty pavement areas are defined as having car and pickup truck loading conditions. Heavy duty areas are defined as having delivery, storage, and garbage truck loading conditions along with service drives. Assuming:

- 1. The 12" of subgrade soils below the base course are compacted to 98 percent of Modified Proctor test maximum dry density (ASTM D 1557) with a design LBR value of 40 (after stabilization),
- 2. A 20-year design life,
- 3. Terminal serviceability index (P₀) of 2,
- 4. Reliability of 85 percent, standard deviation of 0.45, and total equivalent 18-kip single axle loads (E_{18} SAL) of 109,500,
- 5. An asphalt section that consists of two layers, a structural course and a separate wearing surface.

We recommend the design shown in the following Table 7 for a standard duty asphalt pavement.

	TABLE 7 STANDARD DUTY ASPHALT/LIMEROCK PAVEMENT						
Pav	ement Layer	Thickness	Minimum Requirements				
Asphalt Wearing Surface	Type S-III (max 25% recycle)	1"	96% Laboratory Marshall Density, Mix				
Asphalt Structural Course	Type S-I (max 50% recycle)	2"	to be approved by Universal.				
Limerock		6 inch minimum	98% Modified Proctor test maximum dry density, Limerock Bearing Ratio (LBR) of at least 100.				
Stabilized Subgrade		6 inch minimum	98% Modified Proctor test maximum dry density, Limerock Bearing Ratio (LBR) of 40.				

Our recommendations for a heavy duty flexible asphalt pavement for total equivalent 18-kip single axle loads (E_{18} SAL) of 335,800 are shown in Table 8 below.

	TABLE 8 HEAVY DUTY ASPHALT/LIMEROCK PAVEMENT						
Pave	ment Layer	Thickness	Minimum Requirements				
Asphalt Wearing Surface	Type S-III (max 25% recycle)	1½ "	96% Laboratory Marshall Density, Mix				
Asphalt Structural Course	Type S-I (max 50% recycle)	21⁄2 "	to be approved by Oniversal.				
Limerock		6 inch minimum	98% Modified Proctor test maximum dry density, Limerock Bearing Ratio (LBR) of at least 100.				
Stabil	ized Subgrade	6 inch minimum	98% Modified Proctor test maximum dry density, Limerock Bearing Ratio (LBR) of 40.				

9.2.2.1 Stabilized Subgrade

We recommend that subgrade materials be compacted in place according to the requirements in the "Site Preparation" section of this report. Stabilize the subgrade materials to a minimum Limerock Bearing Ratio (LBR) of 40 percent as specified by FDOT requirements for Type B Stabilized Subgrade. The subgrade material should be compacted to at least 98 percent of the Modified Proctor maximum dry density (ASTM D 1557, AASHTO T-180) value. The 98 percent compaction requirement (as opposed to the 95 percent Wal Mart requirement) is an FDOT Standard which results in a higher subgrade resilient modulus.

The single LBR test result indicates that some of the surficial in-situ sands may not meet the LBR requirements for a stabilized subgrade material. Additional LBR testing should be performed on representative in-situ and/or imported soil samples prior to reaching a final conclusion on subgrade material suitability. The stabilized subgrade can be a blend of existing soil and imported material such as crushed limerock. If a blend is proposed, we recommend that the contractor perform a mix design to find the optimum mix proportions.

Depending upon the soil type, the subgrade material from an off-site source may have sufficient stability to provide the needed support without additional stabilizing material. Generally sands with crushed limerock have sufficient stability and do not require additional stabilizing material. UES should observe the finished subgrade conditions to evaluate whether or not additional stabilization will be required prior to base course construction.

9.2.2.2 Base Course

We recommend the base course consist of locally available crushed limerock complying with the requirements of Section 911 and Section 200 of the current FDOT Standard Specifications for Roadway and Bridge Construction. The crushed limerock materials should have a minimum LBR of 100 percent and should be mined from an FDOT approved source. The crushed limerock should be placed using maximum 6-inch lifts, and each lift should be compacted to a minimum density of 98 percent of the Modified Proctor maximum dry density.

9.2.2.3 Wearing Surface

The wearing surface should consist of FDOT Type S asphaltic concrete having a minimum Marshall Stability of 1,800 lbs and a flow range of 0.07 to 0.12 inches. Specific requirements for Type S asphaltic concrete wearing surface are outlined in the current Florida Department of Transportation, Standard Specifications for Road and Bridge Construction, 2004 Edition.

The asphaltic concrete should be placed in two layers. Specifically for regular duty areas, the lower binder course should consist of a minimum of 2 inches of FDOT Type S-1. The surface course should be a minimum of 1 inch of FDOT Type S-III. For heavy duty pavements, the binder should consist of a minimum of 2.5 inches of FDOT Type S-1 with a surface course consisting of a minimum 1.5 inches of FDOT Type S-III. The S-1 binder may contain up to 50 percent recycled asphaltic concrete while the S-III mix may contain up to 25 percent recycled asphaltic concrete.

After placement and field compaction, the wearing surface should be cored to evaluate material thickness and to perform laboratory densities. Cores should be obtained at frequencies of at least one core per 10,000 square feet of placed pavement or a minimum of two cores per day's production.

9.2.2.4 Curbing

We recommend that curbing around the landscaped sections adjacent to the parking lots and driveways be constructed with full-depth curb sections. Using extruded curb sections which lie directly on top of the final asphalt level, or eliminating the curbing entirely, can allow migration of irrigation water from the landscape areas to the interface between the asphalt and the base. This migration often causes separation of the wearing surface from the base and subsequent rippling and pavement deterioration. Topsoil placement behind curbs should be limited to 6 inches in vertical thickness within 5 feet of pavement structure. Alternatively, the landscape island could be equipped with underdrains manifolded to a common discharge point.

9.2.2.5 Landscape Areas

In the event, the landscape areas are constructed with poorly draining silty/clayey sands, we recommend that landscape drains be installed around the landscaped sections adjacent to the parking lots and driveways to protect the asphalt pavements from excess rainfall and over irrigation. Migration of irrigation water from the landscape areas to the interface between the asphalt and the base usually occurs unless landscape drains are installed. This migration often causes separation of the wearing surface from the base and subsequent rippling and pavement deterioration. The underdrains or strip drains should be routed to a positive outfall at the pavement area catch basins.

9.2.3 Concrete (Rigid) Pavements

Concrete pavement is a rigid pavement that transfers less wheel pressure to the subgrade soils than a flexible asphalt pavement. Current Wal \star Mart specifications require the use of a base course and stabilized subgrade beneath concrete pavement. Our recommendations for the pavement system are presented below:

- 1. The stabilized subgrade materials should be a minimum of 4 inches thick, be freedraining, and have a minimum LBR value of 40.
- 2. The stabilized subgrade and base materials must be densified to at least 98 percent of Modified Proctor test maximum dry density (ASTM D 1557, AASHTO T180).
- 3. The base course should be a minimum of 4 inches thick, and the base materials should be free-draining and have a minimum LBR of 100. The surface of the base course must be level and any disturbances or wheel rutting corrected prior to placement of concrete.
- 4. Concrete pavement thickness should be uniform throughout, with exception to thickened edges (curb or footing).
- 5. The bottom of the pavement should be separated from the estimated typical wet season groundwater level by at least 18 inches.
- 6. Base and stabilized subgrade courses beneath concrete pavements shall have a minimum permeability (K) greater than or equal to 0.001 cm/sec. The free-draining subgrade material should be at least 12 inches thick and sloped to positive drainage outfall so that a "trapped" water or "bathtub" condition is avoided.

Our recommendations for a standard duty concrete pavement section are based on a modulus of subgrade reaction (k) equal to 150 pounds per cubic inch for clean native sands or imported fill soils compacted to a minimum density of 98 percent of the Modified Proctor maximum dry density according to ASTM D-1557. Our recommendations also consider a 20-year design life, a standard deviation of 4.5, and total equivalent 18-kip single axle loads (E_{18} SAL) of 109,500. We recommend using the design shown in Table 9 on the following page.
STANDARD DUTY	TABLE 9 ((UNREINFORCED) CONCH	RETE PAVEMENT
Minimum Pavement Thickness	Maximum Control Joint Spacing	Minimum Sawcut Depth
5 Inches	10 Feet x 10 Feet	1¼ Inches

Our recommendations for concrete slab thickness for heavy duty concrete pavements for total equivalent 18-kip single axle loads (E_{18} SAL) of 335,800 are shown in Table 10 below.

HEAVY DUTY (TABLE 10 UNREINFORCED) CONCRE	TE PAVEMENT
Minimum Payament Thickness	Maximum Control	Minimum Sawcut Depth
6 Inches	12 Feet x 12 Feet	1½ Inches

We recommend using concrete with a minimum 28-day flexural strength (modulus of rupture) of at least 650 pounds per square inch, based on three point loading of concrete beam test samples. We recommend the rigid pavements be constructed of un-reinforced Portland cement concrete providing a minimum 28-day compressive strength of 4,000 psi; Portland cement should be Type I.

Layout of the sawcut control joints should form square panels, and the depth of sawcut joints should be at least 1/4 of the concrete slab thickness. The saw cut joints should be constructed within six hours of concrete placement, or as soon as the concrete develops sufficient strength to support workers and equipment. We recommend allowing Universal to review and comment on the final concrete pavement design, including section and joint details (type of joints, joint spacing, etc.), prior to the start of construction.

For further details on concrete pavement construction, please reference the "Guide to Jointing of Non-Reinforced Concrete Pavements" published by the Florida Concrete and Products Association, Inc., and "Building Quality Concrete Parking Areas", published by the Portland Cement Association.

9.2.4 Effects of Groundwater

One of the most critical influences on pavement performance in North Central Florida is the relationship between the pavement subgrade and the seasonal high groundwater level. Many roadways and parking areas have been damaged as a result of deterioration of the base and the base/surface course bond. We recommend that the seasonal high groundwater and the bottom of the crushed limerock base course be separated by at least 24 inches.

For concrete pavement the minimum separation may be reduced to 18 inches provided the compacted subgrade is "free-draining" material with positive outfall. The separation should be confirmed by reviewing the final site grading and paving plan. If the separation is not provided by grading and/or permanent surface drainage improvements, underdrains should be provided.

9.2.5 Construction Traffic

Regular duty roadways and incomplete pavement sections will not perform satisfactorily under construction traffic loadings. We recommend that construction traffic (construction equipment, concrete trucks, sod trucks, garbage trucks, dump trucks, etc.) be re-routed away from these roadways or that the pavement section be designed for these loadings.

9.3 Site Preparation

We recommend normal, good practice site preparation procedures. These procedures include: stripping the site of existing vegetation and top soils, proof-rolling and compacting the subgrade, cut operations to grade, and filling to grade with compacted structural fill.

Geotechnical site preparation on the subject parcel will include significant cut and fill earthwork operations. Within the proposed building footprint, cut operations are anticipated to expose clayey sand and clay subgrade soils. Over-excavation of clayey sand soils may be recommended based on their engineering characteristics and/or seasonal groundwater and seepage considerations. Over-excavation of clay soils is recommended.

It also may be recommended to place an underdrain system along the toe of major cut areas up-slope of the building pad and pavement areas to intercept lateral seasonal seepage and stormwater runoffs that could affect performance of these improvements.

Within the proposed parking lot areas, cut operations are anticipated to expose subgrade soils consisting primarily of clayey sands and clay layers. Over-excavation of such clayey sand and clay soils is recommended.

Excavations for retention pond construction are anticipated to yield primarily a mixture of relatively clean sands, slightly clayey sands, and clayey sands. The excavation work may intercept laterally discontinuous clay seams.

Suitability of the excavated soils will require further evaluation, however, as a rule the relatively clean sands should be appropriate for both structural fill and backfill purposes, where as the clayey to very clayey sands generally require more construction/compaction effort, are more sensitive to moisture content in the soil mass, and would require more attention from the Geotechnical Engineer during earthwork activities. Optimal use of the clayey sands might be found in the initial (deeper) fill lifts in both building footprint and parking lot areas. Appropriate compaction levels should be evaluated.

Due to the nature of pinnacled limestone in the area and the differential depth to limestone found in the borings conducted, limestone and in particular hard limestone could be encountered in the deeper cuts. If so, localized blasting and undercutting of the limestone below finished grades could be required to achieved a relatively uniform foundation building pad.

More specifically, we recommend the following:

- 1. Prior to construction, the location of any existing underground utility lines within the construction area should be established. Provisions should be made to relocate interfering utilities to appropriate locations. It should be noted that if underground pipes and septic systems are not properly removed or plugged, they may serve as conduits for subsurface erosion which may subsequently lead to excessive settlement of overlying structures.
- 2. The shallow groundwater level was encountered from about 3 to 23 feet below the existing site grades. Pre-development seasonal high groundwater levels are anticipated to occur in the range from the existing ground levels to 6 feet below the existing site grades. Groundwater control measures may be required during site stripping, and site cut operations. If required, shallow groundwater control can probably be achieved by pumping from sumps located in perimeter ditches or pits. All sump pumps should be located outside the bearing areas to avoid loosening of the fine sandy bearing soils. For deeper excavations where sustained, positive groundwater control is needed, a system of fully sanded vacuum well points may be required. The groundwater level should be maintained at least two feet below the bottom of any excavations during construction, and two feet below the surface of any vibratory compaction operations.
- 3. Strip the proposed construction limits of all vegetation, roots, topsoil, and other deleterious materials within and 10 feet beyond the perimeter of the proposed building and paved areas. Expect clearing and grubbing to an average depth of 6 to 12 inches in most areas. Some areas may require more than a foot of stripping or undercutting to remove the root systems of large trees. Any unsuitable material not encountered in the soil test borings should be removed during site clearing and grubbing operations.
- 4. Cut the various project areas to rough subgrade elevations. A minimum separation of 4 feet should be provided between the prevailing foundation system bearing elevations and the underlying natural clay soils. This may require undercutting to more than 6 feet below finished floor elevations in some areas of the pad. Selective undercutting should be performed under the direction of the geotechnical engineer. A minimum separation of 2 feet should be provided between the bottom of base course in pavement areas and the underlying natural clay soils.
- 5. Proof-roll the exposed subgrades with a heavily loaded, rubber-tired vehicle under the observation of a Geotechnical Engineer or his representative. Proof-rolling will help locate any zones of especially loose or soft soils not encountered in the soil test borings. Then undercut, or otherwise treat these zones as recommended by the Geotechnical Engineer.

If difficult compaction conditions are encountered during the site work operations, the compaction efforts should stop and the UES geotechnical engineer should be contacted. The Geotechnical Engineer should observe proof-rolling of the exposed subgrade to determine if additional compaction is warranted or if any material needs to be over-excavated and replaced.

6. After stripping and proof-rolling operations are completed, the exposed surface soils in the building construction area should be compacted with a vibratory drum roller having a minimum static, at-drum weight of 20 tons. We recommend no less than eight overlapping passes, in 2 perpendicular directions, be completed with the vibratory roller while it operates at its maximum vibrational frequency and a travel speed of not more than 2 mph. Typically, the material should exhibit moisture contents within ±2 percent of the Modified Proctor optimum moisture content (ASTM D 1557) during the compaction operations. Compaction should continue until densities of at least 95 percent of the Modified Proctor maximum dry density (ASTM D 1557) have been uniformly achieved within the upper 12 inches of the compacted soil surface.

Should the surface soils experience pumping and soil strength loss during the compaction operations, compaction work should be immediately terminated and (1) the disturbed soils removed and backfilled with dry structural fill soils which are then compacted, (2) the excess moisture content within the disturbed soils allowed to dissipate before recompacting or (3) the area de-watered and the soils dried.

- 7. Test the subgrade for compaction at a frequency of not less than one test per 2,500 square feet in the building area and one test per 10,000 square feet in pavement areas.
- 8. Place fill material, as required. The fill should consist of sand with less than 10 percent soil fines. Place fill uniformly with loose lift thicknesses not exceeding 12 inches, and compact each lift to a minimum density of at least 95 percent of the Modified Proctor maximum dry density. The last 12 inches of subgrade fill beneath the flexible pavement parking areas should be compacted to 98 percent of the Modified Proctor maximum dry density. Stabilize this subgrade zone with limerock as necessary to obtain a minimum LBR of 40.
- 9. Perform compliance tests within the fill at a frequency of not less than one test per 2,500 square feet per lift in the building areas. In paved areas, perform compliance tests at a frequency of not less than one test per 10,000 square feet per lift.
- 10. Test the bottom of all footing excavations for compaction to a depth of 1 foot below bearing level. We recommend testing of every column footing, and conduct one test for every 100 lineal feet of wall footing.

11. If site preparation work is performed during the rainy season, special care should be taken to maintain positive drainage from the building pad and paved areas to drains or ditches around the site. Unexpected wet periods can also occur in Florida during the "dry" season. Such events can raise water tables to levels above seasonal highs without the associated high temperatures to evaporate ponded water. Therefore, the contractor should practice wet weather means and methods for earthwork during the "dry" season as well. Groundwater and surface water control, use of granular fill material and aeration are the normal means to accommodate wet weather construction. All fill materials that are excavated from below the water table should be stockpiled for a sufficiently long period to allow drainage.

9.4 Groundwater Control

The groundwater table will fluctuate seasonally depending upon local rainfall. The rainy seasons in North Central Florida is normally between June to September and December to February. Estimates of the pre-development seasonal high groundwater levels are provided in previous sections of this report.

It should be noted that the estimated seasonal high groundwater levels do not provide any assurance that groundwater levels will not exceed these estimated levels during any given year in the future. Should impediments to surface water drainage exist on the site, or should rainfall intensity and duration, or total rainfall quantities, exceed the normally anticipated rainfall quantities, groundwater levels may exceed the seasonal high estimates. We recommend positive drainage be established and maintained on the site during construction. We further recommend permanent measures be constructed to maintain positive drainage from the site throughout the life of the project. All foundation designs, pavement designs, and stormwater retention designs should consider of the seasonal high groundwater conditions.

Due to the anticipated high groundwater conditions, temporary dewatering may be required at this site if construction proceeds during the wet season, particularly for the installation of underground utility structures and below grade structures such as truck loading docks, TLE pit, etc. We recommend that the contract documents provide for determining the depth to groundwater just prior to construction, and for any remedial dewatering which may be required. Further, we recommend that the groundwater table be maintained at least 24 inches below all earthwork and compaction surfaces during construction.

9.5 Weather Considerations

As noted in the previous section, the rainy seasons in North Central Florida normally occur between the months of June through September and December through February, with the potential for additional heavy rainfall continuing through the end of the hurricane season in November. During this period, frequent afternoon thunderstorms are likely, with short periods of intense rainfall.

The groundwater level typically rises to the estimated perched seasonal high level during the latter part of the rainy season, and earthwork extending below the perched seasonal high groundwater levels will require temporary dewatering measures. Further, the short periods of intense rainfall can saturate surface soils, leading to instability during compaction and placement.

Where the subgrade soils become saturated and unstable due to rainfall, the contractor should be prepared to windrow and aerate the subgrade soils to promote drying. In cases of extreme saturation, temporary dewatering or over-excavation and replacement of saturated soils may be required. In contrast, if construction proceeds during the drier portions of the year (December through May), additional applications of water may be required to maintain soil moisture contents in the optimum range during compaction activities. During dry periods, the contractor should be prepared with sufficient equipment (water trucks, tanker or hydrant meters) to adequately wet the subgrade soils to maintain the appropriate moisture contents.

To minimize the potential for moisture related instability during compaction of imported fill soils, we recommend that fill soils to be used on the subject site contain less than 5 percent material passing the No. 200 sieve. Materials with soil fines contents up to 10 percent or so may also be used; however, these soils may require stricter moisture control measures during stockpiling, placement, and compaction.

9.6 Stormwater Retention Pond

9.6.1 General

The subsurface conditions at the proposed stormwater management areas were evaluated in the field using standard penetration test borings. The soil profile encountered in the proposed retention pond area can be generalized as follows: 1 to 22 feet of relatively clean to slightly clayey sand layer (average layer thickness of approximately 6 feet), followed by a clayey to slightly clayey sand zone with a thickness range of 6 to 40 feet (average thickness of about 24 feet). This lower sand zone is characterized with laterally discontinuous clay lenses or seams found at various depths in the subsurface profile.

Groundwater levels were not apparent in any of the stormwater retention pond boreholes during the exploration work. The results of the field exploration programs suggest groundwater levels in the proposed stormwater retention pond area will be at depths greater than 35 feet below site grade, outside perched groundwater areas. The results of the laboratory permeability tests on the surficial sands ranged from 1 to 9 feet per day indicating moderate infiltration characteristics.

The coefficients of permeability from the laboratory test and those shown on the Soil Survey are intended to provide an indication of the soil's drainage characteristics. The actual exfiltration rate may vary due to pond geometry, retention volume, soil stratification and groundwater mounding effects.

The USDA Soil Survey of Alachua County, Florida describes the near-surface soil profile in the proposed retention pond area (north end of site) as Norfolk loamy fine sand with 2 to 8 percent slopes. Norfolk soils are characterized as sloping, well drained soils. The Norfolk loamy fine sand soils have an estimated high water table in the range of 4 to 6 feet below ground. It should be noted that the impact that the near-surface soils may have on retention pond design and performance will be directly related to the finished pond elevations.

It should be noted that estimated seasonal high groundwater levels are not a guarantee that groundwater levels will not exceed these estimated levels during any given year in the future. Should impediments or enhancements to surface water drainage exist on the site or adjacent off-site, or should rainfall intensity and duration, or total rainfall quantities, exceed the normally anticipated rainfall quantities, localized groundwater levels may exceed seasonal high estimates.

9.6.2 Groundwater Levels

As discussed in the preceding Groundwater Control section of this Report, the groundwater table can be expected to fluctuate seasonally depending upon local rainfall, with the groundwater levels rising to the normal peak near the end of the rainy season that normally occurs between June and September. Based upon our review of the soil and groundwater conditions encountered during the field investigation, Soil Survey data, and regional hydrogeology, our best estimate for the predevelopment seasonal high groundwater table at the boring locations performed in the stormwater management area is from the existing ground levels to 6 feet below the existing site grades.

It should be noted that the estimated seasonal high groundwater levels do not provide any assurance that groundwater levels will not exceed these estimated levels during any given year in the future. Should impediments or enhancements to surface water drainage exist on the site or adjacent off-site, or should rainfall intensity and duration, or total rainfall quantities, exceed the normally anticipated rainfall quantities, localized groundwater levels may exceed seasonal high estimates. We recommend positive drainage be established and maintained on the site during construction and that permanent measures be constructed to maintain positive drainage from the site throughout the life of the project. We also recommend that all stormwater retention analyses incorporate consideration of the seasonal high groundwater conditions.

Based on our local project and general site area knowledge, the anticipated pre-development wet season water table levels, and the presence of relatively shallow groundwater conditions, we recommend that a wet stormwater retention pond be considered for this project. Temporary dewatering will likely be required during the excavation of the stormwater management areas.

9.6.3 Borrow Fill Suitability

Based on the results of the subsurface exploration programs completed for the subject project, it is our professional opinion that a significant portion of the subsurface soils encountered within the proposed stormwater retention pond area would be classified as belonging to either Group "A" or Group "B" or Group "C" soils. This section explains the applicability/purpose of fill reuse of the different soil types encountered. Presented in the following paragraphs are our recommendations concerning the suitability of the soils encountered for use as structural fill.

Group "A": These soils consist of clean sands which have less than 5 percent soil fines. Group "A" soils are the most desirable for use as engineered fill because they drain freely when excavated from beneath the groundwater table, and are not as susceptible to moisture related instability.

Group "B": These soils consist of sand with silt or sand with clay which contain between 5 and 12 percent soil fines. Group "B" soils are good sources of engineered fill, but require some extra care during placement and compaction. The moisture content of these soils should not be higher than the optimum during placement and compaction in order to reduce the potential for moisture related instability. These soils drain fairly well, but may require some stockpiling and aeration time if allowed to become saturated during earthwork activities.

Group "C": These soils consist of silty and clayey sands which contain 12 to 20 percent soil fines. Group "C" soils are more difficult to use because they are more moisture sensitive. The moisture content of these soils should be maintained below the optimum moisture content in order to help mitigate the potential for moisture-related instability during placement and compaction. If these materials are successfully placed and compacted, they should be graded to shed water from the site and prevent ponding, both during and after construction. If water ponds atop these soils, previously compacted soils can become overly wet and lose stability. Caution should be used when placing these soils during the rainy season and the contractor should be prepared to aerate and dry, and/or excavate and replace these soils when moisture contents exceed the optimum levels.

Group "D": These soils consist of silty and clayey sands and clays which have greater than 20 percent soil fines. These soils are not recommended for use as engineered fill because they will be too difficult to practically dry and work. During the rainy season it is virtually impossible to obtain stable compaction of these soils.

9.6.3.1 Additional Steps for Use of Group C and D Soils

We understand that the economics of the site development tends to force contractors and developers to use soils with higher fines content such as Group C and some Group D soils for fill material. In consideration of this we offer the following discussion.

It is possible to use Groups C and D soils as fill material. However, due to the frequent rains, the high moisture content of these soils when excavated from below the water table, as these will be, unfamiliarity with these soils, and the time constraints placed on most construction projects, it is sometimes more practical to over-excavate borrow areas where more suitable soils are encountered, or use more suitable imported fill material. In order to use Group "D" and some Group "C" a prospective contractor should be prepared to incorporate the following steps:

- 1. Dewater the borrow area, prior excavation of the soils so they may be excavated in a dry manner.
- 2. Aerate the soils until they are at their optimum moisture content, as determined by laboratory testing, prior to placement and compaction.
- 3. Place and compact the soils in 6-inch thick loose lifts using <u>only</u> static compaction. A sheepsfoot or a raised pad roller can be useful for this purpose.
- 4. Work in small areas that are graded to shed water and avoid ponding. Positive drainage must be maintained both during and after construction in order to get rainwater off the compacted fill area as quickly as possible.
- 5. Disc and aerate areas that are subjected to rainfall or otherwise become wet. Do not leave these soils exposed to the elements for long periods as soils that have already been compacted may become wet and unstable. Protect the fill soil each night and before rain by mounding the soil and smooth-rolling the surface to allow water to shed off to reduce the amount of water infiltration.
- 6. Do not place lifts of Group "A" or "B" soils on top of Group "C" and "D" soils for final grade. This will provide a medium for a "perched" groundwater table to occur, which may result in pavement and/or landscape area saturation.

It is our experience that implementation of the above steps, which we are imperative for successful placement and compaction of these soils, can become difficult and expensive for site work contractors, and must be considered during the bidding process. Consequently, we recommend that the construction documents include information advising prospective site work contractors of the soils present on the site.

9.7 Sewer and Utility Lines

9.7.1 General

Sands and slightly clayey sands should be suitable for support of the planned utility lines and for reuse as backfill.

The slightly clayey sands, when excavated from below the water table, may require spreading and drying prior to reuse to achieve a moisture content sufficient to obtain the recommended degree of compaction. However, the clayey to very clayey sands and clays (SC,CL and CH) are not suitable for structural fill use, and should be removed and replaced with compacted structural fill to a depth of two feet below the invert of any conduit.

9.7.2 Trench Excavation and Backfill Recommendations

The following are our recommendations for construction of the project's buried utility lines.

- 1. If dictated by site conditions at the time of construction and/or deemed necessary by the contractor, install a dewatering system capable of maintaining the groundwater level at least 3 feet below the anticipated bottom of conduit.
- 2. After excavation to design invert elevations, the in-situ bedding soils should be compacted to at least 95 percent of the Modified Proctor test maximum dry density (ASTM D 1557) to a depth of 12 inches below the bedding level. Compaction in confined areas can probably be achieved using jumping jacks or light weight walk-behind vibratory sleds and/or rollers.
- 3. After installing the conduits, backfill with suitable sand fill placed in 4 to 6 inch loose lifts. Starting 12 inches above the top of the conduit, the lifts should be compacted to at least 95 percent of the Modified Proctor test maximum dry density (ASTM D 1557). Beneath pavement areas, the top 12 inches of backfill should be compacted to at least 98 percent.
- 4. If difficult compaction operations are encountered beneath the utilities due to excessive fines and/or wet conditions, saturated soils may be overexcavated and replaced with FDOT No. 57 stone.
- 5. Excavation work will be required to meet OSHA Excavation Standard Subpart P regulations, Type C Soils. Either a trench box, braced sheet pile structure or an excavation with temporary side slopes cut back at 1.5:1 (H:V) can be implemented. The 1.5:1 side slope is contingent upon the dewatering system adequately controlling slope seepage. Sheet piling should be designed according to OSHA sheeting and bracing requirements. We recommend a Florida registered Professional Engineer design any required sheeting/bracing system.

6. Backfill above and around thrust blocks should consist of clean fine sands (SP) compacted at least 98 percent of Modified Proctor maximum dry density (ASTM D 1557). For a design criteria, we recommend using an allowable passive earth pressure coefficient of K_p =3.0.

9.8 Additional Considerations

Based on the limited borings performed, the soil conditions encountered beneath the gasoline station lot area were similar to those found across the Wal \star Mart site. Therefore, in general, the recommendations contained in this Report should be suitable for planning, design and construction on the out parcel.

9.9 Construction Related Services

We recommend that the owner retain Universal Engineering Sciences to perform construction materials tests and observations on this project. Field tests and observations include verification of foundation and pavement subgrades by monitoring proof-rolling operations, undercutting of potential shrink/swell clays beneath building and pavement areas, and performing quality assurance tests on the placement of compacted structural fill and pavement courses. The geotechnical engineering design does not end with the advertisement of the construction documents. The design is an on-going process throughout construction. Because of our familiarity with the site conditions and the intent of the engineering design, we are most qualified to address problems that might arise during construction in a timely and cost-effective manner.

10.0 LIMITATIONS

During the early stages of most construction projects, all pertinent geotechnical issues may not be fully addressed in the geotechnical report document. Because of the natural limitations inherent in working with the subsurface, it is not possible for a geotechnical engineer to predict and address all possible problems. An Association of Engineering Firms Practicing in the Geosciences (ASFE) publication, "Important Information About Your Geotechnical Engineering Report" appears in Appendix G, and will help explain the nature of geotechnical issues.

Further, we present documents in Appendix G: Constraints and Restrictions, to bring to your attention the potential concerns and the basic limitations of a typical geotechnical report.

11.0 CLOSURE

Our interpretation of the site soil and groundwater conditions is based on our general knowledge of the area, subsurface borings performed and laboratory analysis conducted. UES did not identify any geotechnical considerations that will significantly impact the planned building or parking areas at the site, as we currently understand it, using conventional construction practices. Standard methods of surficial stripping, excavation, proof rolling, compaction and backfilling should adequately prepare the site. This Report has been prepared for the exclusive use of Wal-Mart Stores, Inc., and CPH Engineers, Inc., and their respective successors and assigns.

APPENDIX A

Site Location Map



Note: United States Geological Survey Topographic Map, Alachua, Alachua County.



UNIVERSAL ENGINEERING SCIENCES

WAL-MART STORE TRACKING No. 3873-00 S.E. CORNER OF I-75 & U.S. HIGHWAY 441 ALACHUA, ALACHUA COUNTY, FLORIDA

SITE LOCATION MAP

DRAWN BY	FAA	DATE:	3/25/05	CHECKED BY: FA	DATE: 5 19	20
SCALE:	NOT TO SCALE	ORDER NO:	70080-077-06	REPORT NO: 383573	PAGE NO:	A-1

APPENDIX B

Preliminary Study Boring Location Plan Preliminary Study Boring Logs Key to Boring Logs Field Exploration Procedures



PROJECT NO.: 70080-077-03 UNIVERSAL ENGINEERING SCIENCES REPORT NO .: 367801 **BORING LOG** PAGE: B-2 B-1 1 of 1 WAL-MART STORE TRACKING NO. 95484-00 SHEET: BORING DESIGNATION: PROJECT: S.E. CORNER OF I-75 & HIGHWAY 441 SECTION: 15/16 TOWNSHIP: 8S RANGE: 18E ALACHUA, ALACHUA COUNTY, FLORIDA CPH ENGINEERS, INC. CLIENT: GS ELEVATION(ft): +132 (MSL)DATE STARTED: 10/12/04 LOCATION: SEE BORING LOCATION PLAN WATER TABLE (ft): NE 10/12/04 DATE FINISHED: REMARKS: AIR BLOWING OUT OF BOREHOLE AT DEPTH OF 40 TO 45 DATE OF READING: N.A. DRILLED BY: R. WOODARD FEET TYPE OF SAMPLING: ASTM D-1586 EST. WSWT (ft): N.A. v ATTERBERG BLOWS Ν κ ORG. DEPTH MP L E м В О -200 MC LIMITS PER 6" (BLOWS/ W.T. DESCRIPTION (FT./ CONT. (%) (%) (FT.) INCREMENT FT.) DAY) (%) LL ΡI 0 Firm brown SANDY CLAY [CH] 1-4-5 9 Loose light brown, orange & tan CLAYEY to very 3-4-4 8 CLAYEY SAND [SC] 5 4-3-4 7 ::.loose 4-3-3 6 ...loose 4-5-4 9 ...loose 5-7-8 15 ...firm... 10 1-2-2 4. 15 ...soft clay lense ...loose tan & brown 1-2-3 5. 20 Light tan to white SAND [SP] 3-4-5 9 ...loose 25 3-4-6 . 10 ...loose 30 2-2-2 4 ...very loose 35 Very loose light green to light tan CLAYEY SAND [SC] 1-0-1 .1. 40 Very soft green CLAY, trace of limestone fragments [CH] WOH-1-1 2 45 Tan LIMESTONE 7-7-11 50 Boring terminated at 50'

PROJECT NO .: 70080-077-03 UNIVERSAL ENGINEERING SCIENCES REPORT NO .: 367801 **BORING LOG** PAGE: B-3 B-2 1 of 1 BORING DESIGNATION: SHEET: WAL-MART STORE TRACKING NO. 95484-00 PROJECT: RANGE: S.E. CORNER OF I-75 & HIGHWAY 441 SECTION: 15/16 TOWNSHIP: 8S 18E ALACHUA, ALACHUA COUNTY, FLORIDA 10/12/04 GS ELEVATION(ft): +125 (MSL)DATE STARTED: CLIENT: CPH ENGINEERS, INC. 10/12/04 LOCATION: SEE BORING LOCATION PLAN WATER TABLE (ff): ΝE DATE FINISHED: R. WOODARD AIR BLOWING OUT OF BOREHOLE AT DEPTH OF 34 FEET DATE OF READING: N.A. DRILLED BY: REMARKS: TYPE OF SAMPLING: ASTM D-1586 EST. WSWT (ft): N.A. ATTERBERG Ŷ К ORG. BLOWS AMPLE Ν -200 MC . М В О LIMITS DEPTH (FT./ CONT. **PER 6**" (BLOWS/ W.T. DESCRIPTION (%) (%) (FT.) DAY) (%) INCREMENT FT.) LL ΡI n Brown & gray CLAYEY SAND [SC] ...very loose 3 1-1-2 3-4-5 9 loose Loose green & orange very CLAYEY SAND [SC/CL] .9. 5 3-4-5 9 6-4-5 ...loose 5-7-5 12 ...firm 13firm..... 6-6-7 10 Stiff green slightly SANDY CLAY [CH] 2-3-5 8 15 Light tan to white SAND [SP] 2-3-4 7. ...loose 20 2-3-4 7. ...loose 1. 25 Tan LIMESTONE 10-50/4" 50/4" 30 13-50/3" 50/3" Extremely hard Boring terminated at 34.5'

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PROJECT NO .: 70080-077-03 UNIVERSAL ENGINEERING SCIENCES REPORT NO .: 367801 **BORING LOG** PAGE: B-5 B-4 1 of 1 PROJECT: WAL-MART STORE TRACKING NO. 95484-00 BORING DESIGNATION: SHEET: TOWNSHIP: 8S S.E. CORNER OF I-75 & HIGHWAY 441 SECTION: 15/16 RANGE: 18E ALACHUA, ALACHUA COUNTY, FLORIDA CLIENT: CPH ENGINEERS, INC. GS ELEVATION(ft): +95 (MSL) DATE STARTED: 10/12/04 LOCATION: SEE BORING LOCATION PLAN WATER TABLE (ft): NE DATE FINISHED: 10/12/04 DATE OF READING: N.A. **REMARKS:** DRILLED BY: M. BOATRIGHT EST, WSWT (ft): N.A. TYPE OF SAMPLING: ASTM D-1586 S BLOWIS N SY ATTERBERG ĸ OPC

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PROJECT NO .: 70080-077-03 UNIVERSAL ENGINEERING SCIENCES REPORT NO .: 367801 **BORING LOG** PAGE: B-6 1 of 1 BORING DESIGNATION: B-5 SHEET: WAL-MART STORE TRACKING NO. 95484-00 PROJECT: SECTION: 15/16 TOWNSHIP: 8S RANGE: 18E S.E. CORNER OF I-75 & HIGHWAY 441 ALACHUA, ALACHUA COUNTY, FLORIDA 10/13/04 +89 (MSL) DATE STARTED: GS ELEVATION(ft): CPH ENGINEERS, INC. CLIENT: 10/13/04 DATE FINISHED: WATER TABLE (ft): NE LOCATION: SEE BORING LOCATION PLAN DATE OF READING: N.A. DRILLED BY: M. BOATRIGHT REMARKS: TYPE OF SAMPLING: ASTM D-1586 N.A. EST. WSWT (ft): Т 1

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PROJECT NO .: 70080-077-03 UNIVERSAL ENGINEERING SCIENCES REPORT NO .: 367801 **BORING LOG** B-7 PAGE: 1 of 1 B-6 WAL-MART STORE TRACKING NO. 95484-00 BORING DESIGNATION: SHEET: PROJECT: 18E TOWNSHIP: 8S RANGE: S.E. CORNER OF I-75 & HIGHWAY 441 SECTION: 15/16 ALACHUA, ALACHUA COUNTY, FLORIDA GS ELEVATION(ft): +86 (MSL) DATE STARTED: 10/12/04 CPH ENGINEERS, INC. CLIENT: 10/12/04 LOCATION: SEE BORING LOCATION PLAN WATER TABLE (ft): NE DATE FINISHED: DRILLED BY: M. BOATRIGHT DATE OF READING: N.A. REMARKS: TYPE OF SAMPLING: ASTM D1586 EST. WSWT (ft): N.A. 1 T SI Ţ 151

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PROJECT NO .: 70080-077-03 UNIVERSAL ENGINEERING SCIENCES 367801 REPORT NO .: **BORING LOG** PAGE: B-8 B-7 1 of 1 SHEET: WAL-MART STORE TRACKING NO. 95484-00 BORING DESIGNATION: PROJECT: TOWNSHIP: 85 RANGE: 18E S.E. CORNER OF I-75 & HIGHWAY 441 SECTION: 15/16 ALACHUA, ALACHUA COUNTY, FLORIDA +79 (MSL) DATE STARTED: 10/12/04 GS ELEVATION(ft): CPH ENGINEERS, INC. CLIENT: DATE FINISHED: WATER TABLE (ft): NE 10/13/04 LOCATION: SEE BORING LOCATION PLAN DATE OF READING: N.A. R. WOODARD DRILLED BY: REMARKS: TYPE OF SAMPLING: ASTM D-1586 EST. WSWT (ft): N.A. ĩ 1 ATTERREPO Т 101 ISI

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						Loose tan, orange & brown SAND [SP-SM]						
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-						tan & orange, w/limestone fragments						
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KEY TO BORING LOGS

UNIFIED CLASSIFICATION SYSTEM



RELATIVE DENSITY (sand-silt)

Very Loose - Less Than 4 Blows/Ft. Loose - 4 - 10 Blows/Ft. Medium - 10 to 30 Blows/Ft. Dense - 30 to 50 Blows/Ft. Very Dense - More Than 50 Blows/Ft.

CONSISTENCY (clay)

Very Soft - Less Than 2 Blows/Ft. Soft - 2 to 4 Blows/Ft. Medium - 4 to 8 Blows/Ft. Stiff - 8 to 15 Blows/Ft. Very Stiff - 15 to 30 Blows/Ft. Hard - More Than 30 Blows/Ft.

MAJOR DIVISIONS SYMBOLS TYPICAL N SYMBOLS GW Weil-graded gravels an mixtures, little or no fine	AMES d gravel-sand is ind gravel-sand
GW Weil-graded gravels an mixtures, little or no fine	d gravel-sand 35 1nd gravel-sand
\$ ⁰8₽ 4≥	and gravel-sand
GP Poorly graded gravels a mixtures, little or no fine	15
GM Slity gravels, gravel-sar	rd-silt mixtures
GC Clayey gravels, gravel-4 mixtures	and-clay
SW Well-graded sands and little or no lines	gravelly sands,
SP Poorly graded sands ar sands, little or no fines	xi gravelly
・ SM Sility sands, sand-silit mi	ixtures
Clayey sands, sand-cla	y mixtures
ML Inorganic silts, very fine flour, silty or clayay fine	sands, rock I sands
CL Inorganic clays of low to plasticity, gravelly clays SI 8 2 2 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5) medium , sandy clays,
State P J State 90 92 35 OL Organic silts and organic si	ic slity clays of
MH Inorganic slits, micaceo diatomaceous fine sand slits	us or is or silts, elastic
E C P F V V P F V V P F V V P F V V P F V V P F V V P F V V P F V V P F	piasticity, fat
0H Organic clays of medius plasticity	m to high
Highly Organic Soils PT Peat, muck and other h soils	ighly organic

* Based on the material pasing the 3-in. (75-mm) sieve.



Field Exploration Procedures

Standard Penetration Test Borings

The penetration borings were made in general accordance with the latest revision of ASTM D 1586, "Penetration Test and Split-Barrel Sampling of Soils". The borings were advanced by rotary drilling techniques using a circulating bentonite fluid for borehole flushing and stability. At 2 ½ to 5 foot intervals, the drilling tools were removed from the borehole and a split-barrel sampler inserted to the borehole bottom and driven 18 inches into the soil using a 140 pound hammer falling on the average 30 inches per hammer blow. The number of blows for the final 12 inches of penetration is termed the "penetration resistance, blow count, or N-value". This value is an index to several in-place geotechnical properties of the material tested, such as relative density and Young's Modulus.

After driving the sampler 18 inches (or less if in hard rock-like material), the sampler was retrieved from the borehole and representative samples of the material within the split-barrel were placed in plastic containers and sealed. After completing the drilling operations, the samples for each boring were transported to our laboratory where they were examined by our geotechnical engineer in order to verify the driller's field classification.

Auger Borings

The auger borings were performed mechanically by the use of a continuous-flight auger attached to the drill rig and in general accordance with the latest revision of ASTM D 1452, "Soil Investigation and Sampling by Auger Borings". Representative samples of the soils brought to the ground surface by the augering process were placed in plastic containers, sealed and transported to our laboratory where they were examined by our geotechnical engineer to verify the driller's field classification.

APPENDIX C

Final Study Boring Location Plan Final Study Boring Logs Key to Boring Logs Field Exploration Procedures



PROJECT NO .: 70080-077-06 UNIVERSAL ENGINEERING SCIENCES REPORT NO .: 385573 **BORING LOG** PAGE: C-2 1 of 1 WAL * MART STORE TRACKING NO. 3873-00 A-1 BORING DESIGNATION: SHEET: PROJECT: RANGE: 18E TOWNSHIP: 8S S.E. CORNER OF 1-75 & U.S. HIGHWAY 441 SECTION: 16 ALACHUA, ALACHUA COUNTY, FLORIDA GS ELEVATION(ft): 135,30 DATE STARTED: 2/7/05 CPH ENGINEERS, INC. CLIENT: 2/7/05 SEE BORING LOCATION PLAN WATER TABLE (ft): NE DATE FINISHED: LOCATION: R. WOODARD DATE OF READING: DRILLED BY: NA REMARKS: TYPE OF SAMPLING: ASTM D-1586 EST. WSWT (ft): NA ATTERBERG Ÿ ORG. AMPLE κ BLOWS N MC . М В О -200 DEPTH LIMITS (FT./ CONT. DESCRIPTION W.T. PER 6" (BLOWS/ (%) (%) (FT.) DAY) (%) INCREMENT FT.) LL ΡI 0 Brown clayey SAND [SC] 1-1-3 4 Very loose ... Medium gray, orange & tan, w/lenses of clay 4-6-7 13 Medium... .5.7.7.... ·14 5 9-7-8 15 Medium... 9-9-8 17 Medium... Medium... 9-9-8 10 Green & orange CLAY [CH] 3-5-611 Stiff... 15 2-3-36 Medium... 20

Medium light gray clayey SAND [SC]

Boring terminated at 25'

4-6-8

25

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PROJECT NO .: 70080-077-06 UNIVERSAL ENGINEERING SCIENCES **REPORT NO.:** 385573 **BORING LOG** PAGE: C-3 1 of 1 BORING DESIGNATION: A-2 SHEET: WAL * MART STORE TRACKING NO. 3873-00 PROJECT: SECTION: 16 TOWNSHIP: 8S RANGE: 18E S.E. CORNER OF I-75 & U.S. HIGHWAY 441 ALACHUA, ALACHUA COUNTY, FLORIDA 2/7/05 135.00 CPH ENGINEERS, INC. GS ELEVATION(ft): DATE STARTED: CLIENT: 2/7/05 WATER TABLE (ft): NE DATE FINISHED: LOCATION: SEE BORING LOCATION PLAN DATE OF READING: NA DRILLED BY: R. WOODARD REMARKS: TYPE OF SAMPLING: ASTM D-1586 EST. WSWT (ft): NA Ŷ ATTERBERG ORG. κ BLOWS N -200 MC LIMITS . М В О DEPTH MP (FT./ CONT. (BLOWS/ W.T. DESCRIPTION PER 6" (%) (%) (FT.) DAY) (%) INCREMENT FT.) ΡI LL E Т 0 Brown SAND [SP] Very loose brown & orange clayey SAND [SC] 1-1-3 4 10 3-4-6 Loose gray & orange.. Green, orange & gray CLAY, trace of sand [CH] 5 4-5-6 -14 Stiff.... Stiff... 8-7-8 15 Very stiff... 8-8-9 17 Medium gray & orange very clayey SAND [SC] 9-10-10 20 10 Green & orange CLAY [CH] 2-2-3 5 Medium... 15 Green, w/trace of limestone fragments 5 2-2-3 Medium... 20 Light gray to white clayey SAND [SC] 4-5-6 Medium... ...11 25 Boring terminated at 25'

J	UNIVERSAL ENGINEERING BORING LOG	PROJECT NO.: 70080-077-06 REPORT NO.: 385573 PAGE: C-4					
PROJECT:	WAL★ MART STORE TRACKING NO. 3873-00 S.E. CORNER OF I-75 & U.S. HIGHWAY 441 ALACHUA, ALACHUA COUNTY, FLORIDA	BORING DESIGNAT	ΓΙΟΝ: A- TOWNS	3 s HIP: 8\$ F	RANGE: 18	of 1	
CLIENT:	CPH ENGINEERS, INC.	GS ELEVATION(ft):	136.30	DATE START	ED; 2/7/0	05	
LOCATION:	SEE BORING LOCATION PLAN	WATER TABLE (ft):	NE	DATE FINISHE	ED: 2/7/0	05	
REMARKS:		DATE OF READING	: NA	DRILLED BY:	R. V	OODARD	
		EST, WSWT (ff):	NA	TYPE OF SAM	IPLING: AST	M D-1586	
DEPTH M		N	-200 N		RG K	ORG.	

(F1.) L INCREMENT FT.) O L PI DAY) (%) 0 - </th <th>DEPTH M</th> <th>BLOWS PER 6"</th> <th>'S N "(BLOWS/</th> <th>w.т.</th> <th>M B</th> <th colspan="2">DESCRIPTION</th> <th>MC (%)</th> <th colspan="2">MC LIMITS (%)</th> <th>(FT./</th> <th>CONT.</th>	DEPTH M	BLOWS PER 6"	'S N "(BLOWS/	w.т.	M B	DESCRIPTION		MC (%)	MC LIMITS (%)		(FT./	CONT.
0 Brown clayey SAND [SC] 1-2-3 5 4-5-7 12 Medium orange & gray very clayey 5		INCREMENT	ENT FT.)		ŌL		(70)	(70)	LL	PI	DAY)	(%)
Brown clayey SAND [SC] 1-2-3 5 4-5-7 12 Medium orange & gray very clayey 5	0											
- 1-2-3 5 Loose 4-5-7 12 Medium orange & gray very clayey 5 - - 6-5-6 11 Medium - 7-8-6 14 Medium Medium 6-8-8 16	ľ t	>	1			Brown clayey SAND [SC]						
X 4-5-7 12 Medium orange & gray very clayey 5		1-2-3	3 5			Loose						
5 - X ·····5-7·5 ···· 12 ·····12 ····· Medium gray & orange clayey - 6-5-6 11 Medium - 7-8-6 14 Medium - 6-8-8 16 Medium		4-5-7	' 12			Medium orange & gray very clayey			-			
A 6-5-6 11 Medium - 7-8-6 14 Medium - 6-8-8 16 Medium	5-X	5.7.5	····12····	¦		••• Medium gray & orange clayey•		- • • • • • • • • • • • • • •	• • • • • • • • • • • •	• • • • • • • •		
-X 7-8-6 14 Medium K 6-8-8 16 Medium		6-5-6	8 11			Medium						
X 6-8-8 16 Medium		7-8-6	6 14			Medium						
	10-X	6-8-8	16			Medjum			• • • • • • • • • • •	<i>.</i>	· • • • • • • • • • • • • • • • • • • •	
	-											
Green & orange CLAY [CH]	-					Green & orange CLAY [CH]						
-X 2-3-4 7 Medium	🛛	2-3-4	ı 7			Medium						
		¥	· · · · · · · · · · · · · · · · ·									
	-											
20 <u>X</u> 2-3-3 <u>6</u> <u>Medium</u>	20	2-3-3	<u>}6</u>			Medium						
Light tan to white clayey SAND [SC]						Light tan to white clayey SAND [SC]						
		3-6-6	12	<u> </u>		Medium						
Boring terminated at 25'	25					Boring terminated at 25'						
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UNIVERSAL ENGINEERING SCIENCES BORING LOG

 PROJECT NO .:	70080-077-06
REPORT NO .:	385573
PAGE:	C-5

PROJECT: WAL★ MART STORE TRACKING NO. 3873-00 S.E. CORNER OF I-75 & U.S. HIGHWAY 441 ALACHUA, ALACHUA COUNTY, FLORIDA CLIENT: CPH ENGINEERS, INC.

LOCATION: SEE BORING LOCATION PLAN

REMARKS:

5

BORING DESIGNATIC SECTION: 16	DN: A-4 TOWNSH	4 11P: 85	SHEET: RANGE:	1 of 1 18E
GS ELEVATION(ft):	134.70	DATE STAR	TED:	2/7/05
WATER TABLE (ff):	NE	DATE FINIS	HED:	2/7/05
DATE OF READING:	NA	DRILLED BY	<i>(</i> :	R. WOODARD
EST. WSWT (ft):	NA	TYPE OF SA	AMPLING:	ASTM D-1586

DEPTH (FT.)	AMPL	BLOWS PER 6" INCREMENT	N (BLOWS/ FT.)	w.т.	Y MBO-	DESCRIPTION	-200 (%)	MC (%)	ATTER LIMI	BERG TS PI	K (FT./ DAY)	ORG. CONT. (%)
	E					an a						
0-				<u> </u>		Brown SAND [SP]						
-	\mathbb{X}	1-1-2	3		77.Z	Very loose brown slightly clayey SAND [SM]						
-	X	2-2-4	6			Loose brown very clayey SAND [SC]						
5-	X	·····7-6-0····	12		///	•• Medium orange & light gray clayey					•••••	
-	R	6-7-7	14			Medium						
-	X	6-7-6	13			Medium						
-	\mathbb{X}	5-6-7	13			Medium						
- 10												
-	-					Green & orange CLAY, w/trace of sand [CH]	-					
-	\bigtriangledown	B A F				h dia alia una						
15 —	\sim	3-3-0	<u>.</u>			Medium	• • • • • • • • • • • • • • •	• • • • • • • • • • • • • • • •		••••		• • • • • • • • • • • • • •
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-												
20	Д	2-3-5	8			Medium		· · · · · · · · · · · · · ·				
-	-											
-]					Light gray to white clayey SAND [SC]						
	Х	1-2-2	4			Very loose						
25-						Boring terminated at 25'						
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UNIVERSAL ENGINEERING SCIENCES BORING LOG

PROJECT NO .:	70080-077-06
REPORT NO .:	385573
PAGE:	C-6

PROJECT: WALX MART STORE TRACKING NO. 3873-00 S.E. CORNER OF I-75 & U.S. HIGHWAY 441 ALACHUA, ALACHUA COUNTY, FLORIDA CLIENT: CPH ENGINEERS, INC.

CLIENT: CPH ENGINEERS, INC.

LOCATION: SEE BORING LOCATION PLAN REMARKS:

-	BORING DESIGNATIC SECTION: 16	DN: A-5 TOWNSH	D IIP: 8S	SHEET: RANGE:	1 of 1 ^{18E}
	GS ELEVATION(ft):	133.90	DATE STAR	TED:	2/8/05
	WATER TABLE (ft):	23	DATE FINIS	HED:	2/8/05
	DATE OF READING:	2/9/05	DRILLED BY	·.	J. STILLSON
	EST. WSWT (ft):	NA	TYPE OF SA	MPLING:	ASTM D-1586

CHOREBMENT FT.1 Q C C LL PI Data 0 46.7 13 Example MOTSPI	DEPTH	A M P	BLOWS PER 6"	N (BLOWS/	w.т.	Р М В	DESCRIPTION	-200 (%)	MC (%)	LIMITS		K (FT./	ORG. CONT.
0	((1))	E	INCREMENT	FT.)		U L		()	() 	LL	PI	DAY)	(%)
4.8-7 13 2.8-7 12 5	o	ļ					Prove CAND (CD)			+			
25-7 12 2-6-7 12 2-6-8 -13 2-6-8 10 2-6-9 -13 2-6-9 -13 2-6-9 -13 2-6-9 -13 2-6-9 -13 2-6-9 -14 2-6-9 -12 2-6-9 -12 2-6-9 -12 2-6-9 -12 2-6-9 -12 2-6-9 -12 2-7 -24-9 2-7 -24-9 2-7 -24-9 2-7 -24-9 3-7-9 -25 2-7 -24-9 2-7 -25 2-7 -27 2-7 -28-7 2-7 -27 2-7 -27 2-7 -27 2-7 -27 2-7 -28-7 2-7 -29 2-7 -29 2-7 -29 <td>-</td> <td></td> <td>4-6-7</td> <td>13</td> <td></td> <td>1111</td> <td>Stiff orange & gray sandy CLAY [CH]</td> <td>-</td> <td></td> <td></td> <td></td> <td></td> <td></td>	-		4-6-7	13		1111	Stiff orange & gray sandy CLAY [CH]	-					
5	-	${\bf i}$	2-5-7	12		/////	Loose orange & brown clavey SAND [SC]				•		
4-5-8 13 Loose 10 3-6-5 10 10 3-6-5 12 15 3-6-5 11 16 3-6-5 11 17 3-6-5 11 18 SWT. 20 3-4-5 9 21 SWT. 20 SWT. 21 SWT. 22 SWT. 23 SWT. 24 Light gray clayey SAND [SC] Medum. Boring terminated at 25	5-	X	2-5-8	····19····							•••••		•••••
3.4-6 10 10 .3-6-9 15 .12 15 .3-5.9 16 .3-5.9 17 18 19 10 15 16 17 18 19 10 11 12 13 14 15 16 17 18 19 10 11 12 13 14 15 16 17 18 19 10 10 <t< td=""><td></td><td>X</td><td>4-5-8</td><td>13</td><td></td><td></td><td>Loose orange & gray Loose</td><td></td><td></td><td></td><td></td><td></td><td></td></t<>		X	4-5-8	13			Loose orange & gray Loose						
10 3:6.6 .12 Medium orange & gray very olsysys 15 3:5.6 .11 Green & orange CLAY [CH] 20 3:4.5 9 Stiff. 20 Light gray clayey SAND [SC] 25 Boring Terminated at 25	-	X	3-4-6	10			Loose						
3.5-6 .11 3.5-7 .12 Image: Clark (CH) Stiff. 20 3.5-7 12 3.5-7 12 Image: Clark (CH) Stiff. 21 3.5-7 12 Image: Clark (CH) Stiff. Stiff. 25 3.5-7 12 Image: Clark (CH) Stiff. Stiff. Stiff. Stiff. Stiff. Image: Clark (CH) Stiff. Stiff.<	10	\boxtimes	3-6-6	12			Medium orange & gray very clayey						
15 .3.9.6	-												
15													
20 3:4:5 .9 .Stiff	- 15	X	3-5-6	. 11			Stiff.						
20													
20 X	-												
20 25 25 3.5.7 .12 Light gray clayey SAND [SC] Medium Boring terminated at 25'		\boxtimes	3-4-5	9			Stiff						
Light gray clayey SAND [SC] Medium Boring terminated at 25'	20-												
25 3.5.7. 12 Medium Boring terminated at 25'	-				⊻		Light gray clayey SAND [SC]						
Boring terminated at 25'		∇	3-5-7	12		///	Medium						
	25 —						Boring terminated at 25'						
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PROJECT NO .: 70080-077-06 UNIVERSAL ENGINEERING SCIENCES REPORT NO .: 385573 **BORING LOG** C-7 PAGE: 1 of 1 A-6 WAL * MART STORE TRACKING NO. 3873-00 BORING DESIGNATION: SHEET: PROJECT: S.E. CORNER OF I-75 & U.S. HIGHWAY 441 TOWNSHIP: 8S RANGE: 18E SECTION: 16 ALACHUA, ALACHUA COUNTY, FLORIDA GS ELEVATION(ft): 132.90 DATE STARTED: 2/8/05 CPH ENGINEERS, INC. CLIENT: 2/8/05 NE DATE FINISHED: SEE BORING LOCATION PLAN WATER TABLE (ft): LOCATION: J. STILLSON DATE OF READING: NA DRILLED BY: REMARKS: TYPE OF SAMPLING: ASTM D-1586 EST. WSWT (ft): NA ATTERBERG Ÿ к ORG. AMPLE BLOWS N MC -200 . М В О LIMITS DEPTH (FT./ CONT. (BLOWS/ W.T. DESCRIPTION PER 6" (%) (%) (FT.) DAY) (%) INCREMENT FT.) LL PI Т 0 Brown fine SAND Loose brown & orange very clayey SAND [SC] 4-4-6 10 Medium clayey... 4-5-8 13 ..19 Medium... 5 4-5-8 16 Medium... 4-8-8 4-6-8 14 Medium... Stiff green & orange very sandy CLAY [CH] 4-5-7 Stiff. 10 5-5-7 ...12 Stiff... 15 Medium, slightly sandy... 3-3-4 7. 20 87 3-4-6 10 Stiff. 25 Boring terminated at 25'

PROJECT NO .: 70080-077-06 UNIVERSAL ENGINEERING SCIENCES 385573 REPORT NO .: BORING LOG PAGE: C-8 1 of 1 BORING DESIGNATION: A-7 SHEET: WAL ★ MART STORE TRACKING NO. 3873-00 PROJECT: S.E. CORNER OF I-75 & U.S. HIGHWAY 441 SECTION: 16 TOWNSHIP: 85 RANGE: 18E ALACHUA, ALACHUA COUNTY, FLORIDA GS ELEVATION(ft): 131.00 2/8/05 DATE STARTED: CLIENT: CPH ENGINEERS, INC. LOCATION: SEE BORING LOCATION PLAN 2/8/05 WATER TABLE (ft): NE DATE FINISHED: DATE OF READING: NA DRILLED BY: J. STILLSON REMARKS: TYPE OF SAMPLING: ASTM D-1586 EST. WSWT (ft): NA S S Т ATTERBERG Ι Г Т

DEPTH	M	BLOWS PER 6"	N (BLOWS/	w.T.	M B	DESCRIPTION	-200 (%)	MC (%)	LIMITS		K (FT./	ORG. CONT.
(=1.)	LE	INCREMENT	FT.)		O L		(,,,)	(,,,,,	LL	PI	DAY)	(%)
0												
					777	Brown SAND [SP]	1					
	-K	4-5-6	11									
	X	4-5-5	10			Loose		l	-	·		
5-	X	3-6-11	17	••••••		·· Medium light brown, light gray & orange						
	X	3-3-7	10			Loose						
-	-X	3-3-4	7			Medium orange & green very sandy CLAY [CH] Medium						
	K	3-4-5	9	l		Stiff green & orange						
10	-											
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	\downarrow					- 117						
15 —	\bowtie	3-4-6	10			Stitt				• • • • • •	••••••	
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.				[Light gray slightly clayey SAND [SM]						
		4-4-4	8			Loose				. <i>.</i>		
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	\mathbf{b}		10									
25	\vdash	5-6-7	13		<u> 77.</u>	Boring terminated at 25'		•••••				
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PROJECT NO .: 70080-077-06 UNIVERSAL ENGINEERING SCIENCES REPORT NO .: 385573 **BORING LOG** PAGE: C-9 1 of 1 A-8 WAL * MART STORE TRACKING NO. 3873-00 SHEET: BORING DESIGNATION: PROJECT: S.E. CORNER OF I-75 & U.S. HIGHWAY 441 TOWNSHIP: 8S RANGE: 18E SECTION: 16 ALACHUA, ALACHUA COUNTY, FLORIDA GS ELEVATION(ft): 128.40 DATE STARTED: 2/7/05 CPH ENGINEERS, INC. CLIENT: 2/7/05 WATER TABLE (ft): NË DATE FINISHED: LOCATION: SEE BORING LOCATION PLAN J. STILLSON DATE OF READING: NA DRILLED BY: REMARKS: EST. WSWT (ft): NA TYPE OF SAMPLING: ASTM D-1586

DEPTH (FT.)	SAMPLE	BLOWS PER 6" INCREMENT	N (BLOWS/ FT.)	w.т.	S M B O L	DESCRIPTION	-200 (%)	MC (%)	ATTER LIMI LL	BERG TS PI	K (FT./ DAY)	ORG. CONT. (%)
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-	X	2-3-6	9			Brown SAND [SP] Loose brown & orange clayey SAND [SC]						
		2-0-0	10			Loose very clayey						
	Ŕ	3-4-5	9			Loose orange & gray clayey						
	A	3-4-5	9			Loose						
40-	Х	3-4-4	8			Medium green & orange very sandy CLAY	1				• • • • • • • • • • • • • •	
10 — - - 15 —	X	4-4-9	13			Stiff						
-						Light gray & orange clayey SAND [SC]						
	\square	2-3-6	9			Loose						
20-			********	1								
-			10			Light gray slightly clayey SAND [SM]						a,
25	again a gain	2-2-2	IIV	 	22	Boring terminated at 25'						

PROJECT NO .: 70080-077-06 UNIVERSAL ENGINEERING SCIENCES 385573 REPORT NO .: **BORING LOG** PAGE: C-10 1 of 1 A-9 SHEET: BORING DESIGNATION: WAL ★ MART STORE TRACKING NO. 3873-00 PROJECT: SECTION: 16 TOWNSHIP: 8S RANGE: 18E S.E. CORNER OF I-75 & U.S. HIGHWAY 441 ALACHUA, ALACHUA COUNTY, FLORIDA DATE STARTED: 2/7/05 GS ELEVATION(ft): 126.20 CLIENT: CPH ENGINEERS, INC. LOCATION: SEE BORING LOCATION PLAN 2/7/05 WATER TABLE (ft): NE DATE FINISHED: DATE OF READING: NA DRILLED BY: J. STILLSON REMARKS: EST. WSWT (ft): TYPE OF SAMPLING: ASTM D-1586 NA IS | S V ATTERBERG Г Í Í v

DEPTH	ΙÑ	BLOWS PER 6"	(BLOWS/	w.T.	M B	DESCRIPTION	-200	MC (%)	LIMITS		л (FT./	CONT.
(FT.)	L F	INCREMENT	FT.)		Ŏ		(70)	(70)	LL	PI	DAY)	(%)
	h~											
- 0						Brown slightly clayey SAND [SM]						
-	Д	2-2-2	4		111	Very loose brown clayey SAND [SC]						
	Ц	2-3-3	6			Loose						
5	X	2-3-5	····8····			Loose brown & light brown						• • • • • • • • • • • • • • •
	Х	3-4-4	8			Loose orange & light brown						
	X	3-4-5	9			Loose						
10-	X	3-5-8				Medium orange & light gray		,				
- 10												
					11/1	Green & orange CLAY [CH]						
-	∇	3.7-9	16			Very stiff	ļ					
15	Ë			1								
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	\vdash											
20	Å	4-5-6		·····		Stiff			• • • • • • • • • • •	•••••	· · · · · · · · · · · · · · ·	• • • • • • • • • • • • • • •
-							-					
	L					Light gray clayey SAND [SC]						
25	\boxtimes	3-5-6		ļ		Medium,						
20						Boring terminated at 25						
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PROJECT NO .: 70080-077-06 UNIVERSAL ENGINEERING SCIENCES REPORT NO .: 385573 **BORING LOG** PAGE: C-11 1 of 1 A-10 SHEET: WAL ★ MART STORE TRACKING NO. 3873-00 BORING DESIGNATION: PROJECT: SECTION: 16 TOWNSHIP: 8S RANGE: 18E S.E. CORNER OF I-75 & U.S. HIGHWAY 441 ALACHUA, ALACHUA COUNTY, FLORIDA 2/7/05 CPH ENGINEERS, INC. GS ELEVATION(ft): 124.30 DATE STARTED: CLIENT: 2/7/05 LOCATION: SEE BORING LOCATION PLAN WATER TABLE (ft): NE DATE FINISHED: DATE OF READING: NA DRILLED BY: J. STILLSON REMARKS: TYPE OF SAMPLING: ASTM D-1586 EST. WSWT (ft): NA A BLOWS Y ATTERBERG К ORG. Ν

DEPTH	M	PER 6"	(BLOWS/	W.T.	M B	DESCRIPTION	-200	MC (%)	LIMITS		(FT./	CONT.
(=1.)	ΪĽ.	INCREMENT	FT.)		ō.		(70)	(/0)	LL	PI	DAY)	(%)
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	大7		_		1//	Brown & orange very clayey SAND [SC]						
	Þ	2-4-6	10			Loose orange & brown			1			
-	ťΧ	2-3-6	9							· ·		
· _ ·	Ń											
5-	KŸ					Orange & green sandy CLAY [CH]						
	М	2-3-5	8			Medium						
.	ĮΧ	2-3-6	9			Stiff						
-	Ŕ					0416						
10	μ	3-3-5		••••••		<u> </u>		• • • • • • • • • • • • • • • • •	• • • • • • • • • •		••••••	
-	4											
-	1]
-	\mathbf{L}]		111	Loose light gray clayey SAND [SC]						
15_	X	2-4-5	9									
- 1	-											
-	{					Loose tan & light gray						
- 1	łX	3-4-5	9	1		Loose fan a light gray						
20 —	<u> </u>			••••••	11	***************************************						
-	1											
]					Light gray SAND [SP]						
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25 —	\square	2-5-6	<u>11</u>			Medium Revine terminated at 25'		•••••	• • • • • • • • • •	• • • • • • •	• • • • • • • • • • • • •	
						Boring terminated at 20						
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PROJECT NO .: 70080-077-06 UNIVERSAL ENGINEERING SCIENCES REPORT NO .: 385573 **BORING LOG** PAGE: C-12 A-11 1 of 1 SHEET: BORING DESIGNATION: WAL ★ MART STORE TRACKING NO. 3873-00 PROJECT: SECTION: 16 TOWNSHIP: 8S RANGE: 18E S.E. CORNER OF I-75 & U.S. HIGHWAY 441 ALACHUA, ALACHUA COUNTY, FLORIDA 120.60 1/28/05 GS ELEVATION(ft): DATE STARTED: CLIENT: CPH ENGINEERS, INC. NE 1/28/05 LOCATION: SEE BORING LOCATION PLAN WATER TABLE (ft): DATE FINISHED: DATE OF READING: NA DRILLED BY: M. BOATRIGHT REMARKS: TYPE OF SAMPLING: ASTM D-1586 EST. WSWT (ft): NA S Y Γ ATTERBERG ĸ ORG

DEPTH	M	PER 6"	(BLOWS/	w.т.	M B	DESCRIPTION	-200 (%)	MC (%)	LIMI	TS	(FT./	CONT.
(٣Ŧ.)		INCREMENT	FT.)		ļ		(70)	(/0/	LL	PI	DAY)	(%)
			l		<u>hu</u>							
0		·······				Brown SAND						
	М	4-4-3	7			Brown & orange clayey SAND [SC]						
-	\square	4-6-6	12									
5_	$\overline{\mathbf{X}}$					Stiff tan, brown & orange very sandy CLAY [CH]		,				
	${\mathbb R}$	2-0-0	-									
. .	Θ	2-3-4				weatum						
	\ominus	3-5-6	11									
10 —	Å	2-3-5	8			Medium					· · · · · · · · · · · · · · · ·	
· -												
-	\bigtriangledown	112	5									
15 —	\sim			•••••	11112	- Medium light green & orange	• • • • • • • • • • • • • • •	•••••		• • • • • • • •		
Į						Boring terminated at 10						j
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PROJECT NO .: 70080-077-06 UNIVERSAL ENGINEERING SCIENCES REPORT NO .: 385573 **BORING LOG** C-13 PAGE: 1 of 1 A-12 SHEET: BORING DESIGNATION: WAL * MART STORE TRACKING NO. 3873-00 PROJECT: SECTION: 16 TOWNSHIP: 8S RANGE: 18E S.E. CORNER OF I-75 & U.S. HIGHWAY 441 ALACHUA, ALACHUA COUNTY, FLORIDA 115.80 2/1/05 GS ELEVATION(ft): DATE STARTED: CPH ENGINEERS, INC. CLIENT: 2/1/05 WATER TABLE (ft): NE DATE FINISHED: LOCATION: SEE BORING LOCATION PLAN DATE OF READING: NA DRILLED BY: J. STILLSON REMARKS: TYPE OF SAMPLING: ASTM D-1586 EST. WSWT (ft): NA Г S S 1 ATTERBERG 1 Í 12

DEPTH	M	BLOWS PER 6"	N (BLOWS/	w.t.	M M B	DESCRIPTION	-200	MC		TS TS	K (FT./	ORG. CONT.
(FT.)		INCREMENT	FT.)		0 L		(%)	(%)	LL	PI	DAY)	(%)
0-					****		[
-	\leftarrow					Brown & orange sandy CLAY [CH]						
-	Ŕ	2-2-4	6			Medium						
-	Ю	4-3-5	8			Medium						
5-	Ŕ			1								
-	Ю	4-5-7	12			Suit gray & orange						
-	₿	5-5-0	11			Stiff						
10 —	ľ			1				*********				
-	\triangleright	224				Loose light gray & tan slightly clayey SAND [SM]]		ł			
15 —	$ egap = \sum_{i=1}^{n} \sum_{j=1}^{n} \sum_{i=1}^{n} \sum_{j=1}^$				<u>- [:/:</u>]	Boring terminated at 15'				•••••		
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				PR	OJECT NO .:	70080-077	7-06
				RE	PORT NO .:	385573	
	BORING	G LUG		PA	GE:	C-14	
PROJECT:	WAL★ MART STORE TRACKING NO. 3873-00 S.E. CORNER OF I-75 & U.S. HIGHWAY 441 ALACHUA, ALACHUA COUNTY, FLORIDA	BORING DESIGNA SECTION: 16	ATION: TOW	A-13 NSHIP:	SHEE 8S RANG	ET: 10 GE: 18E	of 1
CLIENT:	CPH ENGINEERS, INC.	GS ELEVATION(ft)): 108.90	DAT	FE STARTED:	2/2/0	5
LOCATION:	SEE BORING LOCATION PLAN	WATER TABLE (ft)): NE	DAI	re finished:	2/2/0	5
REMARKS:		DATE OF READIN	G: NA	DRI	LLED BY:	G. W	HITAKER
		EST. WSWT (ft):	NA	TYF	'E OF SAMPLI	NG: ASTI	M D-1586
	BLOWS N N M		-200	мс	ATTERBERG	к (Т, (ORG.

	PER 6"	N (BLOWS/	w.т.	м В	DESCRIPTION	-200 (%)	MC (%)	LIMI	TS	۲. ۲٦)	CONT.
(⁽ ⁽ ⁽ , ,))) L	INCREMENT	FT.)		Ö L		(76)	(70)	LL	PI	DAY)	(%)
										·····	
	1-2-2 2-2-3	4 5			Brown clayey SAND [SC] Very loose brown Loose		-				
5-X. -X	4-6-7	····8····· 13			··· Loose orange & brown very clayey		•••••		••••		
	5-7-9	16			Stiff green & orange CLAY [CH] Very stiff						
10	5-7-8				Stiff			•••••		••••••	
	2-4-8	12			Stiff						
15					Boring terminated at 15'		********				
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PROJECT NO .: 70080-077-06 UNIVERSAL ENGINEERING SCIENCES REPORT NO .: 385573 **BORING LOG** PAGE: C-15 1 of 1 A-14 WAL★ MART STORE TRACKING NO. 3873-00 BORING DESIGNATION: SHEET: PROJECT: TOWNSHIP: 8S RANGE: 18E S.E. CORNER OF I-75 & U.S. HIGHWAY 441 SECTION: 16 ALACHUA, ALACHUA COUNTY, FLORIDA GS ELEVATION(ft): 138.90 DATE STARTED: 2/7/05 CPH ENGINEERS, INC. CLIENT: 2/7/05 LOCATION: SEE BORING LOCATION PLAN WATER TABLE (ft): NE DATE FINISHED: DATE OF READING: R. WOODARD REMARKS: NA DRILLED BY: EST. WSWT (ft): TYPE OF SAMPLING: ASTM D-1586 NA S | S Г ATTERBERG v

DEPTH	M	BLOWS PER 6"	N (BLOWS/	W.T.	M	DESCRIPTION	-200	MC (%)	LIMITS		K (FT./	ORG. CONT.
(F1.)	LE	INCREMENT	FT.)		0 L		(70)	(70)	LL	ΡI	DAY)	(%)
0				1		Brown SAND [SP]						
i -	X	1-1-3	4		7.7.7	Manufactor Internet CAND (CC)						
-	\bigtriangledown	3-4-5	<u>م</u>		111	Very loose brown clayey SAND [SC]						
	Ø	5-4-5				Medium orange, tan & gray very clayey			-			
5-	Ĥ	4-5-6 ····	····]			Medium						
	Ц	7-5-5	10			Loose						
- 1	X	6-7-7	14			Medium						
- 1	∇	7-9-9	18			Medium						
10	۲°			1	11/							
					11/1	Green & orange CLAY [CH]						
· -												
-	K	2-2-3	5			Medium						
15-	ŕ											
	-											
-	X	3-3-3	6		V///	Medium						
20-	ľ	.,										
-					Щ	Lisht aroute white alovey CAND (SC)	ł					
	┨					Eight gray to white dayey SAND [SC]						
	K	4-5-6	11			Medium						
25-						Boring terminated at 25'						
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				PF	OJECT NO.:	70080-07	7-06
	UNIVERSAL ENG	SINEERING SCIENCES		RE	PORT NO .:	385573	
	BOF			PA	NGE:	C-16	
PROJECT:	WAL★ MART STORE TRACKING NO. 3873-00 S.E. CORNER OF I-75 & U.S. HIGHWAY 441 ALACHUA, ALACHUA COUNTY, FLORIDA	BORING DESIGN SECTION: 16	iation: Toi	A-15 WNSHIP:	SHEE 8S RANG	ET: 1 (GE: 18E	of 1
CLIENT:	CPH ENGINEERS, INC.	GS ELEVATION(ft): 140.1	10 DA ⁻	TE STARTED:	2/7/0)5
LOCATION:	SEE BORING LOCATION PLAN	WATER TABLE (ft): NE	• DA ⁻	TE FINISHED:	2/7/0)5
REMARKS:		DATE OF READ	NG: NA	DRI	ILLED BY:	R. W	/OODARD
		EST. WSWT (ft):	NA	TYF	PE OF SAMPLI	NG: ASTI	M D-1586
DEPTH M		DESCRIPTION	-200	MC	ATTERBERG LIMITS	К (FT./	ORG. CONT.

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DEPTH	Ň	PER 6"	(BLOWS/	W.Т.	M B	DESCRIPTION	-200 (%)	MC (%)	LIMI	TS	(FT./	CONT.
(FT.)	L	INCREMENT	FT.)		ļõ		(70)	(70)	LL	PI	DAY)	(%)
	-											
0						Brown SAND [SP]						
-	Х	1-2-2	4		777	Venciose brown clavey SAND ISCI						
-	Χ	2-3-4	7			Loose			-			
5-	\mathbf{X}	5.7.9	16								·····	
	Ħ	10_8_8	16			Very stiff orange & gray sandy CLAY [CH]						
- 1	\bigtriangledown	0.0.0	14			Medium gray & orange very clayey SAND, w/lenses						
-		8-8-0	14		\langle / \rangle							
10 —	\square			•••••	///	Meaturn	• • • • • • • • • • • • • • • • • • • •			•••••	•••••	
-					1111	Green & orange CLAY (CH)						
_												
	∇	3-4-4	8									
15	Ľ			•••••								
-												
-												
20	Х	2-3-4	7									
-						Light gray clayey SAND [SC]						
	\vdash											
25	Ρ	3-3-3	lb	·····	<u> </u>	Boring terminated at 25'		•••••		•••••		
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PROJECT NO .: 70080-077-06 UNIVERSAL ENGINEERING SCIENCES REPORT NO .: 385573 **BORING LOG** PAGE: C-17 A-16 1 of 1 WAL * MART STORE TRACKING NO. 3873-00 SHEET: BORING DESIGNATION: PROJECT: S.E. CORNER OF I-75 & U.S. HIGHWAY 441 18E TOWNSHIP: 8S RANGE: SECTION: 16 ALACHUA, ALACHUA COUNTY, FLORIDA GS ELEVATION(ft): 139.40 DATE STARTED: 2/7/05 CPH ENGINEERS, INC. CLIENT: 2/7/05 WATER TABLE (ft): NE DATE FINISHED: LOCATION: SEE BORING LOCATION PLAN DATE OF READING: NA R. WOODARD DRILLED BY: REMARKS: EST. WSWT (ft): NA TYPE OF SAMPLING: ASTM D-1586

	S A M P	BLOWS PER 6"	N (BLOWS/	w. . .	S Y M B	DESCRIPTION	-200 (%)	MC (%)	ATTER LIMI	BERG TS	К (FT./	ORG. CONT.
(F1.)	L E	INCREMENT	FT.)		O L		(10)	(10)	LL	PI	DAY)	(%)
0												
-						Brown SAND [SP]						
	\ominus	1-1-2	3			Very loose brown clayey SAND [SC]						
-	\ominus	1-2-3	5			Loose						
5	\ominus	2-3-5	8			··· Loose						
-	\ominus	5-3-5	8			Loose light gray & orange, w/lenses of clay					:	
	\ominus	5-6-4	10			Loose						
10 —	Å	5-6-7	13	•••••		Medium				•••••		• • • • • • • • • • • • •
-												
-	Х	3-4-4	8	ĺ		Medium						
15 —												
ļ												
1	\triangleleft		-									
20 —	4	1-2-3				Medium						
_				ļ		Green, w/lenses of sand						
	Х	2-3-4	7	l		Medium						
20						Boring terminated at 25'						
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			UN	IVEF	RSAL ENGINEERING S	CIENCES	PR		NO.:	70080-077	7-06	
N					BORING LOG			PA	GE:	v o	C-18	
PROJECT:	WAL★ MAR S.E. CORNE ALACHUA, J	T STORE ER OF I-75 ALACHUA	TRA0 5 & U.	CKING S. HIGI NTY, F	NO. 3873-00 HWAY 441 LORIDA	BORING DESIGNA SECTION: 16	TION: TOV	A-17 vnship:	85	SHEI RAN	ет: 1 с ЭЕ: 18Е	of 1
CLIENT: LOCATION: REMARKS:	CPH ENGIN SEE BORIN	EERS, IN G LOCAT	C. ION P	LAN		GS ELEVATION(ff) WATER TABLE (ff) DATE OF READIN EST. WSWT (ft):): 136.7): NE G: NA NA	0 DA1 DA1 DRI TYF	TE STAF	RTED: SHED: Y: AMPLI	2/7/0 2/7/0 R. W NG: ASTI	5 5 OODARD M D-1586
DEPTH M (FT.) L E	BLOWS PER 6" INCREMENT	N (BLOWS/ FT.)	W.Т.	S Y M B O L	DESCRIPTION		-200 (%)	MC (%)	ATTER LIM LL	BERG	K (FT./ DAY)	ORG. CONT. (%)
	1-2-3 3-3-5 748-12 10-10-10 11-10-9 8-8-8 2-3-4	5 8 20 20 19 16 7			Brown very clayey SAND [SC] Loose Very stiff orange & gray very sand Very stiff Very stiff Gray & orange clayey SAND [SC] Medium	4y CLAY [CH]			-			
	2 - 2-4	6			Medium		.,				******	

Light gray to white clayey SAND [SC]

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Medium... Boring terminated at 25'

.4-5-6 .11

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PROJECT NO .: 70080-077-06 UNIVERSAL ENGINEERING SCIENCES REPORT NO .: 385573 **BORING LOG** PAGE: C-19 1 of 1 A-18 SHEET: BORING DESIGNATION: WAL * MART STORE TRACKING NO. 3873-00 PROJECT: SECTION: 16 TOWNSHIP: 85 RANGE: 18E S.E. CORNER OF I-75 & U.S. HIGHWAY 441 ALACHUA, ALACHUA COUNTY, FLORIDA GS ELEVATION(ft): 133.30 DATE STARTED: 2/8/05 CLIENT: CPH ENGINEERS, INC. LOCATION: SEE BORING LOCATION PLAN 2/8/05 WATER TABLE (ft): NE DATE FINISHED: DATE OF READING: NA DRILLED BY: R. WOODARD REMARKS: TYPE OF SAMPLING: ASTM D-1586 EST. WSWT (ft): NA ٢ S I S ł ATTERBERG ſ

DEPTH	A M P	BLOWS PER 6"	N (BLOWS/	W.T.	Y M B	DESCRIPTION	-200	MC (%)		TS	К (FT./	ORG. CONT.
(F1.)	L E	INCREMENT	FT.)		Ö L		(70)	(70)	LL '	PI	DAY)	(%)
0				ļ								
					///	Brown very clayey SAND [SC]						
	Å	1-3-4	7			Loose orange, light gray & tan clayey, w/lenses of						
	Ц	5-6-7	13	1		clay			-			
5	X		17	<u> </u>	///	Medium						• • • • • • • • • • • • • • •
-	X	8-7-7	14			Medium						
- 1	X	8-8-6	14	1		Orange, groop & grou CLAX, trace of aloway cand						
	X	6-7-8	15			[CH]						
10						Stiff						
-						Green , w/lenses of sand						
Į -	\vdash		Į	ļ		· · · · · · · · · · · · · · · · · · ·	ļ		ļ			
15 —	Å	2-3-4		.		Medium						• • • • • • • • • • • • • •
[-				ļ								
-]					Light gray to white clayey SAND [SC]						
	$\overline{\mathbf{X}}$	2-2-3	5			Loose		1				
20	ľ											
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25 —	М	5-5-5	10		///	Loose	•••••	• • • • • • • • • • • • •	• • • • • • • • • • •			
						Boning terminated at 25						
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PROJECT NO.: 70080-077-06 UNIVERSAL ENGINEERING SCIENCES REPORT NO .: 385573 **BORING LOG** PAGE: C-20 1 of 1 A-19 WAL ★ MART STORE TRACKING NO. 3873-00 BORING DESIGNATION: SHEET: PROJECT: S.E. CORNER OF I-75 & U.S. HIGHWAY 441 SECTION: 16 TOWNSHIP: 85 RANGE: 18E ALACHUA, ALACHUA COUNTY, FLORIDA GS ELEVATION(ft): 128.60 DATE STARTED: 2/8/05 CPH ENGINEERS, INC. CLIENT: NE 2/8/05 LOCATION: SEE BORING LOCATION PLAN WATER TABLE (ft): DATE FINISHED: DATE OF READING: NA DRILLED BY: R. WOODARD REMARKS: TYPE OF SAMPLING: ASTM D-1586 EST. WSWT (ft): NA A Y ATTERBERG Κ ORG. BLOWS Ν 200 MC

(FT)	P	PER 6"	(BLOWS/	W.T.	B	DESCRIPTION	(%)	(%)		10	(FT./	CONT.
(11)	L F	INCREMENT	FT.)		l C		. /		ԼԼ	ΡI	DAT)	(%)
	_											
0-					777	Brown clayey SAND [SC]						
-	∇	122	5		///	9200						
	⇔	1-2-3	5									
	\square	3-6-7	13			Medium brown very clayey						
5—	Ж		13			Stiff gray & orange sandy CLAY [CH]		·····		••••	•••••	· · · · · · · · · · · · · · · ·
-	\mathbf{X}	7.7-8	15			ISC]						
		7-1-0				Orange & tan						
-	\ominus	8-8-7	15		///	Medium						
10	Х	6-9-8	17			Medium, very clayey						
						Orange & green very sandy CLAY [CH]						
-												
-	М	2-3-4	7	ĺ		Medium						
15 —						******						
-		-			(////							
						Light gray & orange clayey SAND [SC]						
-	∇					Versileen						
20 —	$ \bigtriangleup $	····· Z-Z-Z ·····				very loose				•••••	• • • • • • • • • • • • • • •	•••••
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-						White						
25	Д	4-6-7				Medium	, 			•••••	• • • • • • • • • • • • • • • •	
20						Boring terminated at 25'						
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PROJECT NO .: 70080-077-06 UNIVERSAL ENGINEERING SCIENCES REPORT NO .: 385573 **BORING LOG** C-21 PAGE: A-20 1 of 1 WAL★ MART STORE TRACKING NO. 3873-00 BORING DESIGNATION: SHEET: PROJECT: TOWNSHIP: 8S RANGE: 18E S.E. CORNER OF I-75 & U.S. HIGHWAY 441 SECTION: 16 ALACHUA, ALACHUA COUNTY, FLORIDA 124.80 2/7/05 GS ELEVATION(ft): DATE STARTED: CLIENT: CPH ENGINEERS, INC. 2/7/05 LOCATION: SEE BORING LOCATION PLAN WATER TABLE (ff): NE DATE FINISHED: J. STILLSON DATE OF READING: NA DRILLED BY: REMARKS: TYPE OF SAMPLING: ASTM D-1586 EST. WSWT (ft): NA T 151 SI Т Т ATTEDBEDO T r Т

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DEPTH	Ā	BLOWS		WT	M	DESCRIPTION	-200	MC	LIMITS		K (FT./	ORG. CONT.
(FT.)		INCREMENT	FT.)		O B	DECOMINATION	(%)	(%)	LL	Pl	DAY)	(%)
	15		l						Ì			
0				<u> </u>	·, ·,	Brown SAND [SP]						
_	\mathbf{X}	3-3-5	8			Loose brown & orange clayey SAND [SC]						
-	X	3-3-4	7			Loose orange & light gray	-		-			
5-	Å	2-4-6	10			Green & orange sandy CLAY [CH]	†•••••					
-	X	3-4-6	10			Stiff clay						
-	Å	3-4-5	9			Stiff						
10	Д	3-4-4	8			Medium						
	-											
{ _	$\overline{\nabla}$	3.3.5	l g			Loose light gray & grange clavey SAND [SC-SM]	4					
15 —				·····								
_]											
-												
20	Ж	3-4-7	11	 		Medium	27				· · · · · · · · · · · · · · · · · · ·	
	{											
-						Light gray slightly clayey			ļ			
-	∇	3.6.7	13			Medium						
25 —	\vdash		!**	<u>.</u>		Boring terminated at 25'						
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PROJECT NO .: 70080-077-06 UNIVERSAL ENGINEERING SCIENCES REPORT NO .: 385573 **BORING LOG** PAGE: C-22 1 of 1 A-21 SHEET: WAL * MART STORE TRACKING NO. 3873-00 BORING DESIGNATION: PROJECT: TOWNSHIP: 8S RANGE: 18E SECTION: 16 S.E. CORNER OF I-75 & U.S. HIGHWAY 441 ALACHUA, ALACHUA COUNTY, FLORIDA GS ELEVATION(ft): 119.60 DATE STARTED: 1/28/05 CPH ENGINEERS, INC. CLIENT: 1/28/05 WATER TABLE (ft): NE DATE FINISHED: LOCATION: SEE BORING LOCATION PLAN DATE OF READING: NA DRILLED BY: M. BOATRIGHT REMARKS: TYPE OF SAMPLING: ASTM D-1586 NA EST. WSWT (ft): TST Τ ATTERBERG ISI T Т Т

DEPTH	A M	BLOWS PER 6"	N (BLOWS/	w.t.	Y M B	DESCRIPTION	-200	MC (%)		TS	K (FT./	ORG. CONT.
(FT.)	L	INCREMENT	FT.)		Ö L		(%)	(78)	LL	PI	DAY)	(%)
											<u></u>	
- 1					177	Brown SAND [SP]			ĺ		-	
-	X	4-5-5	10			Loose tan, brown & brange clayey SAND [SC]]			
	Х	5-4-4	8			Loose						
5	X	5-6-6	12					•••••		• • • • • • • •		
-	∇	2-4-3	7			Medium green & orange sandy CLAY [CH]						
-	Ń	5-7-7	14			Stiff.						
-	Ŕ	3-3-4	7	1		Medium						
10 —	۴Y		• • • • • • • • • • • •					•••••				
-				5								
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15-	Х	3-4-4	8				• • • • • • • • • • • • • • • • • • • •					
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PROJECT NO .: 70080-077-06 UNIVERSAL ENGINEERING SCIENCES REPORT NO .: 385573 **BORING LOG** PAGE: C-23 A-22 1 of 1 BORING DESIGNATION: SHEET: WAL * MART STORE TRACKING NO. 3873-00 PROJECT: TOWNSHIP: 8S RANGE: 18E SECTION: 16 S.E. CORNER OF I-75 & U.S. HIGHWAY 441 ALACHUA, ALACHUA COUNTY, FLORIDA 114.00 2/3/05 CLIENT: CPH ENGINEERS, INC. GS ELEVATION(ft): DATE STARTED: LOCATION: SEE BORING LOCATION PLAN WATER TABLE (ft): NE DATE FINISHED: 2/3/05 DATE OF READING: NA J. STILLSON DRILLED BY: REMARKS: TYPE OF SAMPLING: ASTM D-1586 EST. WSWT (ft): NA Y M B ATTERBERG Ă M P BLOWS Κ ORG. Ν -200 MC LIMITS DEPTH (FT./ CONT. (BLOWS/ W.T. DESCRIPTION PER 6" (%) (%) (FT.)

	Ē		F1.)		L			LL	PI	0,71)	(70)
∩					, <u>, , , , , , , , , , , , , , , , , , </u>		 				
-				1	///	Brown clayey SAND [SC]					
-	X	1-2-3	5			Loose					
	X	2-2-3	5	1				-			
5 —	Х			<u> </u>		Green & orange CLAY [CH]	 				
-	Х	3-4-4	8			Medium					
	\square	4-5-5	10			Stiff					
-	Ŕ	5-7-8	15			Stiff					
10 —				•••••			 				
_						Lessa light grow to top alougy SAND (SC)					
						Loose light gray to tail clayey SAND [SO]					
15	Х	3-4-5	9				 				
10						Boring terminated at 15'					
				ĺ							
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PROJECT NO .: 70080-077-06 UNIVERSAL ENGINEERING SCIENCES REPORT NO .: 385573 **BORING LOG** PAGE: C-24 1 of 1 A-23 SHEET: BORING DESIGNATION: WAL★ MART STORE TRACKING NO. 3873-00 PROJECT: SECTION: 16 TOWNSHIP: 8S RANGE: 18E S.E. CORNER OF I-75 & U.S. HIGHWAY 441 ALACHUA, ALACHUA COUNTY, FLORIDA 2/2/05 GS ELEVATION(ft): 110.50 DATE STARTED: CPH ENGINEERS, INC. CLIENT: LOCATION: SEE BORING LOCATION PLAN 2/2/05 WATER TABLE (ft): NE DATE FINISHED: DATE OF READING: NA DRILLED BY: G. WHITAKER REMARKS: NA TYPE OF SAMPLING: ASTM D-1586 EST. WSWT (ft): A BLOWS S Y ATTERBERG К ORG. N 200 LINATE

(F) (C) (C) <th>DEPTH</th> <th>P</th> <th>PER 6"</th> <th>(BLOWS/</th> <th>W.T.</th> <th>B</th> <th>DESCRIPTION</th> <th>-200</th> <th>(%)</th> <th>LIV</th> <th>15</th> <th>(FT./</th> <th>CONT.</th>	DEPTH	P	PER 6"	(BLOWS/	W.T.	B	DESCRIPTION	-200	(%)	LIV	15	(FT./	CONT.
0 1.2.2 4 Lose 2.3.3 5	(ГТ.)	Ļ	INCREMENT	FT.)		P		(20)	(74)	LL	PI	DAY)	(%)
0 1-2-2 4 2-3 5 3-4-5 9 4-6-10 16 10 5-7.9 -5-7.9 18 10 5-7.9 11 18 12 5-7.9 13 18 14 -6 15 -7.9 16 -7.9 17 -7.9 18 -7.9 19 -7.9 10 -7.9 10 -7.9 11 -7.9 12 -7.9 13 -7.9 14 -7.9 15 -7.9 16 -7.9 17 -7.9 18 -7.9 19 -7.9 12 -7.9 13 -7.9 14 -7.9 15 -7.9 16 -7.9 17 -7.9				<u> </u>	<u> </u>	-					[
1.22 4 2.33 5	0			<u> </u>		111	Brown clayey SAND [SC]						
2.23 5 3.4.5 9 4.6.10 16 5.7.9 18 Medium light gray & orange 10 57.9 11 Green & orange CLAY [CH] 15 3.5.7. 3.5.7. 12 5.6.7. 12 5.7.9 13 6.7.9 14 7.7.9 15 7.7.9 12 9.7.1 12 9.7.1 12 9.7.1 12 9.7.1 12 9.7.1 12 9.7.1 12 9.7.1 12 9.7.1 12 9.7.1 13 9.7.1 14 9.7.1 15 9.7.1 12 9.7.1 12 9.7.1 12 9.7.1 12 9.7.1 12 9.7.1 13 14.1 15 15.1 14.1 16.1 15.1 17.1 <		\mathbf{X}	1-2-2	4	ļ		Loose						
5 244 0 10 Leese brown & serarae 10 44-10 16 Medium light gray & orange 10 57.8 18 Medium light gray & orange CLAY (CH) 10 57.7 12 Medium light gray & orange CLAY (CH) 16 3.55.7 12 Stift. Boning torminated at 15' Boning torminated at 15' Stift.	-	∇	222	5									
3-4-5 9 4-610 16 5-7.9 18 Mediam light gray & orange Mediam light gray & orange correct daysy 0 5-7.9 10 5-7.9 11 Green & orange CLAY (CH) Stiff. Boring terminated at 15'		Ю	2-2-3				Loose brown & orange						
3-45 9 Loose 10 5.7.9 .16	5-	Ŕ	·····9-4-4·····	1									
4-6-10 16 10 .57.9 .18	-	Ŕ	3-4-5	9			Loose						
10 .5-7-9 .19	-	X	4-6-10	16			Medium light gray & orange						
Green & orange CLAY [CH] 15 - X	10	X	5-7-9	16			Medium light gray & orange very clayey						
15 X	-						Green & orange CLAY [CH]						
15 -X	-			:									
15 - X	- · -	$\overline{\nabla}$	257	10	}		Cliff					ļ	
	15	\sim	<u>3-5-</u> /	!			Boring terminated at 15'		• • • • • • • • • • • • •			•••••••	
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PROJECT NO .: 70080-077-06 UNIVERSAL ENGINEERING SCIENCES REPORT NO .: 385573 **BORING LOG** PAGE: C-25 A-24 1 of 1 WAL * MART STORE TRACKING NO. 3873-00 SHEET: BORING DESIGNATION: PROJECT: TOWNSHIP: 8S RANGE: 18E S.E. CORNER OF I-75 & U.S. HIGHWAY 441 SECTION: 16 ALACHUA, ALACHUA COUNTY, FLORIDA GS ELEVATION(ft): 107.20 DATE STARTED: 2/2/05 CPH ENGINEERS, INC. CLIENT: 2/2/05 WATER TABLE (ft): NE DATE FINISHED: LOCATION: SEE BORING LOCATION PLAN G. WHITAKER DATE OF READING: NA DRILLED BY: REMARKS: TYPE OF SAMPLING: ASTM D-1586 EST. WSWT (ft): NA ATTERBERG ř ORG. AMPLE Κ BLOWS Ν MC -200 LIMITS ́М В О DEPTH DESCRIPTION (FT./ CONT. (BLOWS/ W.T. PER 6" (%) (%) (FT.) DAY) (%) INCREMENT FT.) LL ΡI t. 0 Brown clayey SAND [SC] 5 1-2-3 Loose .. Stiff brown & orange sandy CLAY [CH] 10 3-4-6 .5-6-7.... ·19 5 5-7-8 15 Stiff green & orange ... 12 4-5-7 Medium light brown to tan clayey SAND [SC] 26 6-8-8 16 10 3-5-5 . 10 Loose. 15 Boring terminated at 15'



UNIVERSAL ENGINEERING SCIENCES BORING LOG

PROJECT NO .:	70080-077-06	
REPORT NO .:	385573	
PAGE:	C-26	

PROJECT: WAL.★ MART STORE TRACKING NO. 3873-00 S.E. CORNER OF I-75 & U.S. HIGHWAY 441 ALACHUA, ALACHUA COUNTY, FLORIDA CLIENT: CPH ENGINEERS, INC.

LOCATION: SEE BORING LOCATION PLAN REMARKS:

BORING DESIGNATIC SECTION: 16	DN: A-2 TOWNSH	25 11P: 88	SHEET: RANGE:	1 of 1 18E
GS ELEVATION(ft):	102.00	DATE STAR	TED:	2/3/05
WATER TABLE (ft):	NE	DATE FINIS	HED:	2/3/05
DATE OF READING:	NA	DRILLED BY	<i>(</i> :	R. WOODARD
EST, WSWT (ft):	NA	TYPE OF SA	AMPLING:	ASTM D-1586

DEPTH (FT.)	SAMP-	BLOWS PER 6" INCREMENT	N (BLOWS/ FT.)	w.т.	S Y B O	DESCRIPTION	-200 (%)	MC (%)			K (FT./ DAY)	ORG. CONT. (%)
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o—					1.7.7	Brown slightly clayev SAND [SM]					·····•	
-	\boxtimes	WOH-1	1			Very loose						
-	X	WOH-1-0	1		111	Very loose dark brown clayey SAND [SC]			-			
5 —	X	·····1=1*2····		 		···Very loose				• • • • • • • •		
-	Ø	2-1-2	3			Very loose						
-		1-2-2	4			Very loose						
- 10 —	X	2-2-2	4		///	Very loose						
									2			
-						Brown						· .
15	\boxtimes	2-2-3	5	[///	Loose						
15-						Boring terminated at 15						
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			UN	IVE	RSAL ENGINEERING S	SCIENCES		R	EPORT I	VO.:	385573	
					BORING LOG			PA	AGE:		C-27	
PROJECT:	WAL★ MAR S.E. CORNE ALACHUA, /	T STORE ER OF I-75 ALACHUA	TRA0 5 & U. COU	CKING S. HIG NTY, F	NO. 3873-00 HWAY 441 FLORIDA	BORING DESIGNA SECTION: 16	TION: TOV	A-26 VNSHIP:	8S	SHE	ет: 1 с ЭЕ: 18Е	of 1
CLIENT:	CPH ENGIN	EERS, IN	C.			GS ELEVATION(ft):	137.2	0 DA	TE STAF	RTED:	2/4/0	15
LOCATION:	SEE BORIN	G LOCAT	'ION F	'LAN		WATER TABLE (ft):	NE	DA	TE FINIS	SHED:	2/4/0	15
REMARKS:						DATE OF READING	S: NA	DR	ILLED B	Y:	R. W	OODARD
						EST. WSWT (ft):	NA	TYI	PEOFS	AMPLII	VG: ASTI	M D-1586
DEPTH M	BLOWS PER 6"	N (BLOWS/	w.т.	S Y M B	DESCRIPTION		-200	MC (%)	ATTER	BERG	K (FT./	ORG. CONT.
(F1.) L E	INCREMENT	FT.)		Ö L			(70)	(70)	LL	PI	DAY)	(%)
0				777	Brown very clayey SAND [SC]				+			
	1-2-3	5								'		
	5-6-7	13			Loose orange & gray Medium					·		
5-X		10	• • • • • • • •		···Loose tan; orange & gray	• • • • • • • • • • • • • • • • • • • •		•••••	• • • • • • • • • • •	•••••		
	6-7-9	16			Medium							
	9-10-9	19			Medium orange & gray slightly cla	ayey SAND [SM]						
	000	16		11	Medium gray & orange clayey SA	ND [SC]						

+											
-14	1-2-3	5		///	Lease arange & grav						
]2	5-6-7	13			Medium		1	-			
5-	<u>4-5-5</u>	10		///	Loose tan; orange & gray	+			•••••		
-5	6-7-9	16			Medium						
ť		10		Ϋ́́/	Medium orange & gray slightly clayey SAND [SM]	1					
K	7 9-10-9 7	19		///	Medium drav & orange clavey SAND [SC]	-					
10 -	<u>48-8-8</u>	<u>16</u>		//							
4				LD		_					
1					Green & orange slightly sandy CLAY [CH]						
	7										
15	1-2-3	5		1HA	Medium					•••••••••	
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-				17	Light gray to tan clayey SAND [SC]						
	7	_		[]]							
20	<u> </u>	7	k	///	Loose			• • • • • • • • • • •		•••••	• • • • • • • • • • • • • •
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k	7			//		1					
25	2-3-5	<u>8</u>	f	//.;	Loose	<u>.</u>	••••••		·····		• • • • • • • • • • • • • •
					Bornig terminated at 25						
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PROJECT NO .: 70080-077-06 UNIVERSAL ENGINEERING SCIENCES REPORT NO .: 385573 **BORING LOG** PAGE: C-28 1 of 1 A-27 SHEET: BORING DESIGNATION: PROJECT: WAL * MART STORE TRACKING NO. 3873-00 SECTION: 16 TOWNSHIP: 8S RANGE: 18E S.E. CORNER OF I-75 & U.S. HIGHWAY 441 ALACHUA, ALACHUA COUNTY, FLORIDA GS ELEVATION(ft): 124,40 DATE STARTED: 2/7/05 CPH ENGINEERS, INC. CLIENT: 2/7/05 LOCATION: SEE BORING LOCATION PLAN WATER TABLE (ft): NE DATE FINISHED: DATE OF READING: NA DRILLED BY: J. STILLSON REMARKS: TYPE OF SAMPLING: ASTM D-1586 EST. WSWT (ft): NA T τ

DEPTH (FT.)	S A M P	BLOWS PER 6"	N (BLOWS/	w.т.	Y M B	DESCRIPTION	-200 (%)	MC (%)	ATTER LIMI	BERG TS	K (FT./	ORG. CONT.
	E	INCREMENT	+1.)		L				LL	PI		(70)
0-				ļ .		Prove SAND (SPI						
-	X	3-6-7	13			Medium brown & orange clayey SAND [SC]		2010 2010 2010 2010 2010 2010 2010 2010				
	X	3-4-7	11			Medium light brown & light gray			-			
5	\boxtimes	····· 3-4-8 ····	12		///	···Medium					••••••	
	Х	3-4-8	12			Stiff orange & gray sandy CLAY [CH]						
-	Х	4-4-8	12			Stiff						
- 10	Х	4-6-9	15	.		Stiff green & orange				·····		
-												
	1											
	∇	7_8_9	17			Verv stiff	*****					
15 —	ŕ			••••								
-												
-	-					Medium light gray & orange clayey SAND [SC]						
20	X	4-5-8	13								••••••	
	1											
						Medium light gray						
-	∇	7-8-9	17									
25						Boring terminated at 25						
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				PROJECT NO .:	: 70080-077-06		
		RING SCIENCES		REPORT NO .:	385573	573	
	BORING L	.0G		PAGE:	C-29		
PROJECT:	WAL★ MART STORE TRACKING NO. 3873-00 S.E. CORNER OF I-75 & U.S. HIGHWAY 441 ALACHUA, ALACHUA COUNTY, FLORIDA	BORING DESIGNATION SECTION: 16	ол: A-2 тоwnsh	28 SH IP: 8S RA	IEET: 1 of 1 NGE: 18E		
CLIENT:	CPH ENGINEERS, INC.	GS ELEVATION(ft):	119.30	DATE STARTED); 1/28/05		
LOCATION:	SEE BORING LOCATION PLAN	WATER TABLE (ft):	NE	DATE FINISHED); 1/28/05		
REMARKS:		DATE OF READING:	NA	DRILLED BY:	M. BOATRIG	ΗТ	
		EST. WSWT (ft):	NA	TYPE OF SAMP	LING: ASTM D-158	3	
S A				ATTERBER	G K ORG.	٦	

DEPTH	M	BLOWS PER 6"	N (BLOWS/	w.т.	M	DESCRIPTION	-200 (%)	MC (%)	LIMI	TS	к (FT./	CONT.
(⊢1.)	E	INCREMENT	FT.)		Ŏ		(76)	(76)	LL	PI	DAY)	(%)
<u> </u>	1				<u> </u>							
0-	1					Brown SAND [SP]						
-	X	2-3-3	6			Loose brown & orange clayey SAND [SC]						
-	X	4-5-4	9			Loose light brown & orange						
5—	X	4-4-5	9	• • • • • • • •		Medium light green & orange sandy CLAY [CH]		•••••		•••••	••••••	•••••
-	Ķ	4-4-4	8			Medium w/trace of sand						
-	Å	3-3-3	6			Stiff candy						
10-	Å	4-6-8									••••••	
	1											
-			.			Loose fan & orange very clayey SAND [SC]						
15-	X	1-3-3	6		\mathbb{Z}					•••••		
						Boring terminated at 15						
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			PRC	DJECT NO.:	70080-077	7-06	
\mathbb{L}				REP	ORT NO.:	385573	
	BORINGL	JG		PAG	E:	C-30	
PROJECT:	WAL★ MART STORE TRACKING NO. 3873-00 S.E. CORNER OF I-75 & U.S. HIGHWAY 441 ALACHUA, ALACHUA COUNTY, FLORIDA	BORING DESIGNAT SECTION: 16	rion: A towns	-29 ship: 8	SHEE BS RANC	ET: 1 (BE: 18E	of 1
CLIENT:	CPH ENGINEERS, INC.	GS ELEVATION(ft):	113.40	DATE	E STARTED:	2/3/0	5
LOCATION:	SEE BORING LOCATION PLAN	WATER TABLE (ft):	NE	DATE	E FINISHED:	2/3/0	5
REMARKS:		DATE OF READING	: NA	DRIL	LED BY:	G. W	HITAKER
		EST. WSWT (ft):	NA	TYPE	OF SAMPLIN	NG: ASTI	M D-1586
DEPTH M			-200	мс	ATTERBERG LIMITS	K (FT (ORG.

DEPTH	M	PER 6"	(BLOWS/	W.T.	MB	DESCRIPTION	-200		LIMI	TS	(FT./	CONT
(= 1.)	Ë	INCREMENT	FT.)		ō		(70)	(,0)	LL	PI	DAY)	(%)
					-		1			(
0 —				1		Brown slightly clayey SAND [SM]						
-	X	1-2-5	7			l oose clavey sand			1			
-	Ŕ	246	10									
-	Ю	J-4-0				Loose light gray, orange & brown						
5 —	Ô	·····4-4-4····	18	1	1111	Stiff green & orange sandy CLAY [CH]	1					
-	X	4-5-4	9			Stiff	78					
-	X	4-6-6	12			Stiff				1		
-	X	4-5-7	12			Stiff						
10	Ť			1						ł		
-						Lesse light grow to top glowow SAND [SC]	-					
-	L		Į			Loose light gray to tan clayey SAND [SC]]	ļ	J	ļ		ļ
45	Х	2-4-6	10									
15-						Boring terminated at 15'						
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PROJECT: CLIENT: LOCATION: REMARKS:	WAL ★ MAR S.E. CORNI ALACHUA, . CPH ENGIN SEE BORIN	RT STORE ER OF I-7 ALACHUA IEERS, IN IG LOCAT	: TRAC 5 & U.(\ COU IC. ION P	CKING S. HIG NTY, F 'LAN	NO. 3873-00 HWAY 441 ELORIDA	BORING DESIGN SECTION: 16 GS ELEVATION(ft WATER TABLE (ft DATE OF READIN	ATION: TOV): 106.4): NE G: NA	A-30 WNSHIP: 10 DA DA	8S TE STAF TE FINIS	SHEI RANG TED: HED: Y:	ET: 1 C GE: 18E 2/3/0 2/3/0 G. W	of 1 : :5 :5 /HITAr
DEPTH V(FT.) E	BLOWS PER 6" INCREMENT	N (BLOWS/ FT.)	W.T.	S Y B O L	DESCRIPTION	EST. WSWT (ft):	NA -200 (%)	TY MC (%)	PE OF S	AMPLI BERG ITS	NG: ASTI K (FT./ DAY)	M D-15
	1-2-4 3-4-5	6			Brown very clayey SAND [SC] Loose							
5 	5-6-6 5-7-8 3-4-6	12 15 			Green & orange sandy CLAY [CF Stiff green & orange	1]						
	3-4-6				Tan & orange clayey SAND [SC] Loose Boring terminated at 15'							
							r.					
											•	

PROJECT NO .: 70080-077-06 UNIVERSAL ENGINEERING SCIENCES REPORT NO .: 385573 **BORING LOG** PAGE: C-32 A-31 1 of 1 BORING DESIGNATION: SHEET: WAL ★ MART STORE TRACKING NO. 3873-00 PROJECT: SECTION: 16 TOWNSHIP: 8S RANGE: 18E S.E. CORNER OF I-75 & U.S. HIGHWAY 441 ALACHUA, ALACHUA COUNTY, FLORIDA 101.00 DATE STARTED: 2/3/05 GS ELEVATION(ft): CLIENT: CPH ENGINEERS, INC. 2/3/05 LOCATION: SEE BORING LOCATION PLAN WATER TABLE (ft): NE DATE FINISHED: DATE OF READING: NA DRILLED BY: R. WOODARD REMARKS: TYPE OF SAMPLING: ASTM D-1586 EST. WSWT (ft): NA

DEPTH (FT.)	S A M P -	BLOWS PER 6"	N (BLOWS/ FT.)	w.т.	Y M B O	DESCRIPTION	-200 (%)	MC (%)	ATTER LIM	BERG TS	K (FT./ DAY)	ORG. CONT. (%)
	Ē		,		Ľ	-			<u> </u>	Pl		
o-	-				///	Brown very clayey SAND [SC]						
	\mathbf{X}	1-1-2	3			Very loose	38					
	$\overline{\mathbb{X}}$	1-2-2	4	-		Very loose			-			
5-	\mathbb{X}		10	 		Stiff green & grange CLAY, w/trace of sand [CH]					•••••	
-	\mathbb{X}	6-6-5	11			Stiff						
-	X	5-6-6	12				-					
10	赵	6-7-7	14		///	Medium tan clayey SAND [SC]	· · · · · · · · · · · · · · · · · · ·			•••••	••••••	
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15-	\mathbb{X}	2-3-4	7	 		Loose						
						Boring terminated at 35						
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UNIVERSAL ENGINEERING SCIENCES BORING LOG

PROJECT NO .:	70080-077-06
REPORT NO .:	385573
PAGE:	C-33

PROJECT: WAL★ MART STORE TRACKING NO. 3873-00 S.E. CORNER OF I-75 & U.S. HIGHWAY 441 ALACHUA, ALACHUA COUNTY, FLORIDA

CLIENT: CPH ENGINEERS, INC.

LOCATION: SEE BORING LOCATION PLAN REMARKS:

BORING DESIGNATION SECTION: 16	-N: A TOWNS	32 sheet: HIP: 8s range:	1 of 1 ^{18E}
GS ELEVATION(ft):	129.50	DATE STARTED:	2/4/05
WATER TABLE (ft):	4.5	DATE FINISHED:	2/4/05
DATE OF READING:	2/5/05	DRILLED BY:	R. WOODARD
EST. WSWT (ft):	NA	TYPE OF SAMPLING:	ASTM D-1586

DEPTI	H M	BLOWS PER 6"	N (BLOWS/	w.т.	S ≻ ⊠ B	DESCRIPTION	-200	MC (%)	ATTER LIMI	BERG TS	К (FT./	ORG. CONT.
(F1.)	Ĺ	INCREMENT	FT.)		Ö L		(%)	(70)	LL	PI	DAY)	(%)
0												
Ŭ	-	7				Light brown slightly clayey SAND [SM]						
	- <u>X</u>	1-1-1	2			Very loose brown clavey						
	\rightarrow	1 1-3-4	7		$\mid V$	Loose brown slightly clayey						
5		1										
J	-K	3-3-4										
	÷	6-4-4	8			Loose brown clavey						
	- <u> </u> 2	5-6-5	11			Medium						
10	-X	4-6-8	14	<u>.</u>		Medium				. <i>.</i>		
10		1										
	4_	7]	ļ					}			
40	-X	3-4-4	8			Loose						
15		I										
	_					Prown olightly obviou						•
						prown signify clayey						
	-1X	3-5-6	11			Medium			,			
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	-	4		ļ		Very loose gray & brown clayey			}			
	-1X	1-2-2	4									
25						Boring terminated at 25'						
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UNIVERSAL ENGINEERING SCIENCES **BORING LOG**

PROJECT NO.:	70080-077-06
REPORT NO .:	385573
PAGE:	C-34

WAL* MART STORE TRACKING NO. 3873-00 PROJECT: S.E. CORNER OF I-75 & U.S. HIGHWAY 441 ALACHUA, ALACHUA COUNTY, FLORIDA CPH ENGINEERS, INC.

CLIENT: LOCATION: SEE BORING LOCATION PLAN REMARKS:

BORING DESIG	NATION: A-33		SHEET:	1 of 1
SECTION: 16	TOWNSHIP:	8S	RANGE:	18E

120.90

NE

NA

GS ELEVATION(ft): WATER TABLE (ft): DATE OF READING:

DATE FINISHED:

DATE STARTED:

EST. WSWT (ft): NA

M. BOATRIGHT DRILLED BY: TYPE OF SAMPLING: ASTM D-1586

Y ATTERBERG ORG. AMPLE κ BLOWS Ν MC -200 LIMITS M B O DEPTH (BLOWS/ W.T. DESCRIPTION (FT./ CONT. PER 6" (%) (%) (FT.) DAY) (%) INCREMENT FT.) ΡI LL 1 0 Brown SAND [SP] Loose brown & orange clayey SAND [SC] 1-2-3 5 10 4-5-5 Loose very clayey ... Medium... ·5-47-8····15 5 34 4-4-4 8 Medium tan. Stiff green & orange CLAY [CH] 10 5-5-5 Stiff... 5-6-6 .12 10 Loose brown & tan very clayey SAND [SC] 3-3-47... 1.1.1 15 Boring terminated at 15

J				UN	IVEF	RSAL ENGINEERING S BORING LOG	SCIENCES		PF RE PA	ROJECT PORT N	NO.: IO.:	70080-077 385573 C-35	7-06
PROJECT	:	WAL * MAR S.E. CORNE ALACHUA, /	T STORE ER OF I-79 ALACHUA	TRAC 5 & U.3 COU	CKING S. HIG NTY, F	NO. 3873-00 HWAY 441 'LORIDA	BORING DESIGNA SECTION: 16	TION: TOW	A-34 /NSHIP:	85	SHEE	ET: 1 C GE: 18E	of 1
CLIENT:		CPH ENGIN	EERS, IN	C.			GS ELEVATION(ft)	: 116.20	DAT	LE STAR	TED:	1/28/	05
LOCATIO	N:	SEE BORIN	G LOCAT	ION P	LAN		WATER TABLE (ft)	: NE	DA	re finis	HED:	1/28/	05
REMARK	5:						DATE OF READIN EST, WSWT (ft):	G: NA NA	DRI TYF	LLED B	Y: AMPLII	M. BO	DATRIGHT /I D-1586
DEPTH (FT.)	S A M P I	BLOWS PER 6" INCREMENT	N (BLOWS/ FT.)	w.т.	S Y B O	DESCRIPTION		-200 (%)	MC (%)		BERG TS	K (FT./ DAY)	ORG. CONT. (%)
	Ĕ			<u> </u>	Ĕ					LL.	14		
0-						Brown SAND [SP]	·····						
-	\bigotimes	2 - 4-4 3-4-5	8 9			Brown & orange clayey SAND [So Tan, brown & orange very clayey	C] 			-			
5	X	4-5-6 4-4-5	····11····· 9			Stiff green & orange sandy CLAY	[CH]						

(FT)	191		(0,00,000)	1			(%)	(%)			BA 10	
((1))	Ē	INCREMENT	FT.)		O L		(,,,,	()	LL	PI	DAY)	(%)
								[
-	\vdash					Brown SAND [SP]	-					
-	Ŕ	2-4-4	8			Brown & orange clayey SAND [SC]						
-	Ŕ	3-4-5	9			Tan, brown & orange very clayey			-			
5	Ŕ	4-5-6	••••11•••••	•••••		Stiff green & orange sandy CLAY [CH]					•••••	
· _	Ø	4-4-5	9									
-	Ŕ	3-4-5	9			Stiff						
- 10 —	А	4-6-8	14						• • • • • • • • • •			
_						Tan & brown clavey SAND (SC)						
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	\boxtimes	2-3-4	7									
1.5						Boring terminated at 15'						
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	in state along			UN	IVEF	RSAL ENGINEERING S	CIENCES		PR RF		NO.:	70080-077	7-06		
\mathbb{N}	1					BORING LOG			PA	GE:		C-36			
PROJECT CLIENT: LOCATIO REMARKS	-: N: 3:	WAL★ MAR S.E. CORNE ALACHUA, A CPH ENGIN SEE BORIN	T STORE ER OF I-7 ALACHUA IEERS, IN G LOCAT	: TRAC 5 & U. 5 & U. C. C.	cking S. Hig Nty, F Lan	NO. 3873-00 HWAY 441 FLORIDA	BORING DESIGNATION: A-35 SHEET: SECTION: 16 TOWNSHIP: 8S RANGE GS ELEVATION(ft): 110.40 DATE STARTED: WATER TABLE (ft): NE DATE FINISHED: DATE OF READING: NA DRILLED BY: EST. WSWT (ft): NA TYPE OF SAMPLING					ET: 1 C BE: 18E 2/3/0 2/3/0 G. W NG: ASTI	r: 1 of 1 E: 18E 2/3/05 2/3/05 G. WHITAKEF G: ASTM D-1586		
DEPTH (FT.)	SAN Lu	BLOWS PER 6" INCREMENT	N (BLOWS/ FT.)	w.т.	SYMBO-	DESCRIPTION		-200 (%)	MC (%)	ATTER LIM LL	BERG ITS	K (FT./ DAY)	ORG CON (%)		
0-	с. 	<u> </u>				Brown clayey SAND [SC]						. <u>.</u>			
-	X	1-2-4 2-3-4	6 7			Loose light brown, gray & orange									
5 — - -	X	······3-3-4····· 3-5-6	····· 7 ····· 11			Medium gray & orange						•••••			
- - 10 	X	7-8-10 3-4-5	18 9			Stiff light gray & orange sandy CL ·· Stiff green & orange:	AY [CH]								
-		467	10			Ohite					-				
15 —			!6	- / · · · · ·		Boring terminated at 15'									
			E 												
												•			

PROJECT NO .: 70080-077-06 UNIVERSAL ENGINEERING SCIENCES REPORT NO .: 385573 **BORING LOG** PAGE: C-37 A-36 1 of 1 WAL * MART STORE TRACKING NO. 3873-00 SHEET: BORING DESIGNATION: PROJECT: S.E. CORNER OF I-75 & U.S. HIGHWAY 441 TOWNSHIP: 8S RANGE: 18E SECTION: 16 ALACHUA, ALACHUA COUNTY, FLORIDA GS ELEVATION(ft): 104.10 DATE STARTED: 2/3/05 CPH ENGINEERS, INC. CLIENT: 2/3/05 WATER TABLE (ft): NE DATE FINISHED: LOCATION: SEE BORING LOCATION PLAN DATE OF READING: G. WHITAKER NA DRILLED BY: REMARKS: EST. WSWT (ft): TYPE OF SAMPLING: ASTM D-1586 NA

DEPTH (FT.)	AMPL	BLOWS PER 6" INCREMENT	N (BLOWS/ FT.)	w.r.	У МВО-	DESCRIPTION	-200 (%)	MC (%)	ATTER LIMI LL	BERG TS PI	K (FT./ DAY)	ORG. CONT, (%)
	E :							1				
0-			·····	<u> </u>	1.1	Brown clayey SAND [SC]		1				
	Х	1-2-2	4			Very loose						
-	R	2-2-3	5			Loose			-			
5-	\mathbb{N}	·····0]2*#····		.		·····			ļ			
-	权	2-3-5	8			Loose brown Loose brown & orange very clavey	÷					
-	Ŕ	500	16									
	Ю	0.45										
10 —	\vdash			••••••		- Sull			•••••	******		
-												
] -	L		ļ	ļ								
15-	Х	3-5-7				Stiff						
						Boring terminated at 15						
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Į,				UN	IVEF	RSAL ENGINEERING SCIENCES BORING LOG	\$	PF RE PA	OJECT	NO.: 10.:	70080-07 385573 C-38	7-06			
PROJEC	ľ:	WAL + MAR S.E. CORNE	T STORE ER OF I-7 ALACHUA	: TRA(5 & U. \ COU	CKING 5, HIG NTY, F	NO. 3873-00 BORING DES HWAY 441 SECTION: ~	IGNATION: 16 TOV	A-37 vnship:	85	SHEE	ET: 1 C GE: 18E	of 1			
CLIENT: LOCATIC REMARK	DN: S:	CPH ENGIN SEE BORIN	IEERS, IN G LOCAT	ic. 'Ion P	LAN	GS ELEVATIO WATER TABL DATE OF REA EST. WSWT (GS ELEVATION(ft): 98.10 WATER TABLE (ft): NE DATE OF READING: NA EST. WSWT (ft): NA				DATE STARTED:2/3/05DATE FINISHED:2/3/05DRILLED BY:R. WOODARTYPE OF SAMPLING:ASTM D-158				
DEPTH (FT.)	S A MP L H	BLOWS PER 6" INCREMENT	N (BLOWS/ FT.)	w.т.	S Y B O L	DESCRIPTION	-200 (%)	MC (%)	ATTER LIM LL	BERG ITS	K (FT./ DAY)	ORG CONT (%)			
0-		WOH	WOH			Brown clayey SAND [SC] Very loose									
5		WOH-1-1 ·····↑-0-1····· 1-1-1	2 1 2			Very loose ··Very loose Very loose			-	•••••					
- 10 —		1-1-1 2-2-3	2 <u>5</u>			Very loose Loose brown very clayey									
- 15 —		5-6-8	14			Gray & orange clayey <u>Medium</u> Boring terminated at 15'									
				-											
	1										•				

			1.15.1	1) / 5- 5-		PF	ROJECT	NO.:	70080-077	7-06		
KL/			UN	IVEF		UENCES		RE		10.:	385573	
					BORING LOG			P/	\GE:		C-39	
PROJECT:	WAL★ MAR S.E. CORNE ALACHUA, /	T STORE ER OF I-7 ALACHUA	TRAC 5 & U.S	KING S. HIGI NTY, F	NO. 3873-00 HWAY 441 'LORIDA	BORING DESIGNA SECTION: 16	TION: TOV	A-38 VNSHIP:	85	SHEI RAN(ET: 10 GE: 18E	of 1
CLIENT:	CPH ENGIN	IEERS, IN	IC.		,	GS ELEVATION(ft)): 132.3	0 DA	TE STAF	TED:	2/4/0	5
LOCATION:	SEE BORIN	G LOCAT	ION P	LAN		WATER TABLE (ft)	I: NE	DA	TE FINIS	HED:	2/4/0	5
REMARKS:						DATE OF READIN	G: NA	DR	ILLED B	<i>(</i> :	R. W	OODARD
						EST. WSWT (ff):	NA	TYI	PE OF S	AMPLI	NG: ASTI	A D-1586
DEPTH MP (FT.) L	BLOWS PER 6" INCREMENT	N (BLOWS/ FT.)	w.т.	S Y M B O -	DESCRIPTION		-200 (%)	MC (%)	ATTER LIMI	BERG TS	K (FT./ DAY)	ORG. CONT. (%)
	·							·····				
					Brown clayey SAND [SC]							
	1-2-2	4			Loose brown silty very clayey							
	2-3-4				Medium light gray & orange							
	000	16			Very stiff green & tan slightly sand							
	10 10 9	10			Very stiff	ly obsit [on]						
	7 10-10-9	20			Very stiff green					} 		
	3-4-5	9			Stiff			••••				
20-X	2-2-4	6			Medium					•••••		

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Light green very sandy...

Stiff... Boring terminated at 25'

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3-4-7 11

PROJECT NO .: 70080-077-06 UNIVERSAL ENGINEERING SCIENCES REPORT NO .: 385573 **BORING LOG** PAGE: C-40 A-39 1 of 1 SHEET: BORING DESIGNATION: PROJECT: WAL ★ MART STORE TRACKING NO. 3873-00 SECTION: 16 TOWNSHIP: 8S RANGE: 18E S.E. CORNER OF 1-75 & U.S. HIGHWAY 441 ALACHUA, ALACHUA COUNTY, FLORIDA 1/27/05 GS ELEVATION(ft): 116.10 DATE STARTED: CLIENT: CPH ENGINEERS, INC. 1/27/05 LOCATION: SEE BORING LOCATION PLAN WATER TABLE (ft): NE DATE FINISHED: DATE OF READING: NA DRILLED BY: M. BOATRIGHT REMARKS: TYPE OF SAMPLING: ASTM D-1586 EST. WSWT (ft): NA T Í

DEPTH	A M P	BLOWS PER 6"	N (BLOWS/	w.т.	Ϋ́ Μ Β	DESCRIPTION	-200 (%)	MC (%)	ATTER LIMI	BERG TS	K (FT./	ORG. CONT.
())	E	INCREMENT	(.T-1		O L				LL	Pl	DAY)	(%)
0-						Brown SAND (SP)						
	X	2-2-5	7		11	Loose brown & orange very clayey SAND, w/trace of						
	-17	4-5-6	11			roots [SC] Medium brown slightly clayey SAND [SM]				÷		
5-	X	6-8-7	15			Madium harven 9. seenaa					•••••	
	-X	3-3-3	6			Green & orange sandy CLAY [CH]						
	\mathbb{X}	3-5-6	11			Stiff						
10 -	1	2-2-3	5			Medium						
,,,	-											
]_											
15 -	-12	3-2-3	5			Medium						
						Boring terminated at 15'						
											-	
											-	
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UNIVERSAL ENGINEERING SCIENCES BORING LOG

PROJECT NO .:	70080-077-06
REPORT NO .:	385573
PAGE:	C-41

PROJECT:WAL★ MART STORE TRACKING NO. 3873-00
S.E. CORNER OF 1-75 & U.S. HIGHWAY 441
ALACHUA, ALACHUA COUNTY, FLORIDACLIENT:CPH ENGINEERS, INC.

LOCATION: SEE BORING LOCATION PLAN REMARKS:

BORING DESIGNATIO SECTION: 16	N: A-4 TOWNSH	40 IIP: 8S	SHEET: RANGE:	1 of 1 18E
GS ELEVATION(ft):	111.60	DATE STAR	TED:	1/28/05
WATER TABLE (ft):	NE	DATE FINISI	HED:	1/28/05
DATE OF READING:	NA	DRILLED BY	' :	M. BOATRIGHT
EST. WSWT (ft):	NA	TYPE OF SA	MPLING:	ASTM D-1586

DEPTH (FT.)	SAMPL	BLOWS PER 6" INCREMENT	N (BLOWS/ FT.)	w.т.	0 Y∑≊O	DESCRIPTION	-200 (%)	MC (%)		BERG TS	K (FT./ DAY)	ORG. CONT. (%)
	E		<u> </u>					<u> </u>				
o —		·				Brown SAND [SP]						
-	X	3-1-2	3			Marchana brown daway CAND (CC)						
-	∇	3-4-4	8			Very loose brown clayey SAND [SC]						
5-	\mathbb{X}		₈			Loose brown & orange						• • • • • • • • • • • • • • •
	Ŕ	4-4-5	9			Loose						
	Ŕ	3-4-6	10			Loose gray, brown & grange very clavey						
-	$\overline{\mathbf{X}}$	4-5-7	12			Stiff gray, light green & orange sandy CLAY [CH]						
10	Ľ		!									
-						Green & orange						
			Į			Green & Grange			ļ			
15 —	Д	5-6-6	12			Stiff				•••••		
						boing terminated at 15						
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PROJECT NO .: 70080-077-06 UNIVERSAL ENGINEERING SCIENCES REPORT NO .: 385573 **BORING LOG** PAGE: C-42 1 of 1 BORING DESIGNATION: A-41 SHEET: WAL★ MART STORE TRACKING NO. 3873-00 PROJECT: SECTION: 16 TOWNSHIP: 8S RANGE: 18E S.E. CORNER OF I-75 & U.S. HIGHWAY 441 ALACHUA, ALACHUA COUNTY, FLORIDA GS ELEVATION(ft): 106.50 DATE STARTED: 2/2/05 CLIENT: CPH ENGINEERS, INC. 2/2/05 LOCATION: SEE BORING LOCATION PLAN WATER TABLE (ft): NE DATE FINISHED: DATE OF READING: NA DRILLED BY: J. STILLSON REMARKS: TYPE OF SAMPLING: ASTM D-1586 NA EST. WSWT (ft): 1 5 1 ATTERDEDC Т Т ISI Т ١ 1

DEPTH	A M	BLOWS	N (BLOW(S)	WT	M	DESCRIPTION	-200	MC		TS	К (FT./	ORG. CONT.
(FT.)	2 L E	INCREMENT	FT.)		0 L		(%)	(%)	LL	PI	DAY)	(%)
	-								<u> </u>			
0						Brown SAND [SP]						
	\mathbf{X}	2.3.4	7		[]]	Loose brown clayey SAND [SC]						
		2-3-4	,		///	Loose						
	\ominus	2-1-2	3			Very loose			-			
5—	X	·····1=2-2····			///	···Very loose				•••••	••••••	
·	Х	2-3-4	7		///	Loose very clayey						
_	\mathbf{X}	3-4-5	9									
-	\forall	0,0	10		//	Loose orange & gray Modium						
10 —	$ \bigtriangleup $!	· · · · · · · ·	///		• • • • • • • • • • • • • • • •	•••••			••••••	
-												
-												
	$\overline{\mathbf{X}}$	246	10			Loose light grav						
15 —	$ \bigtriangleup $	5-4-0				Boring terminated at 15'	• • • • • • • • • • • • • •			• • • • • • • •	,	
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			ΠN		RSAL ENGL		CIENCES		PR	OJECT	NO.:	70080-07	7-06
			014						RE	PORT	10.: :	385573	
					DURI	NGLOG			. PA	GE:		C-43	
PROJECT:	WAL★ MAR S.E. CORNE ALACHUA, A	T STORE ER OF I-79 ALACHUA	TRAC 5 & U.(CKING S. HIGI NTY, F	NO. 3873-00 HWAY 441 LORIDA		BORING DESIGNA SECTION: 16	TION: TOW	A-42 (NSHIP:	85	SHEE	ET: 1 c GE: 18E	of 1
CLIENT:	CPH ENGIN	EERS, IN	C.				GS ELEVATION(ft):	101.50	DA1	LE STAF	TED:	2/3/0	5
OCATION:	SEE BORIN	G LOCAT	ION P	LAN			WATER TABLE (ft):	NE	DAT	re finis	HED:	2/3/0	5
REMARKS:							DATE OF READING	: NA	DRI	LLED B	ŕ :	G. W	HITAKER
							EST. WSWT (ft):	NA	TYF	PE OF S	AMPLIN	NG: ASTI	M D-1586
DEPTH M	BLOWS PER 6"	N (BLOWS/	w.т.	S Y M B		DESCRIPTION		-200 (%)	MC (%)	ATTER LIM	BERG ITS	К (FT./	ORG. CONT.
	INCREMENT	FT.)		O L				(14)	(12)	LL	PI	DAY)	(%)
0				///	Brown clayey S	AND [SC]							
$\overline{\nabla}$					1.4			ŀ					· ·

							<u> </u>			
°+		1		Brown clayey SAND [SC]						
	1-2-2	4		Very loose		l			-	
	2-2-2	4		Very loose			-			
5-	X	4		Very loose				•••••	• • • • • • • • • • • • •	• • • • • • • • • • • • • • • • • •
	2-3-5	8		Loose gray, brown & orange						
	4-6-8	14		Stiff green & orange CLAY [CH]	-					
10-	3-5-6			Stiff			· · · · · · · · · · · · ·	· · · · · · · ·		
_		:		Orange & green sandy						
15	3-4-6	10		Stiff						
10				Boring terminated at 15'						
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pytracy is the set									
	UNIVERSAL ENGINEER	ING SCIENCES		REPORT N	573				
	BORINGL	JG		PAGE:	C-44	4			
PROJECT:	WAL★ MART STORE TRACKING NO. 3873-00 S.E. CORNER OF I-75 & U.S. HIGHWAY 441 ALACHUA, ALACHUA COUNTY, FLORIDA	BORING DESIGNATIO SECTION: 16	N: A-4 TOWNSHI	3 P: 8S	SHEET: RANGE:	1 of 1 ^{18E}			
CLIENT:	CPH ENGINEERS, INC.	GS ELEVATION(ft):	96.30	DATE STAR	TED:	2/4/05			

CLIENT: LOCATION: SEE BORING LOCATION PLAN REMARKS:

GS ELEVATION(ft):	96.30
WATER TABLE (ft):	NE
DATE OF READING:	NA
EST. WSWT (ft):	NA

DATE STARTED: DATE FINISHED: DRILLED BY:

R. WOODARD TYPE OF SAMPLING: ASTM D-1586

2/4/05

DEPTH	S A M P	BLOWS PER 6"	N (BLOWS/	w.t.	S Y M B	DESCRIPTION	-200 (%)	MC (%)	ATTER LIMI	BERG TS	K (FT./	ORG. CONT.
(~1.)	Ē	INCREMENT	FT.)		Ö L		(70)	(70)	LL	Ρl	DAY)	(%)
Г о-		<u> </u>	<u> </u>	ļ	1777							
	\downarrow	MOU				Brown clayey SAND [SC]						
	70					Very loose						(
5-	扖	ן ו-ו-ו •••••≁-⊡₌ቀ•••••	 			··Verv loose						
	-17	1-1-1	2			Very loose						
	-X	1-1-1	2			Very loose						
10-	-X	1-1-1	2			Very loose						
10		2-3-4	7			Loose						
15-	_ <u>/_``</u>					Boring terminated at 15						
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UNIVERSAL ENGINEERING SCIENCES BORING LOG

PROJECT NO .:	70080-077-06
REPORT NO .:	385573
PAGE:	C-45

PROJECT: WAL★ MART STORE TRACKING NO. 3873-00 S.E. CORNER OF I-75 & U.S. HIGHWAY 441 ALACHUA, ALACHUA COUNTY, FLORIDA

CLIENT: CPH ENGINEERS, INC.

LOCATION: SEE BORING LOCATION PLAN REMARKS:

BORING DESIGNATIO SECTION: 16	DN: A- TOWNSI	44 SHEE HIP: 8S RANC	T: 1 of 1 BE: 18E
GS ELEVATION(ft):	133.70	DATE STARTED:	2/4/05
WATER TABLE (ft):	4	DATE FINISHED:	2/4/05
DATE OF READING:	2/5/05	DRILLED BY:	R. WOODARD
EST. WSWT (ft):	NA	TYPE OF SAMPLIN	IG: ASTM D-1586

DEPTH B PER 6" (BLOWS/		W.T. B		DESCRIPTION	-200 (%)	MC (%)	ATTER LIMI	BERG TS	K (FT./	ORG. CONT.		
(۴1.)	Ē	INCREMENT	`FT.)		Ŭ L		(%)	(%)	LL	PI	DAY)	(%)
0-						Proven slightly alovey SAND (SMI	<u> </u>					
-	\bigtriangledown		2	ĺ								
	Ŕ	1-1-1		_		very loose						
-	\bigotimes	1-1-0)))))	¥		Loose light gray & orange						
5-	Ŕ	2-3	12									
-	\bigotimes	0 40 40	20			Medium						
_	\bigotimes	9-10-10	20		7/7	Medium gray clayey SAND [SC]						
10 —	КЛ	10-11-11			///		• • • • • • • • • • • • • • •					
						Green & orange CLAY, w/trace of sand & limestone fragments [CH]						
- 15	М	4-5-6	11			Stiff						
- 15												
						Light gray, green & orange sandy						
- 20 —	K	3-3-4	7	ļ		Medium					· · <i>·</i> · · · · · · · · · · · · · · · ·	
-												
	1					Green & orange clay, w/lenses of sand						
-	∇	3-4-5	9			Stiff						
25	ľ					Boring terminated at 25'						
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				}								
			NO.4 4 4									
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	1		}		}							

		PROJECT NO.: 70080-077-06					
		REPORT NO	5573				
	BURING L	.0G		PAGE:	C-4	6	
PROJECT:	WAL★ MART STORE TRACKING NO. 3873-00 S.E. CORNER OF I-75 & U.S. HIGHWAY 441 ALACHUA, ALACHUA COUNTY, FLORIDA	BORING DESIGNATION SECTION: 16	DN: A-4 TOWNSH	15 IP: 85	SHEET: RANGE:	1 of 1 ^{18E}	
CLIENT:	CPH ENGINEERS, INC.	GS ELEVATION(ft):	110.60	DATE START	ED:	1/27/05	
LOCATION:	SEE BORING LOCATION PLAN	WATER TABLE (ft):	NE	DATE FINISH	IED:	1/27/05	
REMARKS:		DATE OF READING:	NA	DRILLED BY:		M. BOATRIG	H
		EST. WSWT (ft):	NA	TYPE OF SA	MPLING:	ASTM D-158	6
S	S S			ATTERB	ERG	K ORG	

DEPTH	С М М	BLOWS PER 6"	(BLOWS/	w.т.	MB	DESCRIPTION	-200 (%)	MC (%)	LIMITS		(FT./	CONT.
(*1.)	L INCREMENT FT.)		ΙÕ		(70)	(70)	LL PI		DAY)	(%)		
0												
-	\square					Brown SAND [SP]						
-	Ø	2-2-2	4		· //	Very loose brown slightly clayey SAND [SM]	1					
-	Ŕ	2-3-4	7			Loose brown, gray & orange	{		.			
5—	Ă		·····8·····	•••••		···Loose gray, orange & brown clayey SAND [SC] ······			• • • • • • • • • • •			• • • • • • • • • • • • • •
	Ø	4-5-7	12			Gray & orange very clayey						
	\bigotimes	8-8-10	18			Stiff green & grange sandy CLAY [CH]						
10	\bowtie	4-4-6	10				• • • • • • • • • • • • • • •					. <i></i>
-										-		
·												
15 —	М	3-3-5	8			Medium		• • • • • • • • • • • • • • • • • • • •				
						Doning terminated at 10						
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PROJECT NO .: 70080-077-06 UNIVERSAL ENGINEERING SCIENCES REPORT NO .: 385573 **BORING LOG** PAGE: C-47 A-46 1 of 1 WAL ★ MART STORE TRACKING NO. 3873-00 BORING DESIGNATION: SHEET: PROJECT: TOWNSHIP: 8S RANGE: 18E S.E. CORNER OF I-75 & U.S. HIGHWAY 441 SECTION: 16 ALACHUA, ALACHUA COUNTY, FLORIDA CPH ENGINEERS, INC. GS ELEVATION(ft): 106.40 DATE STARTED: 1/28/05 CLIENT: WATER TABLE (ft): NE DATE FINISHED: 1/28/05 LOCATION: SEE BORING LOCATION PLAN DATE OF READING: NA M. BOATRIGHT DRILLED BY: REMARKS: EST. WSWT (ft): TYPE OF SAMPLING: ASTM D-1586 NA 1S T Ş | -ATTERBERG Г 0.000

			w.т.			-200 (%)	MC (%)	LIMITS		к (FT./	CONT.
	L INCREMENT FT.)	FT.)		Ō		(70)	(70)	LL	PI	DAY)	(%)
	1										
					Brown SAND [SP-SM]						
I -×	2-2-2	4			very loose brown a brange						
	2-2-2	4			Very loose brown & orange clayey SAND [SC]			-			
5 <u>×</u>	······ 3-3-4····		 		··· Loose			• • • • • • • • • • •		•••••	
	4-5-5	10			Medium						
- <u>×</u>	4-5-5	10		///	Medium						
	3-4-4	8			Loose brown, gray & orange						
				///							
					Green & orange sandy CLAY [CH]	1					
	2.3.5				Medium						
15-	¥ <u>~-~-</u>				Boring terminated at 15'		•••••		•••••		
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UNIVERSAL ENGINEERING SCIENCES **BORING LOG**

PROJECT NO .:	70080-077-06
REPORT NO .:	385573
PAGE:	C-48

PROJECT: WAL * MART STORE TRACKING NO. 3873-00 S.E. CORNER OF 1-75 & U.S. HIGHWAY 441 ALACHUA, ALACHUA COUNTY, FLORIDA CLIENT:

CPH ENGINEERS, INC.

LOCATION: SEE BORING LOCATION PLAN REMARKS:

BORING DESIGNATIC SECTION: 16	N: A-4 TOWNSH	47 11P: 8S	SHEET: RANGE:	1 of 1 18E
GS ELEVATION(ft):	103.30	DATE STAR	TED:	2/2/05
WATER TABLE (ff):	NE	DATE FINISI	HED:	2/2/05
DATE OF READING:	NA	DRILLED BY	' :	J. STILLSON
EST. WSWT (ft):	NA	TYPE OF SA	MPLING:	ASTM D-1586

DEPTH	AMP.	BLOWS PER 6"	N (BLOWS/	w.т.	Y M B	DESCRIPTION	-200 (%)	MC (%)	LIMI	BERG TS	K (FT./	ORG. CONT.
	L E	INCREMENT	<u>۲.)</u>		L				LL	PI		(70)
0	 					Brown SAND (SP)						
	\square	2-1-1	2									
-	X	1-2-1	3		777	Very loose			-			
5—	X	2-2-2	····4····			Loose grav & orange very clavey		·····		•••••		• • • • • • • • • • • • • • •
	Д	2-3-5	8									
-	X	4-5-6	11			Medium						
	X	4-5-7	12			Medium light gray to grange		·····		·····		
						Orange & gray sandy CLAY [CH]						
-	_		ļ					1	[
15 —	Х	2-3-4	7			Medium Boring terminated at 15'	• • • • • • • • • • • • • • •					• • • • • • • • • • • • • • •
						Downg terminated at 10						
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				PROJECT NO .:	70080-077	-06					
\mathbf{k}		REPORT NO .:									
	BORING LOC	BORING LOG									
PROJECT:	WAL★ MART STORE TRACKING NO. 3873-00 S.E. CORNER OF I-75 & U.S. HIGHWAY 441 ALACHUA, ALACHUA COUNTY, FLORIDA	BORING DESIGNATION SECTION: 16	ом: A-4 тоwnshi	8 SHEI P: 8S RANG	ET: 10 GE: 18E	if 1					
CLIENT:	CPH ENGINEERS, INC.	GS ELEVATION(ft):	99.50	DATE STARTED:	2/3/0	5					
LOCATION:	SEE BORING LOCATION PLAN	WATER TABLE (ft):	NE	DATE FINISHED:	2/3/0	5					
REMARKS:		DATE OF READING:	NA	DRILLED BY:	G. W	HITAKER					
		EST. WSWT (ft):	NA	TYPE OF SAMPLI	NG: ASTN	1 D-1586					
	BLOWS N Y		200 MC	ATTERBERG	ĸ	ORG.					

DEPTH	S A M P	BLOWS PER 6"	N (BLOWS/	W.T.	Y M B	DESCRIPTION	-200 (%)	MC (%)	ATTER LIMI	BERG TS	K (FT./	ORG. CONT.
(11.)	L E	INCREMENT	FT.)		Ľ			· · ·		Pl	DAY)	(%)
0	ļ		<u> </u>		777	Brown clavev SAND ISCI						
] -	扠	1-2-2	4			Loose						
	K	2-2-2	4			Loose						
5-	X	2-3-2				··Loose					•••••••••••••	
	X	2-2-2	4			Loose			l			
] -	K	2-3-3	6]		Loose						
10	X	5-6-7	13	 		Medium						
-	1											
_						Green & orange CLAY ICH1, w/lenses of clavey			ļ			
- 15	X	2-3-5	8			sand						
						Boring terminated at 15'						
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PROJECT NO .: 70080-077-06 UNIVERSAL ENGINEERING SCIENCES REPORT NO .: 385573 **BORING LOG** PAGE: C-50 A-49 1 of 1 WAL * MART STORE TRACKING NO. 3873-00 SHEET: BORING DESIGNATION: PROJECT: TOWNSHIP: 8S RANGE: 18E S.E. CORNER OF I-75 & U.S. HIGHWAY 441 SECTION: 16 ALACHUA, ALACHUA COUNTY, FLORIDA 2/4/05 CPH ENGINEERS, INC. GS ELEVATION(ft): 95.10 DATE STARTED: CLIENT: DATE FINISHED: 2/4/05 LOCATION: SEE BORING LOCATION PLAN WATER TABLE (ft): NE R. WOODARD DATE OF READING: NA DRILLED BY: REMARKS: EST. WSWT (ft): TYPE OF SAMPLING: ASTM D-1586 NA

DEPTH	S A M P	BLOWS PER 6"	N (BLOWS/	w. т.	S Y M B	DESCRIPTION	-200 (%)	MC (%)	ATTER LIMI	BERG TS	K (FT./	ORG. CONT.
(11)	L E	INCREMENT	FT.)	ļ	L L				LL	PI	DAT)	(%)
0 - -		WOH WOH-1-1	WOH 2			Brown clayey SAND [SC] Very loose Very loose	~		~			
5-		4-1+2 2-2-2 2-2-2 4-4-4	4 4 8			···Very loose Very loose Very loose gray & orange very clayey sand Loose						
		3-3-5	8			Green, orange & gray CLAY [CH] Medium Boring terminated at 15'						
					and and a second second second second second second second second second second second second second second se							

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UNIVERSAL ENGINEERING SCIENCES BORING LOG

PROJECT NO .:	70080-077-06
REPORT NO .:	385573
PAGE:	C-51

PROJECT: WAL★ MART STORE TRACKING NO. 3873-00 S.E. CORNER OF I-75 & U.S. HIGHWAY 441 ALACHUA, ALACHUA COUNTY, FLORIDA

CLIENT: CPH ENGINEERS, INC.

LOCATION: SEE BORING LOCATION PLAN REMARKS: OFFSET 30' SOUTHEAST (NO ACCESS)

BORING DESIGNATIC SECTION: 16	DN: A- TOWNSH	50 11P: 88	SHEET: RANGE:	1 of 1 18E
GS ELEVATION(ft):	125.50	DATE STAR	TED:	2/7/05
WATER TABLE (ft):	3	DATE FINIS	HED:	2/7/05
DATE OF READING:	2/8/05	DRILLED BY	<u>':</u>	J. STILLSON
EST. WSWT (ft):	NA	TYPE OF SA	MPLING:	ASTM D-1586

DEPTH (FT.)	S A M P 1	BLOWS PER 6"	N (BLOWS/	w.t.	S Y B O	DESCRIPTION	-200 (%)	MC (%)	ATTER LIMI	BERG TS	K (FT./ DAY)	ORG. CONT. (%)
	Ē				Ľ					PI		
0						Brown SAND [SP]						
	\mathbb{X}	2-2-2	4			Very loose	1					
-	Ķ	1-2-2	4	-		Very loose gray & orange clayey SAND [SC]	1		-			
5-	Ŕ		····5····· _							•••••	••••••	
-	\Diamond	2-2-3	5			Loose Gray & orange very clayey						
	段	4-5-6	11			Medium light brown SAND [SP]						
10-	_	••••••			772	Cray player SAND (SC)						
-						Giay clayey on the [50]						
- 15	\mathbf{X}	2-2-2	4			Very loose						
- כו									ļ			
	1											
- 20 —	X	2-6-7	13			Medium					• • • • • • • • • • • • • • • • • • • •	
	-											
25	K	3-6-6	12	 		Stin green signity sandy CLAY [CH]						
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PROJECT NO .: 70080-077-06 UNIVERSAL ENGINEERING SCIENCES REPORT NO .: 385573 **BORING LOG** PAGE: C-52 A-51 1 of 1 WAL★ MART STORE TRACKING NO. 3873-00 BORING DESIGNATION: SHEET: PROJECT: TOWNSHIP: 8S RANGE: 18E S.E. CORNER OF I-75 & U.S. HIGHWAY 441 SECTION: 16 ALACHUA, ALACHUA COUNTY, FLORIDA CPH ENGINEERS, INC. GS ELEVATION(ft): 106.70 DATE STARTED: 1/27/05 CLIENT: 1/27/05 WATER TABLE (ft): NE DATE FINISHED: LOCATION: SEE BORING LOCATION PLAN DATE OF READING: NA DRILLED BY: M. BOATRIGHT REMARKS: EST. WSWT (ft): TYPE OF SAMPLING: ASTM D-1586 NA

DEPTH	A M P	BLOWS PER 6"	N (BLOWS/	W.T.	Y M B	DESCRIPTION	-200 (%)	MC (%)	ATTER LIM	BERG TS	К (FT./	ORG. CONT.
(1.1.)	L E	INCREMENT	FT.)		0 L		(10)	(10)	LL	PI	DAY)	(%)
0-	 		·		1	Brown SAND (SP)						
	\mathbf{X}	1-2-4	6		777	Loose brown clavey SAND (SC)	{		1			
-	Ŕ	5-5-5	10			Loose			-			
5-	X		····g····		///	·· Loose dark brown			••••••			
	Ŕ	5-7-7	14			Medium brown & gray slightly clayey SAND [SM]						
-	\mathbf{X}	2-3-3	6			Green & orange CLAY, w/trace of sand [CH]						
- 10	Х	3-4-7	11			Stiff						
- 10												
						Sandy						
	\bigtriangledown	3-4-6	10			Stiff						
15-				1		Boring terminated at 15'						
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		PR	PROJECT NO.: 70080-077-06									
			UN	IVEr	SAL ENGINEERING 3	CIENCES		RE	PORT N	10.:	385573	
					BORING LOG			PA	GE:		C-53	
PROJECT:	WAL + MAR S.E. CORNE ALACHUA, A	T STORE R OF I-75 ALACHUA	TRAC 5 & U.: COU	CKING S. HIGI NTY, F	NO, 3873-00 HWAY 441 LORIDA	BORING DESIGNATION: A-52 SHEET: 1 OF 1 SECTION: 16 TOWNSHIP: 8S RANGE: 18E						
CLIENT:	CPH ENGIN	EERS, IN	C.			GS ELEVATION(ft)	: 102.7	0 DA1	FE STAR	TED:	1/31/	05
LOCATION:	SEE BORIN	G LOCAT	ION P	LAN		WATER TABLE (ft)	: NE	DAT	re finis	HED:	1/31/	05
REMARKS:						DATE OF READIN	G: NA	DRI	LLED B	Y:	G. W	HITAKER
						EST. WSWT (ft):	NA	TYF	PE OF S	AMPLII	NG: ASTN	A D-1586
DEPTH M (FT.) L E	BLOWS PER 6" INCREMENT	N (BLOWS/ FT.)	W,T.	S Y B O L	DESCRIPTION		-200 (%)	MC (%)	ATTER LIMI LL	BERG ITS PI	K (FT./ DAY)	ORG. CONT. (%)
0				777	Brown clavey SAND [SC]							
	1-2-3	5			Loose brown very clayey							
	2-2-2	4			Very loose				-			
5		10		1.4.1.	···Loose Medium green & orange CLAY IC							
	2-3-4	7			Modium groon a orango on ni jo	1	87					
	4-5-7	12			Stiff							
10	5-6-6	12			Stiff			•••••				· · · · · · · · · · · · · · · · · · ·
				V////								

<u>ئا_</u>									•		
]	入 2-2-2	4		//	Very loose			-			
5	XI].[.]	·· Loose			•••••			•••••
	\exists			11/1/	Medium green & orange CLAY [CH]	07					
	△ 2-3-4	7				0/					
	X 4-5-7	12			Stiff						
_*					049						
10-4	△ <u>5-6-6</u>	12			Sun	•••••	•••••	• • • • • • • • • • •	•••••	••••	
4											
4											
-				111	Lease light gray clayey SAND (SC)						
15 - 	4		•••••		Boring terminated at 15'				•••••		• • • • • • • • • • • • • • •
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UNIVERSAL ENGINEERING SCIENCES BORING LOG

PROJECT NO .:	70080-07	7-06
REPORT NO .:	385573	
PAGE	C-54	

PROJECT: WAL★ MART STORE TRACKING NO. 3873-00 S.E. CORNER OF I-75 & U.S. HIGHWAY 441 ALACHUA, ALACHUA COUNTY, FLORIDA

CLIENT: CPH ENGINEERS, INC.

LOCATION: SEE BORING LOCATION PLAN REMARKS:

BORING DESIGNATIC SECTION: 16	N: A-	53 IIP: 85	SHEET: RANGE:	1 of 1 18E
GS ELEVATION(ft):	99.10	DATE STAR	TED:	2/2/05
WATER TABLE (ft):	11	DATE FINIS	HED:	2/2/05
DATE OF READING:	2/3/05	DRILLED BY	':	J. STILLSON
EST. WSWT (ft):	NA	TYPE OF SA	MPLING:	ASTM D-1586

DEPTH (FT.)	SAMPLE	BLOWS PER 6" INCREMENT	N (BLOWS/ FT.)	w.т.	3YMBOL	DESCRIPTION	-200 (%)	MC (%)		BERG TS	K (FT./ DAY)	ORG. CONT. (%)
0						Brown SAND [SP]						
-	X	1-2-1	3			Very loose brown slightly clayey SAND [SM]						
-	X	1-2-3	5			Loose brown clayey SAND [SC]			-		~ ·	
5-	Ô		9									
-	\ominus	3-3-5	8			Loose brown & gray						
-	\bigotimes	3-3-3	6			Loose						
10	ightarrow	2-2-2			117	Very loose brown & gray very clavey	• • • • • • • • • • • • • • •		• • • • • • • • • • •		•••••	
-				_		Gray & orange sandy CLAY [CH]						
-	$\overline{\nabla}$											
15	Å	4-5-6	11			Stiff		· · · · · · · · · · · · · · · · · · ·	h	•••••	· · · · · · · · · · · · · · ·	
						Boring terminated at 15						:
								-				
											•	

2				UN	IVEF	SAL ENGINEERING S BORING LOG		PR RE		NO.: 1	70080-077 385573	-06	
Supplementation of the second s	PROJECT:	WAL * MAR S.E. CORNE	T STORE	TRAC 5 & U.S	KING 3. HIGI	NO. 3873-00 HWAY 441	BORING DESIGNA SECTION: 16	TION: TOV	P-10 WNSHIP:	85	SHEE	т: 10 БЕ: 18Е	f 1 [.]
нологиянанананананананананананананананананана	CLIENT: LOCATION: REMARKS:	ALACHUA, A CPH ENGIN SEE BORIN	EERS, IN G LOCAT	COUI C. ION P	LAN	LORIDA	GS ELEVATION(ft): WATER TABLE (ft): DATE OF READING EST. WSWT (ft):	90.80 NE 6: NA NA	DAT DAT DRI TYF	TE STAR TE FINIS LLED B ^N PE OF S/	TED: HED: /: \MPLIN	1/24/0 1/24/0 M. BC IG: ASTM	05 05 0ATRIGHT 1 D-1586
ад 2000 на полото на полото на полото на полото на полото на полото на полото на полото на полото на полото на	DEPTH M (FT.) P E	BLOWS PER 6" INCREMENT	N (BLOWS/ FT.)	w.т.	S Y B O L	DESCRIPTION		-200 (%)	MC (%)	ATTER LIMI LL	BERG TS PI	K (FT./ DAY)	ORG. CONT. (%)
	0-	2-3-4	7			Brown SAND [SP]		<u>-</u>					
St. early a constrained of the second s	5	2-2-2 	4			Light brown Very loose brown clayey SAND [S ·· Loose gray & taп.::	5C]					.	
and the second sec		4-4-5 6-6-7 	13 14			Stiff green & tan CLAY [CH] Medium light green & brown sligh [SM]	tly clayey SAND					······································	
gA construction and the second se	15	2-3-5	8			Loose tan & orange						· · · · · · · · · · · · · · · · · · ·	
		3-4-4	8			Light gray & orange clayey SAND) [SC]	27				2	
						Light green & orange		2					
All the second sec	25	2-2-2	4			Light green & orange		-			· · · · · · · · · · · · · · · · · · ·	* * * * * * * * * * * * * * * *	
	30 - - -	2-2-3	5			Loose Tan & orange							
	35	3-4-3	7	******		Loose Tan, gray & orange							
	40	3-2-3	5			Loose Boring terminated at 40'		·					
			-										
Sector Sect							-					ţ	
A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR A CONTRAC													
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							·		PI	ROJECT	NO.:	70080-077	-06
				UNI	VEF	RSAL ENGINEERING	SCIENCES		R	EPORT N	10.: :	385573	′
						BORING LOG			PA	AGE:		 C-113	
Tanang (1990)	PROJECT:			TRAC	KING	NO. 3873-00 HWAY 441	BORING DESIGN	ATION: TOW	P-11 (NSHIP:	8S	SHEE	т: 1 с Е: 18Е	of 1
and a second second		ALACHUA, /	ALACHUA		NTY, F	LORIDA							
	CLIENT:	CPH ENGIN	EERS, IN	IC.	AN		GS ELEVATION(ft): 97.40	DA	TE STAF	RTED:	1/24/ 1/24/	05 05
and a second sec	REMARKS:	SEE BORIN	GLOCAI		-7119		DATE OF READIN	IG: NA	DR	ILLED B	Y:	R. W	OODARD
							EST. WSWT (ft):	NA	ΤY	PE OF S	AMPLIN	IG: ASTI	1 D-1586
Kadanan Internet	DEPTH M	BLOWS PER 6"	N (BLOWS/	w.т.	S Y M B	DESCRIPTION		-200	MC (%)		BERG	K (FT./	ORG. CONT.
	(FT.) F E	INCREMENT	`FT.)		Õ L			(76)	(70)	LL	PI	DAY)	(%)
	0					Dark brown SAND [SP-SM]		<u> </u>		<u> </u>			
)		1-1-1	2			Very loose dark brown							
		2-2-3	5			Loose brown							
	5-X	4_3_4	7			10050							
y Kathanan Katalogi kathanan		5-6-5	11			Medium brown clayey SAND [SC]						-
1	10	6-7-7	14			Stiff light green, gray & orange s	andy CLAY [CH]						
<i>[</i>]	-							.					
	-												
	15	2-4-4	8			Medium				+			
Sector Constraints	_				[[[[Light brown & orange clayey SAI	ND [SC]			-			
ē		3-3-3	6			Loose							
	20					Light green & orange							
						, ,		•					
	25	2-2-3	5		///	Loose	•••••••••••						
ga ⁿ ana sa sa sa						Ten CAND with and a false (CD	CM3						
						Tan SANU, whenses of clay [SP-	5101]						
	30	1-2-2	<u>4</u>	•••••		Very loose		•••••		+	•••••		
	_												
Solution and the solution of t		1-1-2	3			Very loose tan		15					
1.1		.											
$\langle 1 \rangle$													
	40 - X	1-1-1	2			Very loose Boring terminated at 40'		••••••					
61						Dornig terminated at 40		`.					
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in a second													
		<u>[</u>		L				Ļ!		<u></u>	1		ل ـــــــا

AND				UN	IVEF	RSAL ENGINEERING S	CIENCES		Př Ri		NO.: IO.:	70080-077	-06
granica and						BORINGLOG			PA	AGE:		C-114	
Support Sup	PROJECT:	WAL * MAR S.E. CORNE ALACHUA, /	T STORE R OF I-75 ALACHUA	TRAC 5 & U.S	KING S. HIGI NTY, F	NO. 3873-00 HWAY 441 FLORIDA	BORING DESIGNA SECTION: 16	TION: TOV	P-12 vnship:	8S	SHEE	:T: 10 SE: 18E	f 1
A A A A A A A A A A A A A A A A A A A	CLIENT:	CPH ENGIN	EERS, IN	C.			GS ELEVATION(ft)	: 92.70	DA	TE STAR	TED:	1/21/	05
(** *)	LOCATION:	SEE BORIN	G LOCAT	ION P	LAN		WATER TABLE (ft)	: NE	DA	TE FINIS	HED:	1/21/	D5
a 12 for a 12 for a	REMARKS:						EST, WSWT (ft):	G:NA NA	UR TYI	PEOFS	r: AMPLII	J. ST NG: ASTN	1 D-1586
\$ ~~s					S		· ·				PERO		
Arran ar arrange Arran ar ar arrange Arran ar ar ar ar ar ar ar ar ar ar ar ar ar	DEPTH M (FT.) P E	BLOWS PER 6" INCREMENT	N (BLOWS/ FT.)	W.Т.	Y M B O L	DESCRIPTION		-200 (%)	MC (%)			K (FT./ DAY)	ORG. CONT. (%)
	0- -					Brown SAND [SP-SM]		<u> </u>		<u> </u>			
		2-1-1 1-2-2	2 4			Very loose dark brown to orange. Very loose Very loose							
	5	····2-3-4····		•••••		Loose brown & light green clayey	SAND [SC]						
51		3-4-5 3-3-3	9		$\overline{7}$	Loose light brown & orange slight	ly clayey SAND			******			
anto en contra la contra la contra la contra la contra la contra la contra la contra la contra la contra la con El contra la contra la contra la contra la contra la contra la contra la contra la contra la contra la contra la El contra la contra la contra la contra la contra la contra la contra la contra la contra la contra la contra la		3-4-3	7			[SM] Loose							
	- 10	•											
A						Tan to white SAND [SP]							
÷	15	5-6-6	12			Medium							
2000 A								-					
		5-5-6	11			Orange & gray slightly clayey SAI	ND [SM]						
	20			•••••			,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,		,				
						Gray & orange clayey SAND [SC]							
(°)	25	3-4-4	8			Loose		23	• • • • • • • • • • • • • • • • • • • •				
								-					:
£ \$			_			Loose gray							
	30	1-2-3	5	·····					••••	•			
5 2						Tan LIMESTONE							
	35	11-17-25	42									. <i></i>	
i, pri													
geonadaarda alaa ahaan													
and a second sec	40	20-25-19				Boring terminated at 40'		······	•••••				
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62.0										ļ			
6						·····							

			00151050		PR	OJECT NO.:	70080-071	7-06
2.3		UNIVERSAL ENGINEERING	SCIENCES		RE	PORT NO .:	385573	
de la construcción de la		BORING LOG			PA	GE:	C-115	
instruction instr	PROJECT:	WAL★ MART STORE TRACKING NO. 3873-00 S.E. CORNER OF I-75 & U.S. HIGHWAY 441 ALACHUA, ALACHUA COUNTY, FLORIDA	BORING DESIGNA SECTION: 16	TION: TOV	P-13 WNSHIP:	SHEE 8S RANC	ett: 1 C GE: 18E	of 1
	CLIENT:	CPH ENGINEERS, INC.	GS ELEVATION(ft)	: 89.00	DAT	FE STARTED:	1/21/	05
şş	LOCATION:	SEE BORING LOCATION PLAN	WATER TABLE (ft)	: NE	DAT	FE FINISHED:	1/24/	05
And an and a second second	REMARKS:		DATE OF READIN	G: NA	DRI	LLED BY:	R. W	OODARD
9479-1- 			EST. WSWT (ft):	NA	TYF	PE OF SAMPLIN	NG: ASTI	VI D-1586
Barran and Statements	DEPTH M (FT) P	BLOWS N Y PER 6" (BLOWS/ W.T. B DESCRIPTIC	N	-200 (%)	MC (%)	ATTERBERG LIMITS	K (FT./	ORG. CONT,

gytefny contrast of the second

	DEPTH	BLOWS PER 6"	N (BLOWS/	W.T.	S Y N B	DESCRIPTION	-200	MC (%)	ATTER LIM	BERG ITS	К (FT./	ORG. CONT.
•	(FI.) L E	INCREMENT	FT.)		Ō L		(70)	(70)	LL.	PI	DAY)	(%)
чинин на на на на на на на на на на на на на	0	1-1-1	2 .			Brown SAND [SP-SM] Very loose	~~~~					
		1-1-2	3			Very loose dark brown to orange						,
()		3-3-3	6			[SC] Loose						
And the second sec	-X 10-X	3-3-2 3-4-5	5 9			Loose light brown & tan						
500 - 100 -		4-5-6	11			Medium						:
Constant and the second s			,			Brown, gray & tan						
9 9 1 1 1 1 1 1 1 1 1 1	20 - X	2-3-4	7			Loose	, ,	••••••	,			
ар <mark>ит Че</mark> линин колон кале 2 2 с. с. с. с. с. с. с. с. с. с. с. с. с.	25 – X						-	,,,		• • • • • • • •		
	- 	8-15-17										
nang V		22-30-25	55									
Annual Annual												
	40	.14-25-26	<u>5</u> 1			Boring terminated at 40'	· · · · · · · · · · · · · · · · · · ·					
Sector Annual Sect												

		-					······································			PR	OJECT	NO.:	70080-077	7-06
					UN	IVEF	RSAL ENGINEERING S	SCIENCES		RE	PORT	10.:	385573	
							BORING LOG			PA	GE:		C-116	
annan an the second second second second second second second second second second second second second second	PROJECT:		WAL * MAR	T STORE	. TRAC 5 & U.(King S. Hig	NO. 3873-00 HWAY 441	BORING DESIGNA SECTION: 16	TION: TOV	P-14 vnship:	8S	SHEE	ET: 10 GE: 18E	of 1
	CLIENT:		CPH ENGIN	EERS, IN	IC.	NTY, F		GS ELEVATION(ft)	: 94.70	DAT	E STAR	TED:	1/25/	05
	LOCATION	1:	SEE BORIN	G LOCAT	'ION P	LAN		WATER TABLE (ff)	: NE	DAT	E FINIS	HED:	1/25/	05
AND STOCK STOCK	REMARKS	:					¢		G: NA			Y: Amplii	R.W	OODARD
		- C 1		1			-							
na na na na na na na na na na na na na n	DEPTH (FT.)	AMPLE	BLOWS PER 6" INCREMENT	N (BLOWS/ FT.)	W.T.	M B L	DESCRIPTION		-200 (%)	MC (%)		BERG TS	K (FT./ DAY)	ORG. CONT. (%)
	0-	-				- 125	Brown to orange SAND wilenses	of clay [SP_SM]						
		X	1-1-1	2			Very loose	of clay [or-ow]						
		X	1-0-1	1			Very loose							
	5-	X	····· 1-0-0 ····	0			···Very loose			********			•••••	
		\exists	1-0-1 1-1-1	1			Very loose Verv loose							
strans. Marine	10	Ż	1-1-1	2	ļ		Very loose					.	·····	
11-1							Brown clayey SAND [SC]	<u></u>						
1.010.00	15 —	Ą	2-3-4	7			Loose				ļ		·····	
New Programme							Light green, gray & orange sandy	CLAY [CH]						
ا		X	3-5-6	11			Stiff							
	20													
			:				Gray & orange clayey SAND [SC]							
	25 -	Д	4-5-6				Medium			· · · · · · · · · · · · · · · · · · ·				
									-					
		\forall	0.4 5											
	30 —		3-4-5				Loose			,				
7 13			·				Light green & orange							
North Street and Street	35-	X	3-4-5	9	 		Loose					 	•••••	
~.÷₽														
		$ \rightarrow $					Tan & orange SAND, w/ienses of	clay [SP]						
i	40-	Д	2-3-4	7		<u> </u>	Loose Boring terminated at 40'	·······						· · · · · · · · · · · · · · · · · · ·
and and and and and and and and and and														
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	V		•	UN	IVEF	RSAL ENGINEERING S BORING LOG	SCIENCES		PR RE PA		NO.:	70080-077 385573 C-117	7-0 6
	PROJECT:	WAL★ MAR S.E. CORNE ALACHUA, A	T STORE	TRA0 5 & U.	CKING S. HIG NTY, F	NO. 3873-00 HWAY 441 ELORIDA	BORING DESIGNA SECTION: 16	ATION: TOV	P-15 VNSHIP:	8S	SHEE	T: 1 C E: 18E	of 1
in the second seco	CLIENT: LOCATION: REMARKS:	CPH ENGIN	EERS, IN G LOCAT	C. ION P	LAN		GS ELEVATION(ft) WATER TABLE (ft) DATE OF READIN EST. WSWT (ft):): 90.60): NE G: NA NA	DA ⁻ DA ⁻ DRI TYF	TE STAF TE FINIS ILLED B PE OF S.	RTED: SHED: Y: AMPLIN	1/21/ 1/21/ J. ST NG: ASTM	05 05 ILLSON A D-1586
	DEPTH M (FT.) L E	BLOWS PER 6" INCREMENT	N (BLOWS/ FT.)	w.т.	S Y M B O L	DESCRIPTION		-200 (%)	MC (%)	ATTER LIMI LL	BERG ITS PI	K (FT./ DAY)	ORG. CONT. (%)
		2-2-1 1-2-1	3 3			Brown to orange SAND [SP] Very loose Very loose							
,			2 2 2 4			Very loose Very loose Very loose Very loose			*****				
generation contained and the second		5-7-7	14			Gray & orange clayey SAND [SC Medium					· · · · · · · · · · · · · · · · · · ·		
And And And And And And And And And And	20	3-5-7	12			Medium					- 1		
And a second sec		4-5-7	12			Medium		-					
	30 – X	3-4-5	9	••••••		Loose tan to white slightly clayey	SAND [SM]	· • • • •					
Sector and a sector and a sector and a sector a	35		11			Stiff orange & gray CLAY [CH], w trace of limestone fragments	/lenses of sand &						
pinteresting and the second	40	2-2-2	4			Soft Boring terminated at 40'				3 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2		••••••••••••••••••••••••••••••••••••••	
							÷.						
And the second se													

				UN	IVEF		CIENCES		PF RE		NO.: 10.:	70080-077 385573	7-06
						BURINGLUG			PA	GE:		C-118	
	PROJECT:	WAL ★ MAR S.E. CORNE	T STORE	TRAC 5 & U.S	XING 3. HIGI NTY, F	NO. 3873-00 HWAY 441 LORIDA	BORING DESIGNA SECTION: 16	TION: TOV	P-16 VNSHIP:	8S	SHEI RAN(ET: 1 C GE: 18E	of 1
	CLIENT:	CPH ENGIN	IEERS, IN	C.			GS ELEVATION(ft)	: 88.20	DA	TE STAF	RTED:	1/21/	05
7	LOCATION:	SEE BORIN	G LOCAT	ION P	LAN		WATER TABLE (ft)	: NE	DA	TE FINIS	SHED:	1/21/	05
200 ₀₀	REMARKS:						DATE OF READING	G: NA	DR	ILLED B	Y:	R. W	OODARD
							EST. WSWT (ft):	NA	TYI	PE OF S	amplii 	NG: ASTI	√I D-1586
	DEPTH M (FT.)	BLOWS PER 6"	N (BLOWS/	w.т.	S Y M B	DESCRIPTION		-200 (%)	MC (%)	ATTER LIM	BERG	K (FT./	ORG. CONT.
	Ε	INCREMENT	F1.)		L					LL	PI		(70)
	0		<u> </u>	<u> </u>		Brown SAND trace of clay ISP-SI	M1		<u> </u>		<u> </u>		<u> </u>
		1-1-1	2			Verv loose]						
· 		1-1-2	3	-		Very loose dark brown to orange.	••						
	5-X	1 1-2				···Very loose					·····	• • • • • • • • • • • • •	•••••••••••••••••••••••••••••••••••••••
~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	-12	2-1-2	3		. //	Very loose							
Professional Street Street	┃ -⊻	2-2-2	4			Very loose					1		1
 , .		3-4-4	8	<b> </b>		Very loose			· · · · · · · · · · · · · · · ·		ļ		
						Light brown & tan	~						
' 3	15-	3-3-4	7	<b> </b> ;	///	Loose light brown & tan clayey SA	ND [SC]		•••••	. <b> </b> .	ł		
										-			
·)	20 -	3-3-4	7	 		Loose				<b>.</b>	<b>.</b>	3	
						Light green, orange & gray		د					
3	I 7X	3-4-6	10	1	レノイ	Loose				ł	1	l	.l <i></i> .

Tan LIMESTONE

Boring terminated at 40'

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4-7-23

3-2-3

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					PROJECT N	0.: 70080	0-077-06
					REPORT NO	).: 38557	73
		BORING L	OG		PAGE:	C-119	•
	PROJECT:	WAL★ MART STORE TRACKING NO. 3873-00 S.E. CORNER OF I-75 & U.S. HIGHWAY 441 ALACHUA, ALACHUA COUNTY, FLORIDA	BORING DESIGNATION SECTION: 16	on: P- towns	-17 HIP: 8S	SHEET: RANGE:	1 of 1 ^{18E}
.)	CLIENT:	CPH ENGINEERS, INC.	GS ELEVATION(ft):	93.50	DATE START	ED:	1/25/05
(*** <b>)</b>	LOCATION:	SEE BORING LOCATION PLAN	WATER TABLE (ff):	NE	DATE FINISH	ED:	1/25/05
	REMARKS:		DATE OF READING:	NA	DRILLED BY:		R. WOODARD
()			EST, WSWT (ft):	NA	TYPE OF SAI		ASTM D-1586
(*******)	SA	BLOWS N Y		202	ATTERB		ORG.

0.13    bit MOREMENT    PT )    Q    Cold    Cold    Cold    Cold    Cold    Cold    Cold    Cold    Cold    Cold    Cold    Cold    Cold    Cold    Cold    Cold    Cold    Cold    Cold    Cold    Cold    Cold    Cold    Cold    Cold    Cold    Cold    Cold    Cold    Cold    Cold    Cold    Cold    Cold    Cold    Cold    Cold    Cold    Cold    Cold    Cold    Cold    Cold    Cold    Cold    Cold    Cold    Cold    Cold    Cold    Cold    Cold    Cold    Cold    Cold    Cold    Cold    Cold    Cold    Cold    Cold    Cold    Cold    Cold    Cold    Cold    Cold    Cold    Cold    Cold    Cold    Cold    Cold    Cold    Cold    Cold    Cold    Cold    Cold    Cold    Cold    Cold    Cold    Cold    Cold    Cold    Cold    Cold		DEPTH	S A M P	BLOWS PER 6"	N (BLOWS/	w.т.	S Y M B	DESCRIPTION	-200 (%)	MC (%)	ATTERI LIMI	BERG TS	K (FT./	ORG. CONT.
0	(	(( ( )	E	INCREMENT	FT.)		O L				LL	Pl	DAT)	(%)
1-1-1  2  User locating to other best of the other best of the other best of the other best of the other best of the other best of the other best of the other best of the other best of the other best of the other best of the other best of the other best of the other best of the other best of the other best of the other best of the other best of the other best of the other best of the other best of the other best of the other best of the other best of the other best of the other best of the other best of the other best of the other best of the other best of the other best of the other best of the other best of the other best of the other best of the other best of the other best of the other best of the other best of the other best of the other best of the other best of the other best of the other best of the other best of the other best of the other best of the other best of the other best of the other best of the other best of the other best of the other best of the other best of the other best of the other best of the other best of the other best of the other best of the other best of the other best of the other best of the other best of the other best of the other best of the other best of the other best of the other best of the other best of the other best of the other best of the other best of the other best of the other best of the other best of the other best of the other best of the other best of the other best of the other best of the other best of the other best of the other best of the other best of the other best of the other best of the other best of the other best of the other best of the other best of the other best of the other best of the other best of the other best of the other best of the other best of the other best of the other best of the other best of the other best of the other best of the other best of the other best of the other best of the other best of the other best of the other best of the other best of the other best of th		0					17	Brown to orange SAND w/lenses of clay [SP-SM]			<u></u>		<u> </u>	
WOH1  1  Very losse    1-1-1  2  Very losse    1-2-1  3  Very losse    1-1-1  2  Very losse    1-2-1  3  Very losse    1-2-1  3  Very losse    1-2-1  3  Very losse    1-2-1  3  Very losse    1-2-1  3  Very losse    1-2-1  3  Very losse    1-2-1  3  Very losse    1-2-1  2  Very losse    1-2-1  2  Very losse    1-2-1  2  Very losse    1-2-1  2  Very losse    1-2-2  44:3  7    1-2-4  10  Gray & orange sandy CLAY [CH]    30  -  1.2-4    30  -  1.2-4    30  -  1.2-4    30  -  3.4.6    10  3.4.6  10    35  -  10    36  -  2.4.6    10  - <td>: }</td> <td></td> <td>$\square$</td> <td>1_1_1</td> <td>2</td> <td></td> <td></td> <td>Very loose</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>	: }		$\square$	1_1_1	2			Very loose						
5	tin -		Ħ	WOH-1	1			Verv loose						
1-1-1  2  Very loses    10  1-1-1  2    10  1-1-1  2    10  1-1-1  2    10  1-1-1  2    10  1-1-1  2    10  1-1-1  2    11  2  Nery loses    10  1-1-1  2    11  2  Nery loses    11  2  Nery loses    12  4.5-5  10    15  4.5-5  10    16  4.5-5  10    17  Loses  Loses    20  -  4.5-5    10  Loses  34    21  3  5    10  Loses  34    21  3  5    32  2-+6  10    33  2-+6  10    18  Light green & tan clayey SAND [SC]    10  Light green & tan clayey SAND [SC]    10  Light green & tan clayey SAND [SC]    10  Loses		5-	X					··Verv loose		• • • • • • • • • • • • • • • • • • •				
1-2-1  3  Very losse    10  .1-1-1  2    15  .4.4.3  .7    15  .4.4.3  .7    16  .4.5.5  .10    17  .4.5.5  .10    18  .4.5.5  .10    19  .4.5.5  .10    10  .6058    20  .4.5.5    10  .6058    10  .6058    20  .4.5.5    10  .6058    20  .4.5.5    10  .6058    10  .6058    10  .6058    11  .6058    21  .3.5.5    10  .6058    10  .50ff    21  .3.4.6  .10    22  .1.2.4		-	X	1-1-1	2			Very loose						
10  1.1.1.  2.  Mery loose    15  .4.4.3.  .7.  Loose    20  .4.5.5.  .10.  Light brown to orange    20  .4.5.5.  .10.		-	M	1-2-1	3			Very loose						
10			$\square$	1-1-1	2			Very loose						
15		10						Brown & orange						
Light brown to orange 20 4.555 10. 25 3.555 10. 30 4.1-24. 30 4.1-24. 30 5.1.2-4. 40 5.1.10. Light green & tan clayey SAND [SC] Light green & tan clayey SAND [SC] Light green & tan clayey SAND [SC] Loose Boring terminated at 40'			Х	4-4-3	7	 		Loose						
20		- - -		455	10			Light brown to orange						
25  .3-5-5  .10		20 —	$\vdash$	4-0-0								• • • • • • • •		
25					10			Gray & orange clayey SAND [SC]	34			-	4	
30  -  .1-2-4.  .6.    35  -  .2-4-6.  .10.    35  -  .2-4-6.  .10.    Light green & tan clayey SAND [SC]  Losse    40  -  .3-4-6.    .10.  Boring terminated at 40'		25 —	K	3-5-5		·····		Loose						
30		-						Medium gray & orange sandy CLAY [CH]	-					
35  2-4-6  10  .Stiff    10  .Stiff  Light green & tan clayey SAND [SC]    40		- 30 —	Ж	1-2-4	6	<b>.</b>						•••••		
35	And a second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second sec	-		2-4-6	10			Stiff						
Light green & tan clayey SAND [SC] 40		35												
40  -10  Loose    Boring terminated at 40'	Scott and a second	-					[]]]	Light green & tan clayey SAND [SC]						
Boring terminated at 40'	1	40	K	3-4-6				Loose						
	A Lease and a lease and a lease and a lease and a lease and a lease and a lease and a lease and a lease and a lease and a lease and a lease and a lease and a lease and a lease and a lease and a lease and a lease and a lease and a lease and a lease and a lease and a lease and a lease and a lease and a lease and a lease and a lease and a lease and a lease and a lease and a lease and a lease and a lease and a lease and a lease and a lease and a lease and a lease and a lease and a lease and a lease and a lease and a lease and a lease and a lease and a lease and a lease and a lease and a lease and a lease and a lease and a lease and a lease and a lease and a lease and a lease and a lease and a lease and a lease and a lease and a lease and a lease and a lease and a lease and a lease and a lease and a lease and a lease and a lease and a lease and a lease and a lease and a lease and a lease and a lease and a lease and a lease and a lease and a lease and a lease and a lease and a lease and a lease and a lease and a lease and a lease and a lease and a lease and a lease and a lease and a lease and a lease and a lease and a lease and a lease and a lease and a lease and a lease and a lease and a lease and a lease and a lease and a lease and a lease and a lease and a lease and a lease and a lease and a lease and a lease and a lease and a lease and a lease and a lease and a le	-0						Boring terminated at 40'	-					
	( )													
	2.V)													
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<b>Annow The Vote State</b>				UN	IVEF		CIENCES	- <u></u>	PR RE	OJECT PORT N	NO.:	70080-077 385573	-06
11						BORINGLOG			PA	GE:		C-120	
SAMON	PROJECT:	WAL + MAR S.E. CORNE ALACHUA, A	T STORE ER OF 1-75 ALACHUA	TRAC 5 & U. COU	KING 5. HIG NTY, F	NO. 3873-00 HWAY 441 FLORIDA	BORING DESIGNA	ATION: TOV	P-18 WNSHIP:	88	SHEE RANC	:т: 1 с эЕ: 18Е	of 1
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	S DEPTH (FT.) E	BLOWS PER 6" INCREMENT	N (BLOWS/ FT.)	W.т.	S Y M B O L	DESCRIPTION	· ·	-200 (%)	MC (%)	ATTER LIMI LL	BERG TS	K (FT./ DAY)	ORG. CONT. (%)
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		2-1-1	2			Brown SAND [SP] Dark brown to orange							
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ATT CARLES		1-1-1 1-1-1	2			Very loose Very loose							
¢	10-7	1-2-2	4			Very loose	••••••	••••••		• • • • • • • • • • •		•••••••••••	••••••
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2 T 13	15 <del>- X</del>	2-2-2	4			Very loose gray & orange clayey	SAND [SC]			, , , , , , , , , , , ,			
A THE AREA CONTRACTOR		2				Gray		25				2	
	20	3-4-5	9			Loose					* * * * * * * * *	2	
····	25 – ×	4-6-11	17			· · · · · · · · · · · · · · · · · · ·		۔ ،					
()						Gray & orange		-					
	30	3-5-6	11			weaium	••••••••••••••••••••••••	•••••••		•••••			
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<u>.</u>	35-	4	····!/							••••••			
		4 7 10	17			Very stiff gray & orange sandy CL	AY [CH]						
e e e e e e e e e e e e e e e e e e e	40-	4 <u>4-/-1</u> U				Boring terminated at 40'							
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			L							PA	GE:		C-121	
	PROJECT	:	WAL + MAR S.E. CORNE ALACHUA, A	T STORE ER OF I-7: ALACHUA	: TRAC 5 & U.( \ COU[	CKING S. HIG NTY, F	NO. 3873-00 HWAY 441 CORIDA	BORING DESIGNA SECTION: 16	TION: TOV	P-19 VNSHIP:	8S	SHEE RANC	:T: 10 3E: 18E	if 1
	CLIENT:		CPH ENGIN	EERS, IN	IC.			GS ELEVATION(ft)	: 87.60	DAT	'E STAR	TED:	1/21/0	05
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umaan woodbe	REMARKS	5:							G: NA		LLED B	/: • • • • • •	R. W	
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Laboration and the second second second second second second second second second second second second second s	(FT.)	P L E	PER 6" INCREMENT	(BLOWS/ FT.)	W.T.	B O L	DESCRIPTION		(%)	(%)			(FT./ DAY)	CONT. (%)
And a second second second second second second second second second second second second second second second	0-	<u> </u>					Brown SAND [SP]		~~					
b 4	-	X	1-1-2	3			Very loose							
	-	X	1-2-1	3			Verv loose dark brown to orange	slightly clayey						
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ALC: A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR OF A CONTRACTOR A CONTRACTOR A CONTRACTOR A CONTRACTOR A CONT		Ø	1-2-1	3			Very loose							
V	10 —	A	1-2-2	4			Very loose					·····		
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(***)	-	$ \downarrow $			1		Light brown to tart slighly clayey	SAND [Sw]						
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terne 	PROJECT:	WAL★MAR S.E. CORNE ALACHUA, /	T STORE ER OF I-7 ALACHUA	TRAC 5 & U.9 ( COUI	KING 8. HIGI NTY, F	NO. 3873-00 HWAY 441 LORIDA	BORING DESIGNA SECTION: 16	TION: TOV	P-20 VNSHIP:	8S	SHEE RANC	T: 10 E: 18E	f 1
1,	CLIENT:	CPH ENGIN	EERS, IN	C.			GS ELEVATION(ft)	: 91.90	DAT	E STAR	TED:	1/24/	05
	LOCATION:	SEE BORIN	G LOCAT	ION PI	_AN		WATER TABLE (ft)	: NE G: NA	DAT DRI	E FINIS נופט B	HED: ':	1/24/ M. BC	D5 DATRIGHT
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	(FT.)	PER 6" INCREMENT	(BLOWS/ FT.)	W.T.	B O	DESCRIPTION		(%)	(%)	LL	PI	(FT./ DAY)	CONT. (%)
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		2-2-1	3			[SP-SM]							
		1-0-1	1			Nr. 1							
1		}·····1⊶1⊷∿····· ] ] 1-1-1	2			··· very loose							
gillermanning 1 5 6 (1) - ere o Voo		2-1-2	3			Very loose light brown			1				
	10	3-3-3	6			Loose brown & orange							• • • • • • • • • • • • • • •
						Loose brown	~						
÷)	15	4-4-3	7									••••••	
()		5-6-7	13			Stiff gray & orange sandy CLAY [	СН]						
i)						Stiff gray, orange & light green		÷					
	25	4-4-6	10						•••••		•••••		
61						Stiff light green & orange							
	30-X	5-6-6	12								•••••		
4	-		-			Stiff gray, tan & orange							
normality in the second		3-4-5	9										
i	35												
						Stiff brown, gray & orange							
(	40	3-5-6	11		-	Boring terminated at 40'			- • • • • • • • • • • • • • •		•••••		
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		1					BORING LOG			PA	GE:		C-123	
Summarian Anna Anna Anna Anna Anna Anna Anna A	PROJECT:		WAL ★ MART S.E. CORNE	T STORE	TRAC	KING 3. HIG NTY F	NO. 3873-00 HWAY 441 HORIDA	BORING DESIGNA SECTION: 16	TION: TOV	P-21 WNSHIP:	8S	SHEE	:T: <b>1</b> O ≩E: 18E	of 1
	CLIENT:	•	CPH ENGINI	EERS, IN	с.	,.		G\$ ELEVATION(ft)	: 87.80	DAT	E STAR	TED:	1/21/	05
( )	LOCATION	ł: :	SEE BORING	G LOCAT	ION P	LAN		WATER TABLE (ft)	: NE	DAT	E FINIS	HED:	1/21/0	05
	REMARKS	:						EST. WSWT (ft):	S: NA NA	TYP	E OF S	r: AMPLIN	J.ST NG: ASTN	/I D-1586
	DEPTH (FT.)	S A P L	BLOWS PER 6" NCREMENT	N (BLOWS/ FT.)	w.т.	S Y M B O	DESCRIPTION	· · · · · · · · · · · · · · · · · · ·	-200 (%)	MC (%)	ATTER LIMI	BERG TS	K (FT./ DAY)	ORG. CONT. (%)
		Ē				L						11		
	0 — - -		1-2-2 1-1-2	4			Brown fine SAND [SP-SM] Dark brown sand Very loose Very loose		Υ					
	5-	<u>.</u>	····≁-2-1·····	g			···Very loose dark brown to orange	···					•••••	
a		Ä	1-2-1	3			Very loose		:					
		$\exists$	1-2-2 1-2-3	4 5			Loose orange & gray clayey SAN	D [SC]						
· 1	10	<u></u> .												
		_												
/~* <b>a</b>	15	식.	5-6-6	12	ļ		Medium						•••••	
100	20	₫.	8-8-8		ļ		Medium							
	-						Medium gray & grange slightly cl	avev SAND [SM]						
erra			6-9-10	19			w/trace of limestone fragments	1909 OF 110 (0.012)						
	25 -	، الاست			1				-					
177 <b>1</b>						777	Medium gray & brown clayey SA	ND [SC], w/trace of						
	- 30	Щ.	6-10-10	20	••••••		limestone fragments	· · · · · · · · · · · · · · · · · · ·	••••	•••••			•••••	
s <b>1</b>							Tan LIMESTONE							
	35-	<u> </u>	14-14-15				•••••••••••••••••••••••••••••••••••••••						·	
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		S.E. CORNE ALACHUA, A	R OF I-7	5 & U.S \ COUN	8. HIGI NTY, F	HWAY 441 LORIDA	SECTION: 16		NSHIP:	8S	RANG	E: 18E	05
	CLIENT:		EERS, IN		A NI		GS ELEVATION(II):	86.90 NE	UAU TAU			1/21/	05
	REMARKS:	SEE BORING	GLOCAT		-An		DATE OF READING EST. WSWT (ft):	: NA NA	DRI TYF	LLED B	Y: AMPLIN	R.W G: ASTN	DODARD M D-1586
	DEPTH M (FT.) P E	BLOWS PER 6" INCREMENT	N (BLOWS/ FT.)	w.t.	S Y B O L	DESCRIPTION		-200 (%)	MC (%)	ATTER LIM LL	BERG ITS	K (FT./ DAY)	ORG. CONT. (%)
	0 —					Brown & tan SAND [SP]		-		<u> </u>	<u> </u>		

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	<u>م</u>												
£3	-	$\forall$	100				DIOWN & TAN SAIND [SP]						
<u> </u>	-	Ø	1-2-2	4			Very loose dark brown to grange		1	'			
	 	Ø	-2-1 \A/⊖H•	_{₩Ю} н		 	··Verv loose					•••••	
	-c	闵	1-1-1	2			Very loose						
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<u>8</u>	10 —	T				///	Very loose dark brown to orange clayey SAND [SC]						
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	-	团	3-3-4	7			Loose	23				3	
	15 —	۴Ì		[]									
	_	$\left  \right $				///	Brown, gray & orange						
	-	M	3-6-7	12			Medium						
	20 —	۴٩		!?				• • • • • • • • • • • •					
()	-			( )			Gray & orange sandy CLAY [CH]	,					
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	25 —	p	2-4-6	l10		1///	<u>, 900</u>		•••••	••••••	•••••		
£)	_						Grav & grange clavey SAND (SC)	-			1		
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	- 30	Å	5-9-9	18		///	Medium	···	·····		•••••		
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	-	Ľ					Tan & orange						
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Normal Street	PROJECT:		WAL + MAR S.E. CORNE	T STORE	TRAC 5 & U.(	KING S. HIGI	NO. 3873-00 HWAY 441	BORING DESIGNA SECTION: 16	TION: TOV	P-23 VNSHIP:	8S	SHEE	T: 10 E: 18E	f 1
	CLIENT: LOCATION REMARKS	4:	CPH ENGIN	EERS, IN	C. ION P	LAN		GS ELEVATION(ft) WATER TABLE (ft) DATE OF READING EST. WSWT (ft):	: 81.00 : NE G: NA NA	DAT DAT DRI TYF	TE STAR TE FINIS LLED B PE OF S	RTED: HED: Y: AMPLII	1/19/0 1/19/0 J.ST NG: ASTN	05 05 ILLSON M D-1586
Alaria - Caracey Ja	DEPTH (FT.)	SAMP.LE	BLOWS PER 6" NCREMENT	N (BLOWS/ FT.)	w. <b>r</b> .	%≻∑≊O∟	DESCRIPTION	]	-200 (%)	MC (%)	ATTER LIMI LL	BERG TS PI	K (FT./ DAY)	ORG. CONT. (%)
	0-						Brown fine SAND [SP]		····					
		X	10-10-10 8-9-7	20 16			Medium dark brown to orange sli [SM]	ghtly clayey SAND						
	5-	XI.	····2+2+2····	·····4····	•••••		Very loose dark brown to orange.	Clayey SAMD ISCL			•••••			
			2-3-5 4-4-5 4-5-6	9			Loose gray & orange Medium						*******	
	10		4 5 7	40			Na dium	,						
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Concentration of the second second second second second second second second second second second second second	20 —	Δ.	5-6-7	<u>13</u>			Medium						••••••	
	_ 	Χ.	7-12-19											
							Medium orange clayey SAND [S0	3	-					
Second Second	30 —	<u></u> .	4-7-8	15	•••••		Tan weathered I IMESTONE							
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	(FT.) F L E	INCREMENT	FT.)		B O L			(%)	(%)	LL	PI	DAY)	(%)
	0			· · ·		Brown fine SAND [SP-SM]		۰					
5. "F		2-2-2	4			Dark brown to orange							
Provide Statement	5	2-3-3	6 			Loose							
		3-4-5	9			Loose	i						
A Minimuch and	-2	4-5-5	10			Loose							
1977-197	10-2	4-5-6	11		[]]	Medium Dark brown clayey SAND [SC]							
An units of the second of the fight						Medium gray & orange	×	28				2	
an second	15-	43-5-6	[]]	ł					• • • • • • • • • • • • •			<del>.</del>	• • • • • • • • • • • • • • • •
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- Charles	20	<u> </u>	!**	•••••									
And And And And And And And And And And		5-7-8	15			Light green & orange slightly clay	ey SAND [SM]	2			-		
A A A STORE	25-4	7	!¤										
() 		7				Very stiff gray CLAY [CH], w/trac fragments	e of limestone	-					
and a second second second	30	4-8-25	33		·····	Tan LIMESTONE	•••••					• • • • • • • • • • • • • • •	
	35	7-12-15		<b> </b>			•••••••••••••••••••••••••••••••••••••••						
ŕ													
		8-15-15	30	<b>.</b>									
£ ** \$						Boring terminated at 40'							
Contrast on the Contrast of State				-									
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alatan yang berarak													

					UN	IVEF	RSAL ENGINEERING S BORING LOG	CIENCES		PF RE PA	ROJECT EPORT N AGE:	NO.: 10.:	70080-077 385573 C-135	7-06
	PROJECT	•	WAL & MAR S.E. CORNE ALACHUA, /	T STORE ER OF I-7 ALACHU/	5 & U.( 0 & U.(	XING S. HIG NTY, F	NO. 3873-00 HWAY 441 'LORIDA	BORING DESIGN/ SECTION: 16	ATION: TOV	P-33 WNSHIP:	85	SHEI	ET: 1 C GE: 18E	of 1
- -	CLIENT: LOCATIO REMARKS	N: 3:	CPH ENGIN SEE BORIN	EERS, IN G LOCAT	IC. ION P	LAN		GS ELEVATION(ft WATER TABLE (ft DATE OF READIN EST. WSWT (ft):	): 79.50 ): NE G: NA NA	DA DA DRI TYF	TE STAR TE FINIS ILLED B PE OF SA	RTED: HED: Y: AMPLI	1/19/ 1/19/ J. ST NG: ASTI	05 05 ILLSON VI D-1586
	DEPTH (FT.)	SAMPLE	BLOWS PER 6" INCREMENT	N (BLOWS/ FT.)	′ w.т.	SY⊠®O∟	DESCRIPTION		-200 (%)	MC (%)	ATTER LIMI LL	BERG TS	K (FT./ DAY)	ORG. CONT. (%)
	0		4-4-4 4-5-6	8 11			Brown SAND [SP] Loose dark brown clayey SAND [ Loose Medium	SC]						
Millin, same a more AMING	5 - - - 10		6-7-8 6-8-10 6-9-11 6-11-11	15 18 20 22			Medium Medium light brown Medium Medium							
			4-7-6	13			. Medium tan to yellow very clayey.						1	
	  20	X	6-6-6	12			Tan weathered LIMESTONE			•••••				
		X	. 10-11-4	15					,	••••				
	- - - 30	X							-					
of factors and the address and the		X	10-12-15											
of children commune of the second	- - 40	X	12-20-20				Boring terminated at 40'						•••••	
of Without manufactor Westmann Marchide							-							
194946" Idon ( ^ 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1								<b>*</b>						
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толицияния 	5	1-2-2 1-2-2 3-4-4	·····4···· 4 8	   		Loose dark brown							
остория 2 - тр. dd		3-4-5	9			Stiff green & orange sandy CLAY	[CH]	•••••					
e de la construcción de la construcción de la construcción de la construcción de la construcción de la constru de la construcción de la construcción de la construcción de la construcción de la construcción de la construcción de la construcción de la construcción de la construcción de la construcción de la construcción de la construcción de la construcción de la construcción de la construcción de la construcción de la construcción de la construcción de la construcción de la construcción de la construcción de la construcción de la construcción de la construcción de la construcción de la construcción de la construcción de la construcción de la construcción de la construcción de la construcción de la construcción de la construcción de la construcción de la construcción de la construcción de la construcción de la construcción de la construcción de la construcción de la construcción de la construcción de la construcción de la construcción de la construcción de la construcción de la construcción de la construcción de la construcción de la construcción de la construcción de la construcción de la construcción de la construcción de la construcción de la construcción de la construcción de la construcción de la construcción de la construcción de la construcción de la construcción de la construcción de la construcción de la construcción de la construcción de la construcción de la construcción de la construcción de la construcción de la construcción de la construcción de la construcción de la construcción de la construcción de la construcción de la construcción de la construcción de la construcción de la construcción de la construcción de la construcción de la construcción de la construcción de la construcción de la construcción de la construcción de la construcción de la construcción de la construcción de la construcción de la construcción de la construcción de la construcción de la construcción de la construcción de la construcción de la construcción de la construcción de la construcción de la construcción de la construcci		4-5-8	13			Stiff light green & orange			· · · · · · · · · · · · · · · ·			•••••	
		4-4-5	ÿ			Medium orange & tan slightly clay	vey SAND [SM]					••••••	• • • • • • • • • • • • • • • • • • • •
			13	   				-					
Annuar Charles	30	4-6-8	14			Medium tan & orange clayey SAN	ID [SC]	~		· · · · · · · · · ·			
Annual Contraction of the second second second second second second second second second second second second s		- <del>4-9-</del> 8	1/			Medium gray, tan & orange						••••••	
	40	5-6-12				Boring terminated at 40'		· · · · · · · · · · · · · · · · · · ·				••••••	
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dia 17 dia 18	LOCATION:	SEE BORIN	G LOCAT	ION P	LAN		WATER TABLE (ft)	: NE	DAT	E FINIS	HED:	1/21/	05 U CON
and a second second second	REMARKS:						EST. WSWT (ft):	G: NA NA	DRI TYF	E OF S	Y: AMPLII	J.ST NG: ASTN	1 D-1586
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	DEPTH M (FT.) L E	BLOWS PER 6" INCREMENT	N (BLOWS/ FT.)	w.т.	Y M B O L	DESCRIPTION		-200 (%)	MC (%)			K (FT./ DAY)	ORG. CONT. (%)
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()		1-2-2	4			Very loose dark brown to orange. Very loose							
a Manadalla que		2-2-3	5			Loose							
	5X	4-4-4	8			loose			<u></u>				
345-11		3-4-7	11			Medium brown clayey SAND [SC]							
and a second second second second second second second second second second second second second second second	10	3-5-7	12			Medium			• • • • • • • • • • • • • • • • • • • •				
линаруучунаарум													
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(° - <b>)</b>						Orange clayey SAND [SC]		:					
San San San San San San San San San San	35	2-3-4	7	•••••		Loose							
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	CLIENT:	CPH ENGIN	EERS, IN	с.			GS ELEVATION(ft)	: 83.60	DAT	TE STAR	TED:	1/20/	05
All a second	LOCATION:	SEE BORIN	G LOCAT	ION PI	LAN	•	WATER TABLE (ft)	NE	DAT	TE FINIS	HED:	1/20/	05 III SON
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Shirthy assessment	0					Brown SAND (SP)			·····				
1}		2-2-3	5			Dark brown to orange clayey SAN	ID [SC]						
A A CONTRACTOR OF A CONTRACT	╡	2-3-3	6			Loose							
1999) 		3-4-5	9			Loose dark brown							
greeva maanooo		4-5-6	11			Medium							
A CLUS		5-6-6	12			Medium						* • • • • • • • • • • • • •	
						Madium and 9 around							
ŝ.,, <b>)</b>	15	4-6-8	14			wedium gray & orange	•						
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(c) (c)		5-6-7	13			Medium							
gift sommineerer V Ng 1 - Series - A				• • • • • • • •									
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	25	6-7-12	19			Tan LIMESTONE	••••••				·····		
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Sector											*********		
	40	8-10-21				Boring terminated at 40'							• • • • • • • • • • • • • • • •
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							BORING LOG	BORING LOG					PAGE: C-139				
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ð.,, <b>f</b>	CLIENT:	1.	CPH ENGIN	EERS, IN	C.	1 4 M		GS ELEVATION(ft): 78.90 DATE STARTED: WATER TABLE (ft): NE DATE FINISHED:						1/19/05 1/19/05			
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1222								EST. WSWT (ft):	NA	TYF	TYPE OF SAMPLING: ASTM D-1586						
	<b></b>	S A	BLOWS	N		S Y			200		ATTER	BERG	ĸ	ORG.			
	DEPTH (FT.)	M P L	PER 6" INCREMENT	(BLOWS/ FT.)	W.T.	BO	DESCRIPTION		-200 (%)	(%)		то Прі	(FT./ DAY)	CONT. (%)			
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	0						Brown SAND [SP] Very loose dark brown clavey SA	ND ISCI									
(***)		$\ominus$	2-2-2	4			Very loose										
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	–	Ą	3-4-4	8			Light gray & orange										
8 I	10 —	$\bigtriangleup$	3-5-7	12										•••••			
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						Tan to light green slightly clayey S	AND [SM]						
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2 A Vina mana ana ana ana ana ana ana ana ana	- - - 15 —	X	6-6-6	12			Tan to yellow slightly clayey SANI Medium	D [SM]					•••••	
		X	25-50/5"	50/5"			Tan LIMESTONE							
	- - 25 — - -	X	20-20-18						, 			· · · · · · · · · · · · · · · · · · ·		
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# **KEY TO BORING LOGS**

UNIFIED CLASSIFICATION SYSTEM



# RELATIVE DENSITY (sand-silt)

Very Loose - Less Than 4 Blows/Ft. Loose - 4 - 10 Blows/Ft. Medium - 10 to 30 Blows/Ft. Dense - 30 to 50 Blows/Ft. Very Dense - More Than 50 Blows/Ft.

## CONSISTENCY (clay)

Very Soft - Less Than 2 Blows/Ft. Soft - 2 to 4 Blows/Ft. Medium - 4 to 8 Blows/Ft. Stiff - 8 to 15 Blows/Ft. Very Stiff - 15 to 30 Blows/Ft. Hard - More Than 30 Blows/Ft.

N	AJOR DIVISI	ONS	GROUP Symbols	TYPICAL NAMES						
*	x	ELS F	GW	Well-graded gravels and gravel-sand mixtures, little or no lines						
SO siev	VELS more of traction n No. 4	CLE	GP	Poorly graded gravels and gravel-sand mixtures, little or no fines						
	O X S D	a T N	GM	Sility gravels, gravel-sand-silt mixtures						
MNED Med on	2, 6 K	GRAVI MT FINE	GC	Clayay gravels, gravel-sand-clay mixtures						
RSE-OP XX retai		NA	SW	Well-graded sands and gravelly sands, little or no lines						
COA then 50	ANDS hen 805 se facti No. 4 t	S C	SP	Poorly graded sands and gravelly sands, little or no fines						
More		Ô 두 있	SM .	Silty sands, sand-silt mixtures						
	2 4	3₹£	sc	Clayay sands, sand-clay mixtures						
	S.		ML.	Inorganic silts, vary fine sands, rock flour, silty or clayay fine sands						
LS 100 sieve*	a AND CL iquid limit	D% or leas	CL	Inorganic clays of low to medium plasticity, gravelly clays, sandy clays, silty clays, lean clays						
ED SOU		3	OL	Organic silts and organic silty clays of low plasticity						
NE-GRAIN	CLAYS	n 50%	мн	Inorganic silts, micaceous or diatomaceous fine sands or silts, elastic silts						
т Хо С	IS AND Llouid 1		СН	Inorganic clays or high plasticity, fat clays						
ъ 	큜	<b>e</b>	ГОН	Organic clays of medium to high plasticity						
H	ighly Organic S	alio	PT	Peat, muck and other highly organic soils						

Based on the meterial pasing the 3-in. (75-mm) slove.



#### **Field Exploration Procedures**

#### **Standard Penetration Test Borings**

The penetration borings were made in general accordance with the latest revision of ASTM D 1586, "Penetration Test and Split-Barrel Sampling of Soils". The borings were advanced by rotary drilling techniques using a circulating bentonite fluid for borehole flushing and stability. At 2 ½ to 5 foot intervals, the drilling tools were removed from the borehole and a split-barrel sampler inserted to the borehole bottom and driven 18 inches into the soil using a 140 pound hammer falling on the average 30 inches per hammer blow. The number of blows for the final 12 inches of penetration is termed the "penetration resistance, blow count, or N-value". This value is an index to several in-place geotechnical properties of the material tested, such as relative density and Young's Modulus.

After driving the sampler 18 inches (or less if in hard rock-like material), the sampler was retrieved from the borehole and representative samples of the material within the split-barrel were placed in plastic containers and sealed. After completing the drilling operations, the samples for each boring were transported to our laboratory where they were examined by our geotechnical engineer in order to verify the driller's field classification.

#### <u>Auger Borings</u>

The auger borings were performed mechanically by the use of a continuous-flight auger attached to the drill rig and in general accordance with the latest revision of ASTM D 1452, "Soil Investigation and Sampling by Auger Borings". Representative samples of the soils brought to the ground surface by the augering process were placed in plastic containers, sealed and transported to our laboratory where they were examined by our geotechnical engineer to verify the driller's field classification.

# APPENDIX D

Final Study Generalized Subsurface Profile Cross-Sections at Proposed Parking Lot Areas Cross-Sections at Proposed Building Footprint Cross-Sections at Proposed Retention Pond





















































# APPENDIX E

Summary of Classifications and Index Testing for Preliminary Study Laboratory Testing Procedures

# Summary of Classification and Index Testing for Preliminary Report

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Boring No.	Sample Depth, Ft.	Permeability (ft/day)	Fine Content (%)	Soil Description	Unified Soil Classification
B-1	0 to 2		58%	Very sandy Clay	СН
B-1	2 to 8.5		43%	Very clayey Sand	SC
B-1	15 to 17		94%	Clay	CH
B-1	41 to 45		73%	Sandy Clay	CH
B-2	6 to 8	<u></u>	89%	Sandy Clay	CH
B-4	3 to 5	0.7	36%	Clayey Sand	SC
B-4	5 to 8		48%	Very clayey Sand	SC
B-5	17 to 23		67%	Very sandy Clay	СН
B-6	6 to 8	2	23%	Clayey Sand	SC
B-6	12to 15	3	21%	Clayey Sand	SC
B-7	11 to 17	``	59%	Very sandy Clay	CH
B-7	17 to 21		39%	Very clayey Sand	SC ·
B-7	21 to 27	1	24%	Clayey Sand	SC

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#### LABORATORY TESTING PROCEDURES

#### PERCENT FINES DETERMINATION ASTM D-1140

The percent fines or material passing the No. 200 mesh sieve was determined. The percent fines are the soil particles in the silt and clay size range.

## pH DETERMINATION (CALIFORNIA DOT 643)

The pH is measured by mixing distilled water with a soil sample until the soil particles are dispersed. Then the sample is checked for pH, using a pH meter.

## **ORGANIC CONTENT DETERMINATION ASTM D-2974**

This test method evaluates the moisture content, ash content, and organic matter in peats and other organic soils, such as organic clay, silt, sand, and "muck".

The organic content measurement was performed by placing a sample of soil in a low temperature oven. The soil is then dried (as described above) to measure the initial moisture content. The soil is then transferred to a high temperature kiln which burns off the organic materials. The organic content is then calculated as the ratio of the weight loss to the dry weight of the soil measured from the low temperature oven; it is expressed as a percent.

# **MOISTURE CONTENT DETERMINATION ASTM D-2216**

Moisture content is the ratio of the weight of water to the dry weight of soil. Moisture content is measured by drying a sample at 105 degrees Celsius. The moisture content is expressed as a percent of the oven dried soil mass.

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# CORROSION TESTING - FM 5-550 and FM5 - 551

Testing for corrosion parameters included pH and resistivity.

#### FALLING HEAD PERMEABILITY TEST - ASTM D - 5084

A number of recovered soil samples were selected to determine to determine Darcy's Coefficient of Permeability (k) of the soil. A falling head permeability test was performed on each soil specimen.

#### ATTERBERG LIMITS - ASTM D - 4318

Certain recovered soil samples were selected for Atterberg Limits testing to determine the soil plasticity characteristics. The soil's Plasticity Index (PI) is the range of moisture content over which the soil deforms as a plastic material. It is bracketed by the Liquid Limit (LL) and the Plastic Limit (PL). The LL is the moisture content at which the soil will flow as a heavy viscous fluid. The PL is the lowest moisture content at which the soil y plastic so as to be manually rolled into a 1/8-inch diameter thread.
# APPENDIX F

Summary of Classifications and Index Testing for Final Study Report of Corrosion Parameters for Final Study Laboratory Testing Procedures

# Summary of Classification and Index Testing for Final Study

Boring No.	ng Sample Fines Atterberg Permeability Depth, Ft. (%) LL PI		Organic Content	Unified Soil Classification			
			(70)				
A-6	20	87			*		СН
A-20	18	27		_			SC
A-24	8.5	26	_				SC
A-31	2	38		_			SC
A-33	4	34	—			_	SC
A-52	5.5	87			—	·	СН
A-59	1	41		_		<u> </u>	SC
A-71	1	30	_			_	SC
A-77	10	41	-	_		-	SC
B-1	16	76	88	54			СН
B-1	18	29	_	_			SC
B-2	10	89	102	57	united and the second second second second second second second second second second second second second second		MH
B-2	15	83	85	46	_		MH
B-3	20	16	<u> </u>	_			SM
B-4	18	31			_	— <u> </u>	SC
B-5	4	86	71	31	_		MH
B-5	10	83	62	34	un de la fait de la fait de la fait de la fait de la fait de la fait de la fait de la fait de la fait de la fait	<u></u>	MH
B-6	28	79	_			_	CH
B-8	9	25		_	_	antinet in the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second se	SC
B-8	19	73	88	51	_		CH-MH
B-9	29	45	36	13			SC
B-10	8	84	60	33	_		СН
B-10	22	24		_			SC
B-11	14	37	41	20		_	SC
B-11	19	85	73	46	_		CH
B-12	31	19	_		_	_	SC
B-13	19	38	41	18	_		SC

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SUMMARY OF FINAL STUDY LABORATORY TEST RESULTS								
Boring Nò.	Sample Depth,	Fines Content	Atterberg Limits		Permeability (Ft/day)	Organic Content	Unified Soil Classification	
an and the later of the second	<b>L L</b> •	(70)	LL	PI		(70)	n An an an an an an an an an an an an an an	
B-14	38	22	_	_		_	SC	
B-15	34	55	60	34		_	CH	
B-15	38	16				_	SM	
B-16	8	82	_	_	_		CH	
B-16	22	18	_			_	SC	
B-21	24	51	52	29	-		СН	
P-6	16	27	-		2		SC	
P-7	31	15			8		SP-SM	
P-8	23	23			2		SC	
P-12	17	22		-1	3		SC	
P-13	22	34	·		4		SC	
P-14	18	35			2		SC	
P-18	13	23			3		SC	
P-21	21	16			9		SP-SM	
P-27	18	21	-		3		SC ·	
P-28	13	28			2		SC	
P-29	13	45			1		SC [.]	
	·					-		

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## **REPORT OF CORROSION PARAMETERS FOR FINAL STUDY**

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Boring No.	Sample Depth, ft.	Sample Description pH Environ Classifi Steel		ımental ïcation Concrete	
A-20	15	Light gray & orange clayey Sand (SC)	4.19	Extremely Aggressive	Extremely Aggressive
A-24	8	Light brown to tan clayey Sand (SC)	5.54	Extremely Aggressive	Moderately Aggressive
B-3	20	Tan & light gray slightly clayey Sand (SM-SC)	6.08	Moderately Aggressive	Moderately Aggressive
B-12	31	Light gray clayey Sand (SC)	6.59	Moderately Aggressive	Moderately Aggressive

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#### LABORATORY TESTING PROCEDURES

#### PERCENT FINES DETERMINATION ASTM D-1140

The percent fines or material passing the No. 200 mesh sieve was determined. The percent fines are the soil particles in the silt and clay size range.

#### pH DETERMINATION (CALIFORNIA DOT 643)

The pH is measured by mixing distilled water with a soil sample until the soil particles are dispersed. Then the sample is checked for pH, using a pH meter.

#### **ORGANIC CONTENT DETERMINATION ASTM D-2974**

This test method evaluates the moisture content, ash content, and organic matter in peats and other organic soils, such as organic clay, silt, sand, and "muck".

The organic content measurement was performed by placing a sample of soil in a low temperature oven. The soil is then dried (as described above) to measure the initial moisture content. The soil is then transferred to a high temperature kiln which burns off the organic materials. The organic content is then calculated as the ratio of the weight loss to the dry weight of the soil measured from the low temperature oven; it is expressed as a percent.

#### **MOISTURE CONTENT DETERMINATION ASTM D-2216**

Moisture content is the ratio of the weight of water to the dry weight of soil. Moisture content is measured by drying a sample at 105 degrees Celsius. The moisture content is expressed as a percent of the oven dried soil mass.

#### CORROSION TESTING - FM 5-550 and FM5 - 551

Testing for corrosion parameters included pH and resistivity.

#### FALLING HEAD PERMEABILITY TEST - ASTM D - 5084

A number of recovered soil samples were selected to determine to determine Darcy's Coefficient of Permeability (k) of the soil. A falling head permeability test was performed on each soil specimen.

#### ATTERBERG LIMITS - ASTM D - 4318

Certain recovered soil samples were selected for Atterberg Limits testing to determine the soil plasticity characteristics. The soil's Plasticity Index (PI) is the range of moisture content over which the soil deforms as a plastic material. It is bracketed by the Liquid Limit (LL) and the Plastic Limit (PL). The LL is the moisture content at which the soil will flow as a heavy viscous fluid. The PL is the lowest moisture content at which the soil sufficiently plastic so as to be manually rolled into a 1/8-inch diameter thread.

# APPENDIX G

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Important Information About Your Geothechnical Report Constrain and Restrictions

# Important Information About Your Geotechnical Engineering Report

## Subsurface problems are a principal cause of construction delays, cost overruns, claims, and disputes.

#### The following information is provided to help you manage your risks.

# Geotechnical Services Are Performed for Specific Purposes, Persons, and Projects

Geotechnical engineers structure their services to meet the specific needs of their clients. A geotechnical engineering study conducted for a civil engineer may not fulfill the needs of a construction contractor or even another civil engineer. Because each geotechnical engineering study is unique; each geotechnical engineering report is uniquely prepared for the client. No one except you should rely on your geotechnical engineering report without first confiding with the geotechnical engineer who prepared it. And no one-not even you-should apply the report for any purpose or project except the one originally contemplated.

#### A Geotechnical Engineering Report is Based on A Unique Set of Project Specific Factors

Geotechnical engineers consider a number of unique project specific factors when establishing the scope of a study. Typical factors include: the client's goals, objectives, and risk management preferences; the general nature of the structure involved, its size, and configuration; the location of the structure on the site; and other planned or existing site improvements, such as access roads, parking lots, and underground utilities. Unless the geotechnical engineer who conduced the study specifically indicates otherwise, do not rely on a geotechnical engineering report that was:

- not prepared for you,
- not prepared for your project
- not prepared for the specific site explored, or
- completed before important project changes were made.

Typical changes that can erode the reliability of an existing geotechnical engineering report include those that affect;

 the function of the proposed structure as when it's changed from a parking garage to an office building, or from a light industrial plant to a refrigerated warehouse,

- elevation, configuration, location, orientation, or weight of the proposed structure,
- composition of the design team, or
- project ownership

As a general rule, always inform your geotechnical engineer of project changes-even minor ones-and request an assessment of their impact. Geotechnical engineers cannot accept responsibility or liability for problems that occur because their reports do not consider developments of when they were not informed.

#### Subsurface Conditions Can Change

A geotechnical engineering report is based on conditions that existed at the time the study was performed. Do not rely on a geotechnical engineering report whose adequacy may have been affected by the passage of time; by man-made events, such as construction on or adjacent to the site; or by natural events such as flood, earthquakes, or groundwater fluctuations. Always contact the geotechnical engineer before applying the report, to determine if it is still reliable. A minor amount of additional testing or analysis could prevent major problems.

#### Most Geotechnical Findings Are Professional Opinions

Site exploration identified subsurface conditions only at those points where subsurface tests are conducted or samples are taken. Geotechnical engineers review field and laboratory data and then apply their professional judgement to render an opinion about subsurface conditions throughout the site. Actual subsurface conditions may differ-sometimes significantly-from those indicated in your report. Retaining the geotechnical engineer who developed your report to provide construction observation is the most effective method of managing the risks associated with unanticipated conditions.

#### **CONSTRAINTS AND RESTRICTIONS**

#### WARRANTY

Universal Engineering Sciences has prepared this report for our client for his exclusive use, in accordance with generally accepted soil and foundation engineering practices, and makes no other warranty either expressed or implied as to the professional advice provided in the report.

#### UNANTICIPATED SOIL CONDITIONS

The analysis and recommendations submitted in this report are based upon the data obtained from soil borings performed at the locations indicated on the Boring Location Plan. This report does not reflect any variations which may occur between these borings.

The nature and extent of variations between borings may not become known until excavation begins. If variations appear, we may have to re-evaluate our recommendations after performing native observations and noting the characteristics of any variations.

#### CHANGED CONDITIONS

We recommend that the specifications for the project require that the contractor immediately notify Universal Engineering Sciences, as well as the owner, when subsurface conditions are encountered that are different from those present in this report.

No claim by the contractor for any conditions differing from those anticipated in the plans, specifications, and those found in this report, should be allowed unless the contractor notifies the owner and Universal Engineering Sciences of such changed conditions. Further, we recommend that all foundation work and site improvements be observed by a representative of Universal Engineering Sciences to monitor field conditions and changes, to verify design assumptions and to evaluate and recommend any appropriate modifications to this report.

#### **MISINTERPRETATION OF SOIL ENGINEERING REPORT**

Universal Engineering Sciences is responsible for the conclusions and opinions contained within this report based upon the data relating only to the specific project and location discussed herein. If the conclusions or recommendations based upon the data presented are made by others, those conclusions or recommendations are not the responsibility of Universal Engineering Sciences.

#### CHANGED STRUCTURE OR LOCATION

This report was prepared in order to aid in the evaluation of this project and to assist the architect or engineer in the design of this project. If any changes in the design or location of the structure as outlined in this report are planned, or if any structures are included or added that are not discussed in the report, the conclusions and recommendations contained in this report shall not be considered valid unless the changes are reviewed and the conclusions modified or approved by Universal Engineering Sciences.

#### USE OF REPORT BY BIDDERS

Bidders who are examining the report prior to submission of a bid are cautioned that this report was prepared as an aid to the designers of the project and it may affect actual construction operations.

Bidders are urged to make their own soil borings, test pits, test caissons or other investigations to determine those conditions that may affect construction operations. Universal Engineering Sciences cannot be responsible for any interpretations made from this report or the attached boring logs with regard to their adequacy in reflecting subsurface conditions which will affect construction operations.

#### STRATA CHANGES

Strata changes are indicated by a definite line on the boring logs which accompany this report. However, the actual change in the ground may be more gradual. Where changes occur between soil samples, the location of the change must necessarily be estimated using all available information and may not be shown at the exact depth.

#### **OBSERVATIONS DURING DRILLING**

Attempts are made to detect and/or identify occurrences during drilling and sampling, such as: water level, boulders, zones of lost circulation, relative ease or resistance to drilling progress, unusual sample recovery, variation of driving resistance, obstructions, etc.; however, lack of mention does not preclude their presence.

#### WATER LEVELS

Water level readings have been made in the drill holes during drilling and they indicate normally occurring conditions. Water levels may not have been stabilized at the last reading. This data has been reviewed and interpretations made in this report. However, it must be noted that fluctuations in the level of the groundwater may occur due to variations in rainfall, temperature, tides, and other factors not evident at the time measurements were made and reported. Since the probability of such variations is anticipated, design drawings and specifications should accommodate such possibilities and construction planning should be based upon such assumptions of variations.

#### LOCATION OF BURIED OBJECTS

All users of this report are cautioned that there was no requirement for Universal Engineering Sciences to attempt to locate any man-made buried objects during the course of this exploration and that no attempt was made by Universal Engineering Sciences to locate any such buried objects. Universal Engineering Sciences cannot be responsible for any buried man-made objects which are subsequently encountered during construction that are not discussed within the text of this report.

#### TIME

This report reflects the soil conditions at the time of investigation. If the report is not used in a reasonable amount of time, significant changes to the site may occur and additional reviews may be required.

# APPENDIX H

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Geotechnical Investigation Fact Sheet Foundation Design Criteria Foundation Subsurface Preparation Pavement Design Calculations Pavement Section Design

#### **GEOTECHNICAL INVESTIGATION FACT SHEET**

PROJECT LOCATION: Wal-Mart SuperCenter Store No. 3873-00 SEC I-75 and U.S. 441, Alachua, Alachua County, Florida PHONE #: 352-372-3392 ENGINEER: David Barreiro, P.E. GEOTECHNICAL ENGINEERING COMPANY: Universal Engineering Sciences REPORT DATE: April 30, 2005 Ground Water Depth: <u>3 to 23 feet below existing site grades</u> Date Groundwater Measured: _____January 27, 2005 through February 9, 2005 Topsoil/Stripping Depth: <u>6 to 12 inches</u> Modified Proctor Results: N/A **Recommended Compaction Control Tests:** 1 Test for Each 2,500 Sq. Ft. each Lift (bldg. area) 1 Test for Each 10,000 Sq. Ft. each Lift (parking area) Structural Fill Maximum Lift Thickness <u>12</u> in. (Measured loose) Subgrade Design CBR value = 26 (LBR = 40)Fill Soils Characteristics: Maximum Liquid Limit: _40 Maximum Plasticity Index: <u>10</u> Specified Compaction: _95% Modified Proctor Moisture Content Range: <u>+/-2% of Optimum</u> CONCRETE **COMPONENT** ASPHALT Standard Heavy Standard Heavy Stabilized Subgrade* <u>4"</u> 6" 6" 4" (If Applicable) Base Material* <u>4"</u> <u>4"</u> <u>6"</u> <u>6"</u> (Limerock or Crushed Concrete) * Free draining materials *. <u>N/A</u> Asphaltic Base Course <u>N/A</u> 2.5" <u>2.0"</u> Leveling Binder Course 1.0" 1.5" <u>5"</u> (conc. thickness) <u>6"</u> Surface Course

# FOUNDATION DESIGN CRITERIA

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PROJECT LOCATION:	Wal-Mart SuperCen SEC I-75 and U.S.	nter Store No. 1 441, Alachua,	3873-00 Alachua Coun	ty, Florida	
ENGINEER:	David Barreiro, P	.E.	PHONE #:	352 <b>-</b> 372-3392	
GEOTECHNICAL ENGIN	EERING COMPAN	Y: Universal	Engineering So	ciences	
REPORT DATE:	April 30, 2005				
Foundation Type: Sp	read Footings				
Allowable bearing pressure:	2,500 psf				
Factor of Safety:	+2				
Minimum footing dimension	ns: Individual:	24"	Continuous:	18"	
Minimum footing Embedme	ent: Exterior:	18"	Interior:		
Frost depth: <u>None</u>					
Maximum foundation settle	ments: Total:	3/411			
	Differential	1/2"			
Slab: Potential vertical rise	: None antic	ipated if under	<u>cut recommen</u>	dations are followed	
Vapor barrier or capillary bi	reak (describe):	Plastic Sheet (	10 MIL Polyet	hylene)	
Subgrade reaction modulus:	150 psi/in Me	thod obtained:	<u>NAVFAC</u>	<u>2 Dm 7.1, page 219,</u>	
Figure 6 Perimeter Drains	s (describe): Buildin	ng: <u>Under</u>	drains for TLE	pit	
Retaining Walls:	Wall drains/underd	rains to preven	t excessive hye	drostatic pressures	
Pavements: Unde	erdrains as dictated 1	oy seasonal hig	h groundwater	levels	
Cement Type: <u>Type I</u>	<u></u>				
Retaining Wall: At rest pressure: $K = 0.5$					
Coefficient of fri	ction:0.4_				
COMMENTS: N/	/A				
NOTE: This information	should not be used	separately fron	n the geotechn	ical report.	

#### FOUNDATION SUBSURFACE PREPARATION

#### WAL★MART SUPERCENTER STORE NO. 3873-00 SEC I-75 AND U.S. 441, ALACHUA, ALACHUA COUNTY, FLORIDA

UNLESS SPECIFICALLY INDICATED OTHERWISE IN THE DRAWINGS AND/OR SPECIFICATIONS, THE LIMITS OF THIS SUBSURFACE PREPARATION ARE CONSIDERED TO BE THAT PORTION OF THE SITE DIRECTLY BENEATH AND 10 FEET BEYOND THE BUILDING AND APPURTENANCES. APPURTENANCES ARE THOSE ITEMS ATTACHED TO THE BUILDINGS PROPER (REFER TO DRAWING SHEET SP1) AND TYPICALLY INCLUDE, BUT ARE NOT LIMITED TO, THE BUILDING SIDEWALKS, GARDEN CENTER, PORCHES, RAMPS, STOOPS, TRUCK WELLS/DOCKS, CONCRETE APRONS AT THE AUTOMOTIVE CENTER, COMPACTOR PAD, ETC. THE SUB-BASE AND THE VAPOR BARRIER, WHERE REQUIRED, DO NOT EXTEND BEYOND THE LIMITS OF THE ACTUAL BUILDING AND APPURTENANCES.

IN CONSIDERATION OF THE INTENDED USE OF AN EXPOSED CONCRETE FLOOR, ESTABLISH THE FINAL SUB-GRADE ELEVATION AT 11.5 INCHES BELOW THE FINISHED CONCRETE ELEVATION TO ALLOW FOR A 5.5-INCH SLAB, OR AT 10 INCHES BELOW THE FINISHED FLOOR TO ALLOW FOR A 4 INCH SLAB, UNDERLAIN BY A 10 MIL THICK POLYETHYLENE VAPOR BARRIER, ATOP A 6 INCH AGGREGATE SUBBASE. PER WAL-MART SPECIFICATIONS, THE SUBBASE SHALL CONSIST OF 4 INCHES OR COARSE AGGREGATE MEETING THE GRADATION REQUIREMENTS OF ASTM D-448 (#67) COVERED BY 2 INCHES OF FINE AGGREGATE MEETING THE GRADATION REQUIREMENTS OF ASTM D-448 (#10) WITH 6% TO 12% MATERIAL PASSING THE NO. 200 SIEVE. MATERIAL SUCH AS CLEAN SAND OR MORE UNIFORMLY GRADED AGGREGATE SUCH AS #57 STONE FOR THE SUBBASE ARE NOT ACCEPTABLE. THE CONTRACTOR SHALL BE RESPONSIBLE FOR OBTAINING ACCURATE MEASUREMENTS OF ALL CUT AND FILL DEPTHS REQUIRED.

STRIP ALL UNSUITABLE SURFACE MATERIALS INCLUDING SURFACE VEGETATION, ORGANICS, TOPSOIL, ROOTS AND ANY UNSUITABLE SURFACE SOILS FROM THE CONSTRUCTION AREA. THESE MATERIALS SHALL BE WASTED FROM THE SITE OR IF APPROVED BY THE OWNER AND ENGINEER, USED AS TOPSOIL IN LANDSCAPE AREAS WHERE PERMITTED. ANY ANTICIPATED FOUNDATION, FLOOR-SLAB, OR FILL AREA SHALL BE DENSIFIED AND THEN PROOFROLLED TO DETERMINE IF ANY UNSTABLE SOIL CONDITIONS EXIST. ANY UNSTABLE AREAS SHALL BE UNDERCUT AND REPLACED WITH COMPACTED STRUCTURAL FILL.

STRUCTURAL FILL PLACED IN THE BUILDING AREA SHALL CONSIST OF INORGANIC, NON PLASTIC GRANULAR SOILS WITH LESS THAN THAT 10 PERCENT PASSING THE #200 SIEVE (RELATIVELY CLEAN SAND WITH UNIFIED SOIL CLASSIFICATION OF SP, SW, SP-SM OR SW-SM). THE FILL SHALL BE PLACED IN MAXIMUM 12 INCH LOOSE LIFTS AND COMPACTED TO AT LEAST 95 PERCENT OF THE MODIFIED PROCTOR MAXIMUM DRY DENSITY (ASTM D-1557). THE MOISTURE CONTENT SHALL BE CONTROLLED TO AT LEAST PLUS OR MINUS 2 PERCENT OF OPTIMUM. STRUCTURAL FILL SHALL MEET THE FOLLOWING REQUIREMENT:

LOCATION WITH RESPECT TO FINAL GRADE	<u>P.I.</u>	<u>L.L</u> .
BUILDING AREA, BELOW UPPER 4 FEET	10	40
BUILDING AREA, UPPER 4 FEET	NP	NP

HIGH PERCHED GROUNDWATER LEVEL CONDITIONS MAY PREVAIL IN SOME AREAS OF THE SITE AND GROUNDWATER CONTROL SHOULD BE ANTICIPATED, PARTICULARLY IN AREAS THAT ARE DEEPLY STRIPPED OR UNDERCUT. SHALLOW GROUNDWATER CONTROL CAN TYPICALLY BE MAINTAINED BY PUMPING FROM SUMPS IN PERIMETER DITCHES OR PITS.

THE FOUNDATION SYSTEM SHALL BE CONTINUOUS STRIP FOOTINGS AT THE WALLS AND ISOLATED SPREAD FOOTINGS AT THE COLUMN LOCATIONS. THE SOILS TO A DEPTH OF 1 FOOT BELOW THE BASE OF ALL FOUNDATION EXCAVATIONS SHALL BE COMPACTED TO 95 PERCENT OF THE MODIFIED PROCTOR MAXIMUM DRY DENSITY (ASTM D1557).

THIS FOUNDATION SUBSURFACE PREPARATION DOES NOT CONSTITUTE A COMPLETE SITE WORK SPECIFICATION. INFORMATION COVERED IN THIS PREPARATION GOVERNS OVER THE CONTRACT SPECIFICATIONS. REFER TO THE SITE WORK SPECIFICATIONS AND THE GEOTECHNICAL REPORT BY UNIVERSAL ENGINEERING SCIENCES DATED APRIL 30, 2005, UES PROJECT NO. 70080-077-06 AND REPORT NO. 385573, FOR SPECIFIC INFORMATION NOT COVERED IN THIS PREPARATION. THE GEOTECHNICAL REPORT IS FOR INFORMATION ONLY AND IS NOT CONSIDERED A DESIGN SPECIFICATION.

AN E-MAIL ADDRESS FOR THE GEOTECHNICAL ENGINEER David Barreiro, P.E.:

dbarreiro@uesorl.com

(A FINAL REVIEW OF THE PAD PREP BEFORE THE CONSTRUCTION DOCUMENTS ARE COMPLETED IS REQUIRED.)

#### PAVEMENT DESIGN CALCULATIONS Wal-Mart Supercenter

Minimum Pavement Design Recommendations per Wal-Mart (revised 4/19/04)

Standard Duty

- design life of 20 years
- Equilvalent 18 kip Single Axle Load (ESAL) = 109,500 for 20 yrs (Supercenter)
- Daily ESAL = 15
- Reliability = 85%
- Initial Serviceability = 4.2
- Terminal Serviceability = 2.0
- Standard Deviation = 0.45 for flexible 0.35 for rigid
- Minimum thickness = 3" of Asphalt and 5" of Concrete

#### Heavy Duty

- design life of 20 years
- Equilvalent 18 kip Single Axle Load (ESAL) = 335,800 for 20 yrs (Supercenter)
- Daily ESAL = 29
- Reliability = 85%
- Initial Serviceability = 4.2
- Terminal Serviceability = 2.0
- Standard Deviation = 0.45 for flexible 0.35 for rigid
- Minimum thickness = 4" of Asphalt and 6" of Concrete

All concrete pavements must be underlain by 4 inches of compacted granular base course or sand with LBR minimum of 20.

#### Flexible Pavement Design

Florida Department of Transportation - Flexible Pavement Design Manual (Jan 2002)

Structural Numbers are calculated by the AASHTO Methods

AASHTO Design Equation for Flexible Pavement

 $\log_{10} W_{18} = Z_R * 9.36 * \log_{10} (SN_R + 1) - 0.20 + \frac{\log_{10} (\frac{\Delta PSI}{4.2 - 1.5})}{0.40 + \frac{1094}{(SN_R + 1)^{519}}} + 2.32 * \log_{10} (M_R) - 8.07$ 

SN_B = Structural Number required

So

 $W_{18}$  = Equilvalent 18 kip Single Axle Load (given by Wal-Mart)

- $Z_{\rm R}$  = Standard Normal Deviate (taken from Page A.3.0 relative to Reliability)
- $M_{\rm B}$  = Resilient Modulus psi (Table 5.1 from estimated LBR results of 20)
  - = Standard Deviation (given by Wal-Mart)
- $\Delta PSI = Change in serviceability (Terminal Serviceability normally assumed 2.5 by$

#### FDOT Calculations continued

Layer Thickness Calculations for Proposed Pavement Sections (SN_c)

$$SN_{C} = (a_{1} * D_{1}) + (a_{2} * D_{2}) + (a_{3} * D_{3}) + \dots + (a_{N} * D_{N})$$

SN _c	= Structural Number calculated
a _N	= Layer coefficient of layer (FDOT Table 5.4 Structural Coefficients)
D _N	= Layer thickness

Standard Duty

Proposed Pavement Section

Туре	<u>d</u>	*	<u>a</u>		
Asphalt	3 inches		0.44		1.32
Shell Base (LBR 100)	6 inches		0.18		1.08
Type B Stabilized (LBR 40)	6 inches	-	0.08		<u>0.48</u>
				Total	2.88

 $SN_{C} = 2.88$  for Asphalt greater than  $SN_{R} = 2.27$ 

#### Heavy Duty

Proposed Pavement Section

Type	<u>d</u>	*	<u>a</u>	
Asphalt	4 inches		0.44	1.72
Shell Base (LBR 100)	6 inches		0.18	1.08
Type B Stabilized (LBR 40)	6 inches		0.08	<u>0.48</u>
			Total	3.32

 $SN_C = 3.32$  for Asphalt greater than  $SN_R = 2.71$ 

Good

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Rigid Pavement Design

AASHTO - Design of Pavement Systems (1993)

Depths of Concrete Required are calculated by the AASHTO Methods

AASHTO Design Equation for Rigid Pavement

$$\log_{10} W_{18} = z_R * s_O + 7.35 * \log_{10}(D+1) - 0.06 + \frac{\log_{10} \left[\frac{\Delta PSI}{4.5 - 1.5}\right]}{1 + \frac{1.624 * 10^7}{(D+1)^{8.46}}} + (4.22 - 0.32p_t) * \log_{10} \left[\frac{s_c' * c_d \left[D^{0.75} - 1.132\right]}{215.63 * J \left[D^{0.75} - \frac{18.42}{(E_c / k)^{0.25}}\right]}\right]$$

D	= Depth of concrete required
W ₁₈	= Equivalent 18 kip Single Axle Load (given by Wal-Mart)
k	= Effective Modulus of Subgrade Reaction (determined from onsite soils)
s' _c	= Mean Concrete Modulus of Rupture (typically 650 psi)
J	= Load Transfer Coefficient (typically 3.2)
c _d	= Drainage Coefficient (typically 1.0)
DPSI	= Design Serviceability loss (given by Wal-Mart)
So	= Standard Deviation (given by Wal-Mart)

The thickness of concrete calculated for standard duty is: 3.16 Required: 5 inches

The thickness of concrete calculated for heavy duty is: 4.65 Required: 6 inches

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